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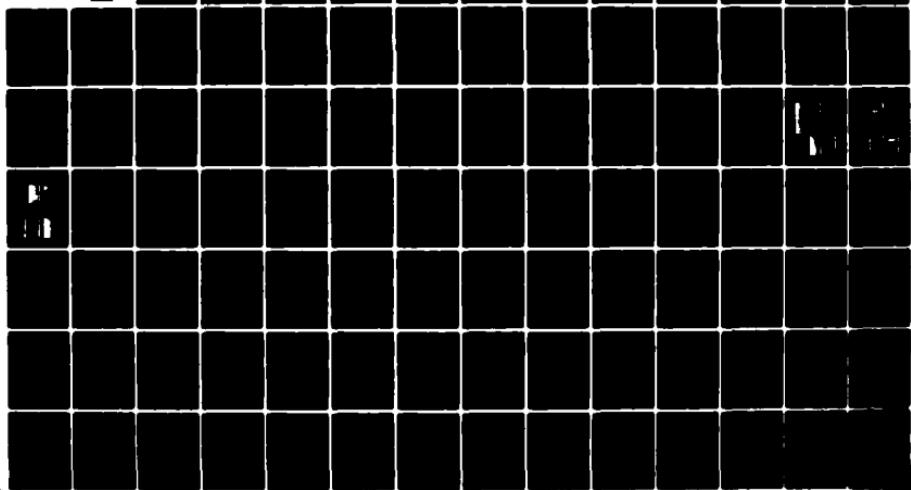
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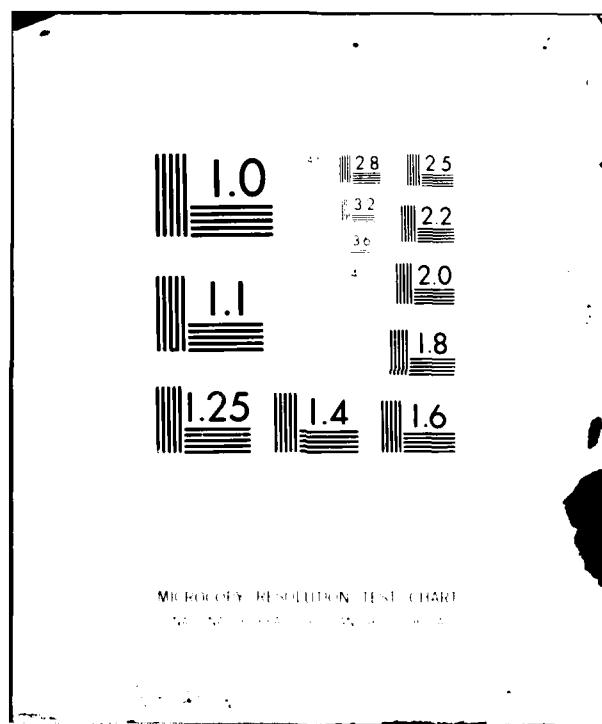
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Monterey, California



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OFFSHORE TRANSPORT AND DIFFUSION IN THE
LOS ANGELES BIGHT - II, NPS DATA SUMMARY

G.E. Schacher, K.L. Davidson

and C.A. Leonard

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Environmental Physics Group

Naval Postgraduate School

Monterey, California

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Prepared for: Outer Continental Shelf Division
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Los Angeles, California 90017

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| The second in a series of tracer measurements of overwater transport and diffusion has been completed. This report includes the meteorological data obtained aboard the RV/Acania. Analyses of radiosonde data to yield mixed layer parameters for mixed layer assessment is also included. | | |

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I. Introduction

During January of 1981 the Environmental Physics Group of the Naval Postgraduate School (NPS) and Aerovironment, Inc. conducted the second of two transport and dispersion experiments in the Santa Barbara Channel area of the California coast. The purpose of these operations was to perform offshore tracer experiments in order to parameterize dispersion models that are in current use and to build a data base for future model development. The purpose of this and the previous data report is to present the pertinent meteorological and source data for use by those who will be involved in the modeling effort. In the previous report only the basic data, reduced to engineering units, was presented. This report presents the second operations data in the same format and, in addition, includes mixed layer parameters for both operations. Application of these results to the models will be the subject of a future joint report by Aerovironment and NPS. A great deal of the discussion of the data in this report is the same as the first report and is included for the sake of completeness.

Although the data gathered in this experiment has much wider application, it was collected for the specific purpose of parameterizing models that will be used to assess the onshore impact of offshore oil exploration

and production sites. Such impact currently has great importance since many coastal areas are near the legal air pollution limit and any significant additional loading could push them over the limit. Air pollution models in current use have not been adequately validated for the overwater regime. The results of this study should remedy the inadequacy of the models.

During the tracer experiments SF₆ gas was released from the ship RV/Acania and tracked by an aircraft, a small boat, and one mobile and fixed stations on shore. Meteorological data was gathered on the ship and on the shore. This report contains shipboard meteorological data and gas source strength. Shore meteorological data and tracer results can be found in a report by Aerovironment.

II. Ship Operation Scenario

Since the impact of offshore sources on the shore is the purpose of these investigations the experiments must be performed during periods of onshore winds. These winds must be of a fairly long duration since it takes a minimum of 6 hours to gather enough data during any one experiment. The preliminary decision to release the tracer gas on any given day must be made on the previous day due to the time needed to prepare all of the sampling sites. Thus, the following schedule was used.

All Days

1. 0800-1200-2000: radio shipboard meteorological data to shore.
2. 1000: Shore obtains weather forecast from Point Mugu.
3. 1200: shore command center makes a go/no-go decision for a release on the following day.

Release Day

4. 0700: begin hourly wind reports to shore.
5. 1000: decision on release made by ship-shore communication, final decision made on shore.
6. Final positioning of ship.
7. 1100: start tracer gas release.
8. 1800: end tracer gas release and hourly wind reports.

Due to the variability of the wind during the period it was normally not possible to start the release by 1100.

Because of difficulty in moving the shore stations, targeting of the plume was accomplished by moving the ship. This had to be done before the release was begun because moving the ship would introduce wander into the plume trajectory and contaminate the results. In order to hold the ship stationary to the degree needed it was anchored during a release.

Significant Events:

At times, the ship was performing tasks not directly associated with this study or was in port. As an aid in interpreting the data we list times of "significant shipboard events" in Table 1.

| | | |
|------|------|---|
| 1/5 | 0940 | Underway from Monterey |
| 1/6 | 1250 | Arrive off Ventura |
| 1/9 | 1820 | Underway for Port Hueneme |
| | 1955 | Dock |
| 1/13 | 0500 | Underway |
| | 0610 | Arrive at operation area |
| 1/15 | 1723 | Underway for Port Hueneme, operation completed |

Table 1 - Significant Shipboard Events

III. Shipboard Equipment

We give here a brief description of the meteorological measurements that were made on the ship. Details of the equipment and calibration procedures can be found in a previous report. Two meteorological stations at heights of 7 m and 20.5 m above mean sea level were used. At each level the following parameters were measured:

relative wind speed

relative wind direction (upper level only)

air temperature

dew point

wind speed fluctuation

The following parameters were also measured:

sea surface temperature

ship roll

ship location

inversion height

temperature and humidity profiles to 5,000 ft.

sky cloud cover

The temperature and humidity profiles were obtained by shipboard radiosonde launch and were taken every 12 hours. The temperature inversion height was determined by an acoustic sounder which gave a continuous strip chart record. Most data listed above was averaged for one half hour intervals. The exceptions were relative wind direction and ships roll. For both, 10 sec averages were obtained and recorded for the full period of a gas release.

IV. Tracer Release Data

Four separate experiments were performed. For each the gas was released through the exhaust of one of the ship's motor generator sets. The exhaust is inclined at an angle of 45° above the horizontal. The motor is a 2 cycle diesel so exhaust flow rate is obtained by multiplying 2/3 times the displacement times the revolutions per minute. The pertinent exhaust outlet data to characterize plume rise are:

| <u>rpm</u> | <u>displacement (Cu in)</u> | <u>Stack Temp. (°F)</u> | <u>Flow Rate (cu in/sec)</u> | <u>Diameter (in)</u> |
|------------|---------------------------------|---------------------------------|--------------------------------------|--------------------------|
| 1500 | 426 | 250 | 7.13×10^3 | 4.5 |

Table 2. Characteristics of exhaust used during tracer gas releases.

For a release, 4 tanks of SF₆ were connected to a single manifold. The manifold has a pressure gauge and two rotometers, one supplied by the manufacturer and one calibrated and supplied by Aerovironment. The second meter was used to set the flow rate the first to monitor it since it was less subject to fluctuations. The gas pressure to the rotometers was maintained at 25 lbs/in.

Using the data found in Table 4 the flow rates for the four releases were

| | | |
|-----------|-------|--------|
| Release 1 | 48.35 | lbs/hr |
| Release 2 | 48.06 | lbs/hr |
| Release 3 | 44.45 | lbs/hr |
| Release 4 | 46.21 | lbs/hr |

During the releases the ship was anchored approximately 5 Nmi SWW of Ventura. As stated above the releases started at approximately 1100 and ended at approximately 1800. The exact times and locations are given in Table 3.

| <u>Release</u> | <u>Date</u> | <u>Latitude</u> | <u>Longitude</u> | <u>Start Time</u> | <u>End Time</u> |
|----------------|-------------|-----------------|------------------|-------------------|-----------------|
| 1 | 1/6 | 34°15.0'N | 119°20.0'W | 1322 | 1800 |
| 2 | 1/9 | 34°14.4'N | 119°20.3'W | 1123 | 1800 |
| 3 | 1/13 | 34°14.4'N | 119°20.3'W | 1134 | 1702 |
| 4 | 1/15 | 34°11.4'N | 119°19.4'W | 1406 | 1700 |

Table 3. Exact locations and start and end times for each release. Times are local, Pacific Daylight Time.

| <u>Bottle Number</u> | <u>Initial Weight (lbs)</u> | <u>Release 1</u> | <u>Release 2</u> | <u>Weight after Release 3</u> | <u>Release 4</u> |
|----------------------|-----------------------------|------------------|------------------|-------------------------------|------------------|
| 8 | 252 | | | | 186 |
| 9 | 256 | | | | 188 |
| 10 | 259 | 148 | | | |
| 11 | 252 | 139 | | | |
| 12 | 251 | | 140 | | |
| 13 | 254 | | 142 | | |
| 14 | 252 | | 157 | | |
| 15 | 260 | | | 185 | |
| 16 | 278 | | | 185 | |
| 17 | 250 | | | 175 | |
| Total Weight | 224 | 318 | 243 | 134 | |
| Total Release Time | 4:38 | 6:37 | 5:28 | 2:54 | |

Table 4. SF₆ bottle weights before and after the four releases. The total times for each release and the total weights of SF₆ used are also given.

V. Wind Histories

Hourly average wind histories taken aboard the RV/Acania are shown in Figures 1. The winds were recorded at least every hour and every half hour immediately before and during each release. These visual presentations were kept up to date on the ship and aided in the go/no-go decisions on release days.

If one compares these histories with those for the first operation during September 1980, it is immediately apparent that the wind was much less predictable during January. During the fall a well established land-sea breeze cycle existed. During the winter the sea breeze during the afternoon was not at all reliable in magnitude nor direction and, on some days, never became established at all.

Figure 1a

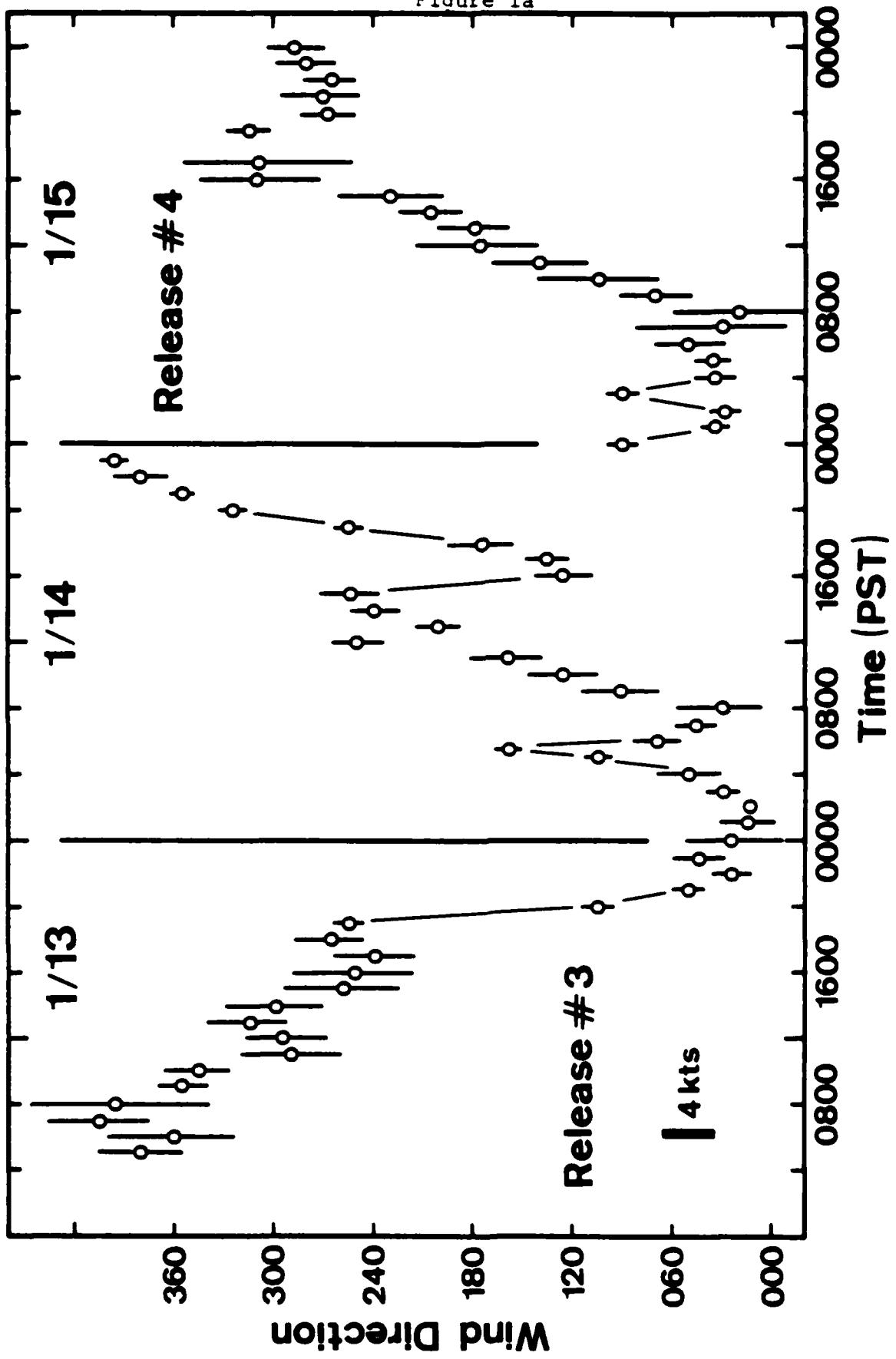


Figure 1b

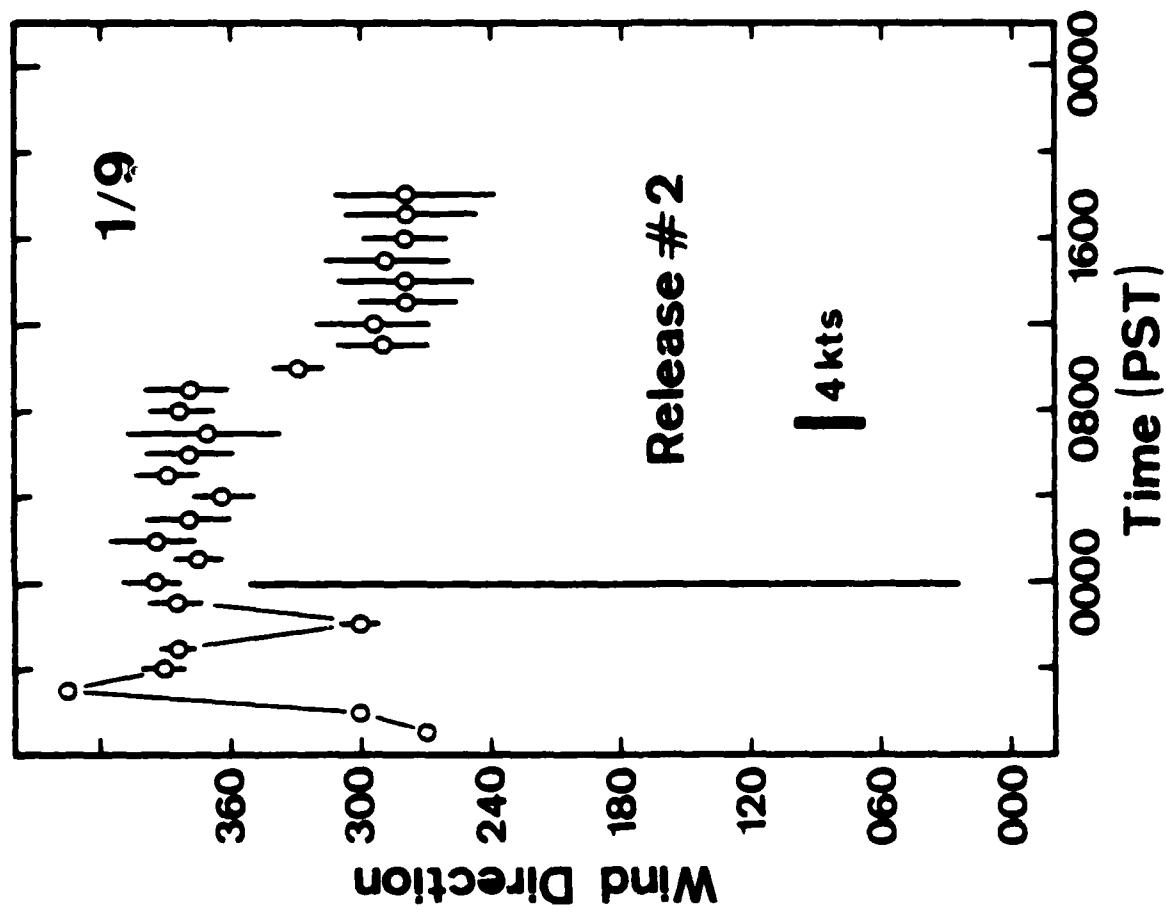
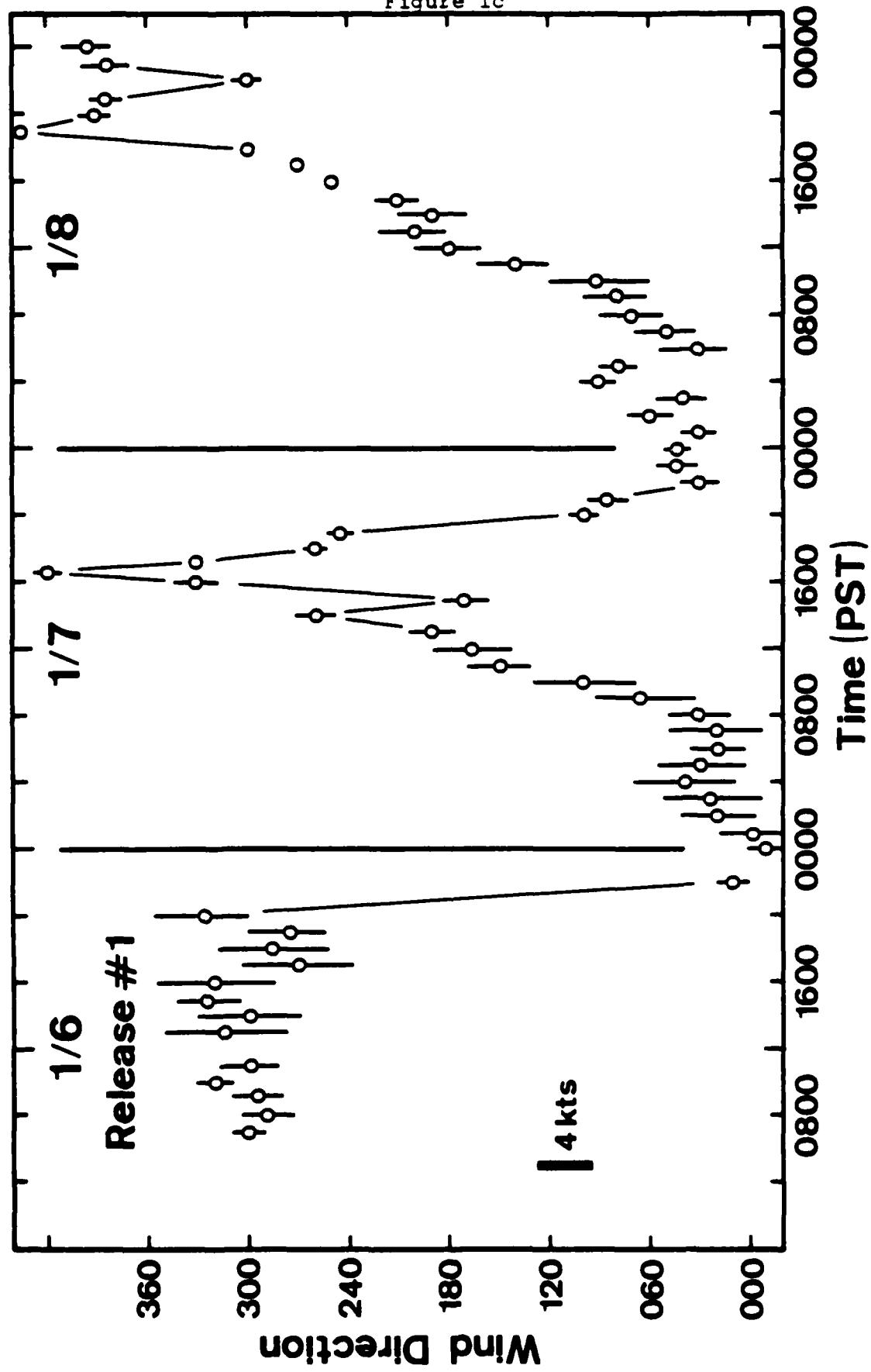


Figure 1c

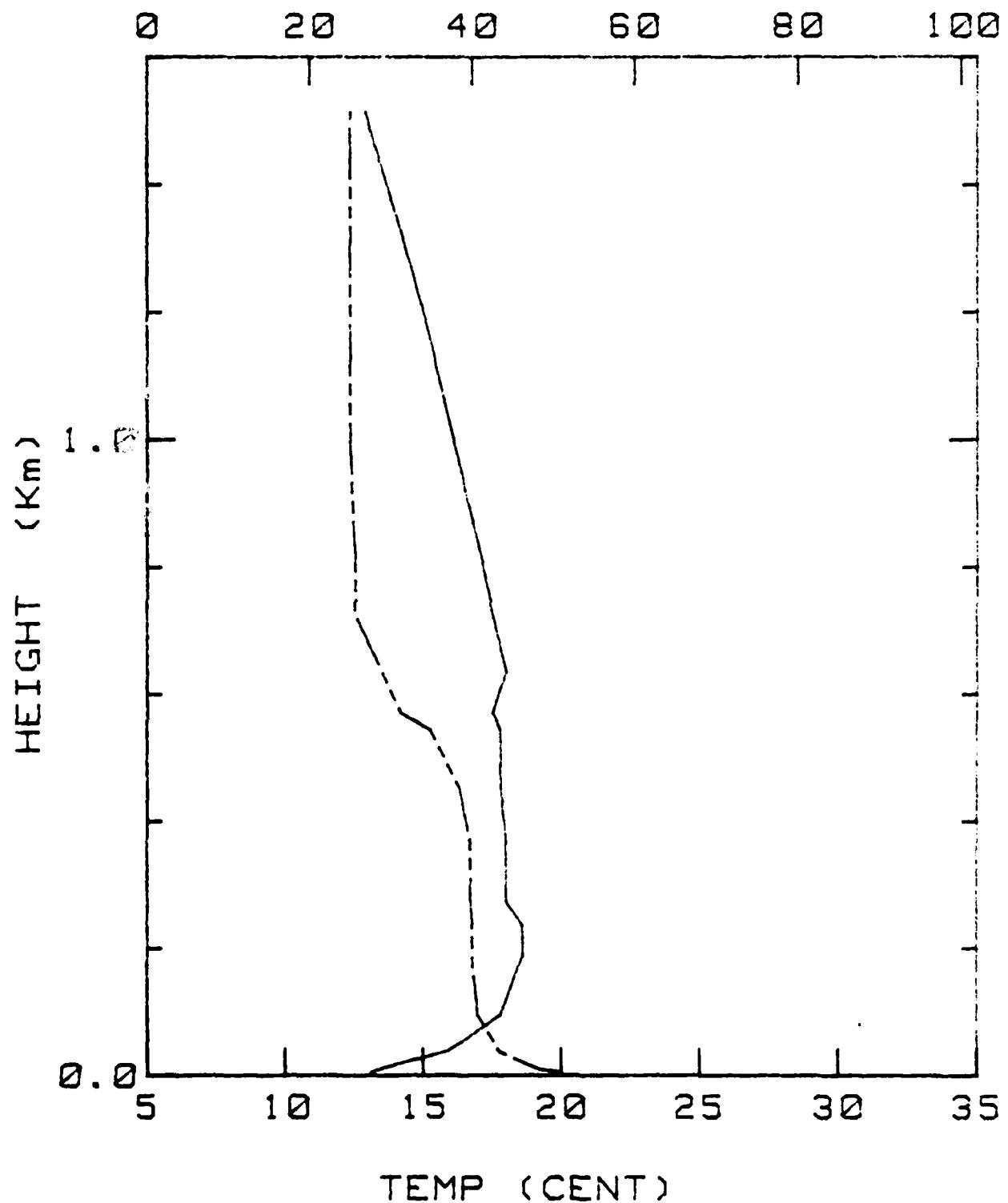


VI. Radiosonde Results

Radiosondes were released from the ship twice in each 24-hour period, generally at 0700 and 1900 PDT. Releases were made and interpreted by a Navy radiosonde team. Temperature and humidity were determined at standard levels and significant points. Since we are interested in the detailed structure of the boundary layer such a treatment is too coarse. Thus, the original strip chart output and the met team determined calibration points were used to construct fine scale graphs, which are presented in Figures 2.

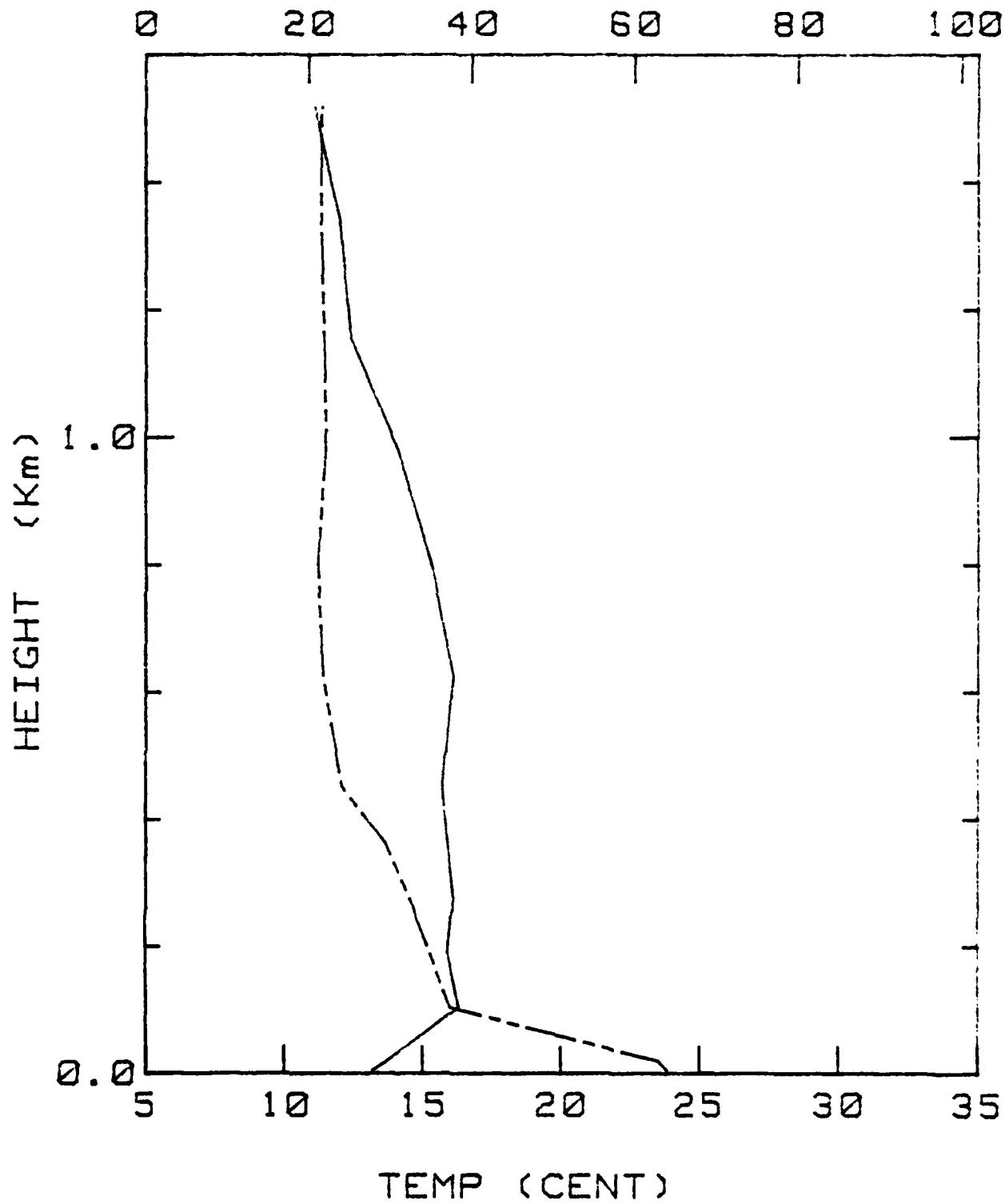
There are two apparent sources of error in these radiosonde results. The lowest height reading, which is obtained at the ship, is subject to ships influence and should not be used. Thus, it is not possible to use the radiosonde to determine properties of the surface layer. The radiosonde humidity system was not capable of measuring a relative humidity below 20%. This is especially apparent in Figure 2i.

Figure 2a
REL HUMIDITY (%)



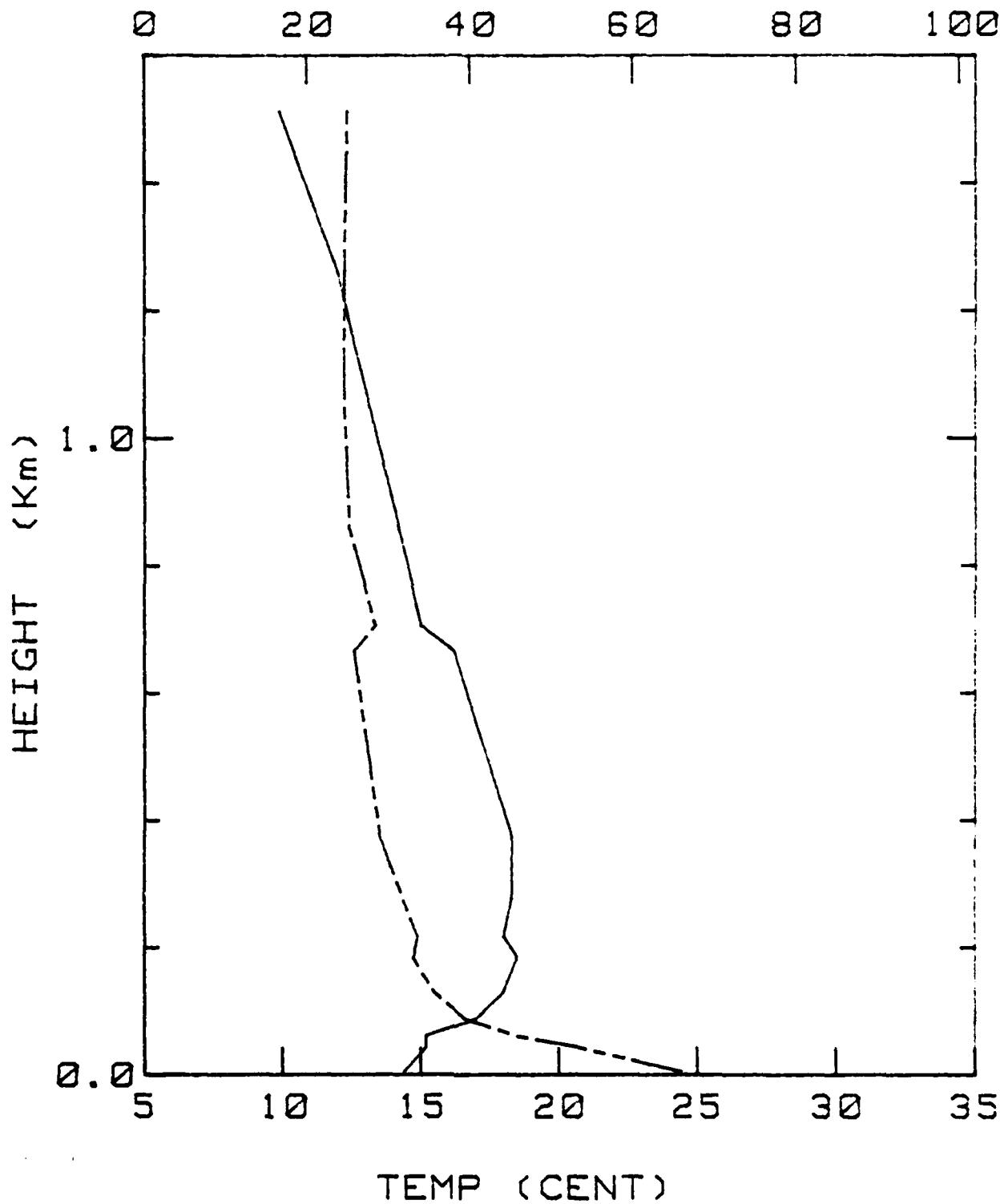
BLM-II 05 JAN 81 1953

Figure 2b
REL HUMIDITY (%)



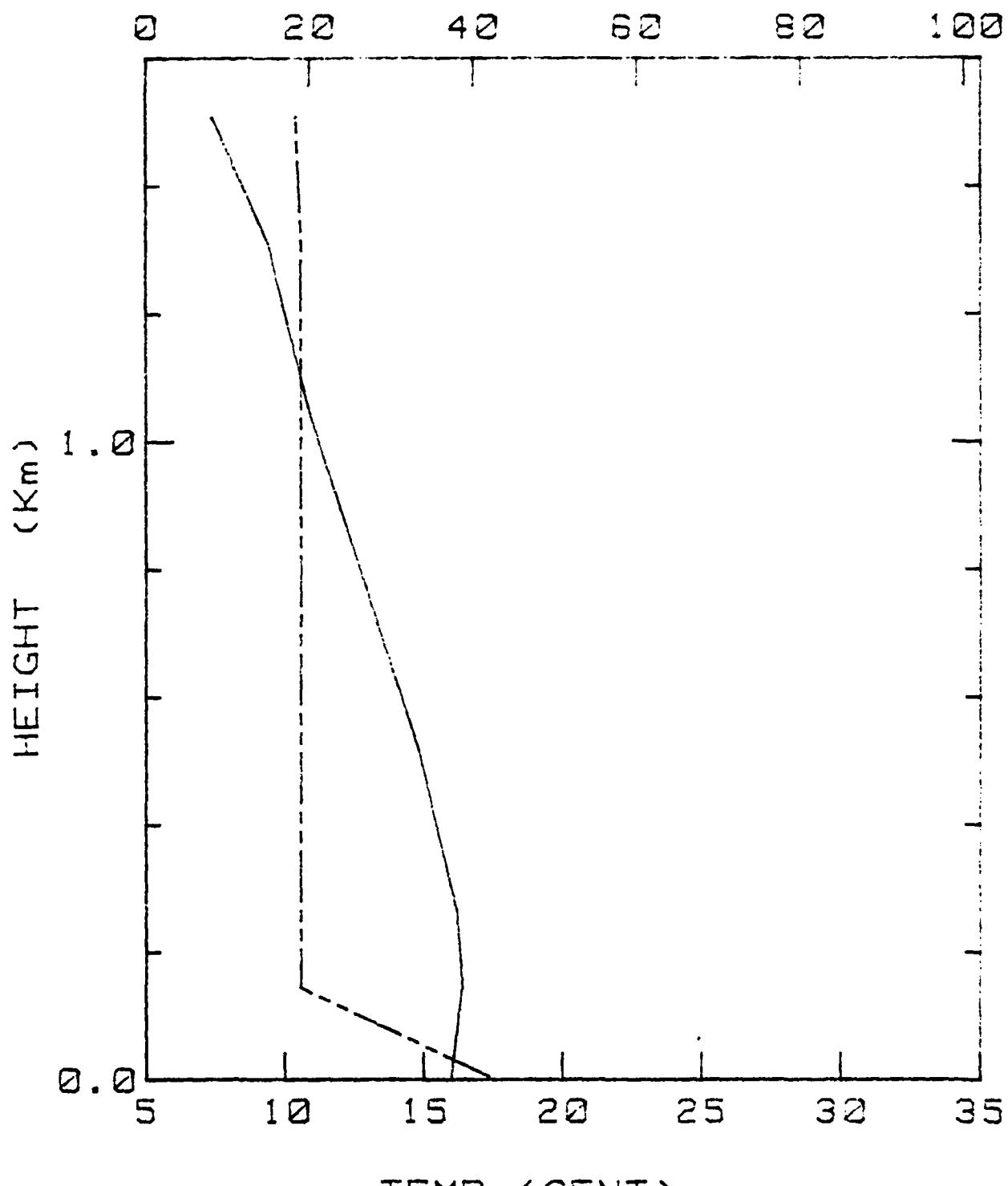
BLM-II 06 JAN 81 740

Figure 2c
REL HUMIDITY (%)



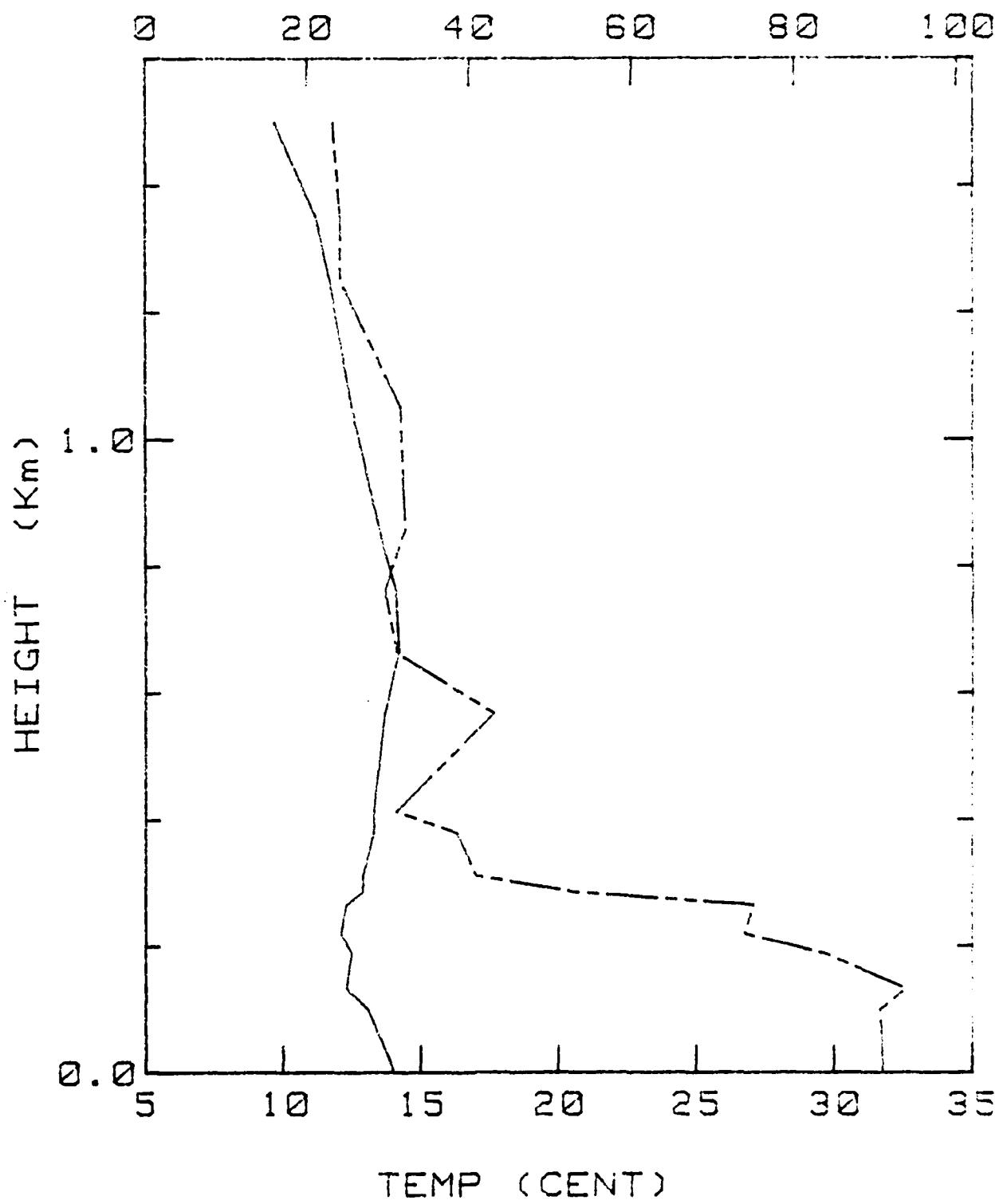
BLM-II 06 JAN 81 1905

Figure 2d
REL HUMIDITY (%)



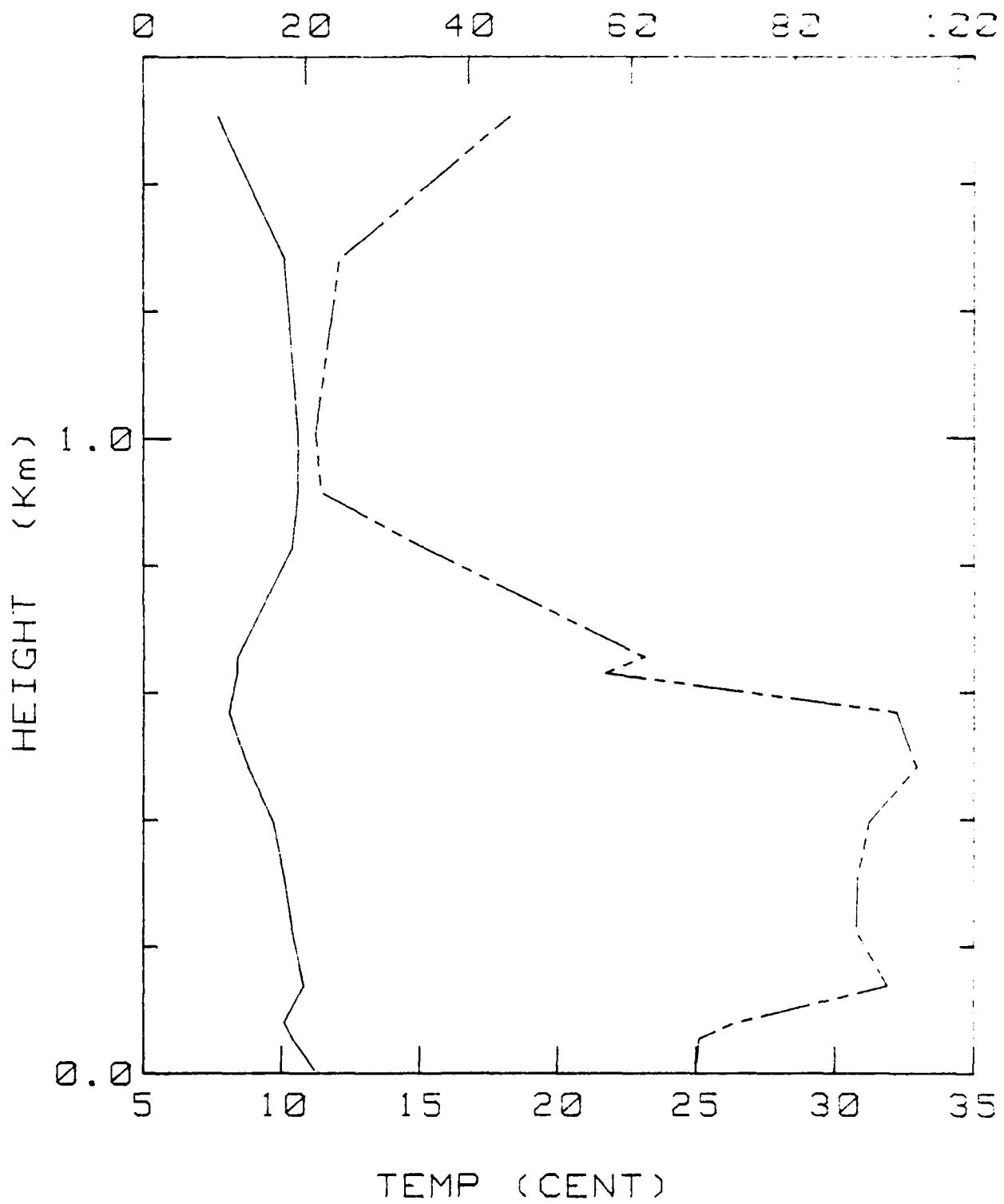
BLM-II 07 JAN 81 800

Figure 2e
REL HUMIDITY (%)



BLM-II 07 JAN 81 1850

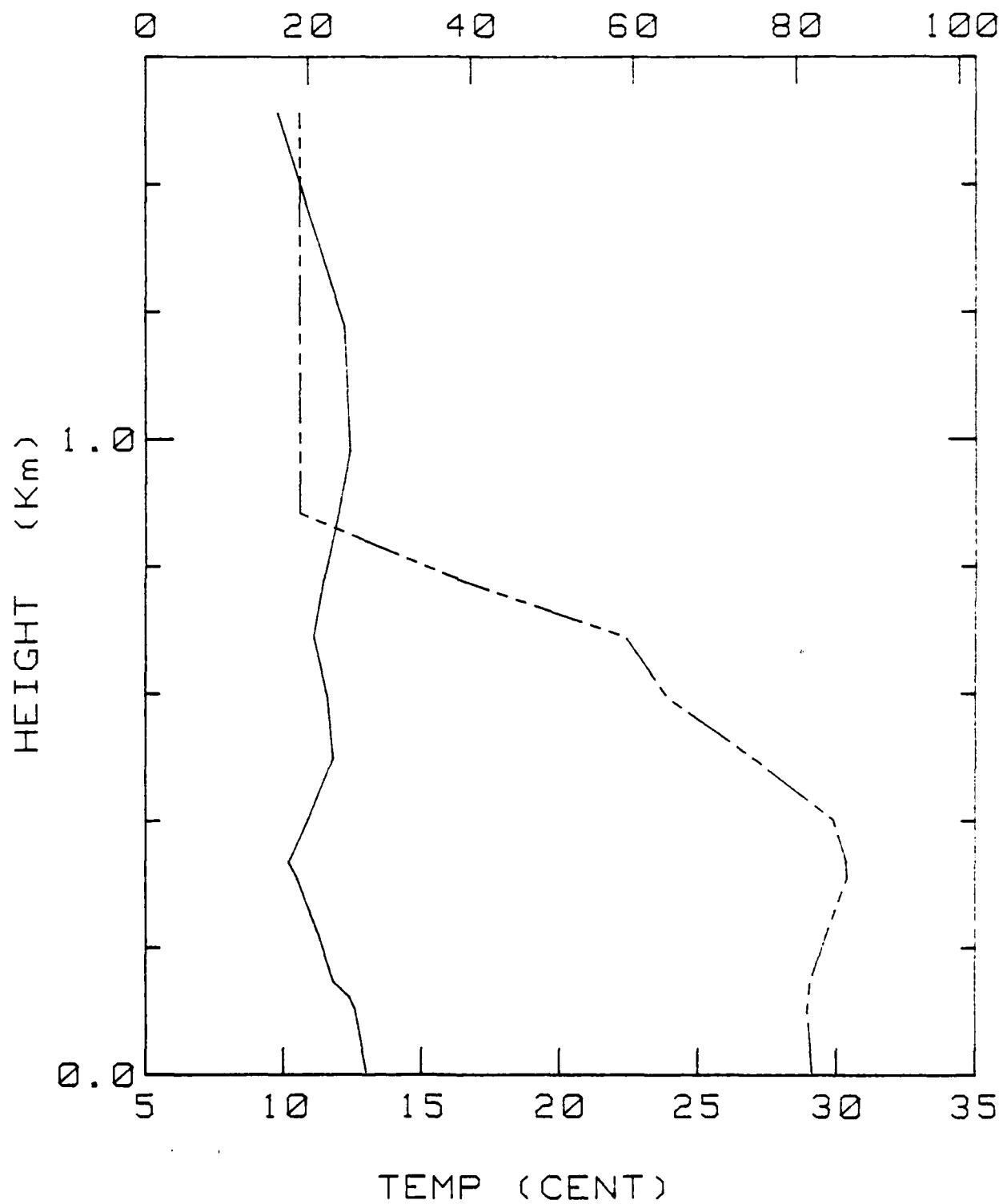
Figure 2f
REL HUMIDITY (%)



BLM-II 08 JAN 81 815

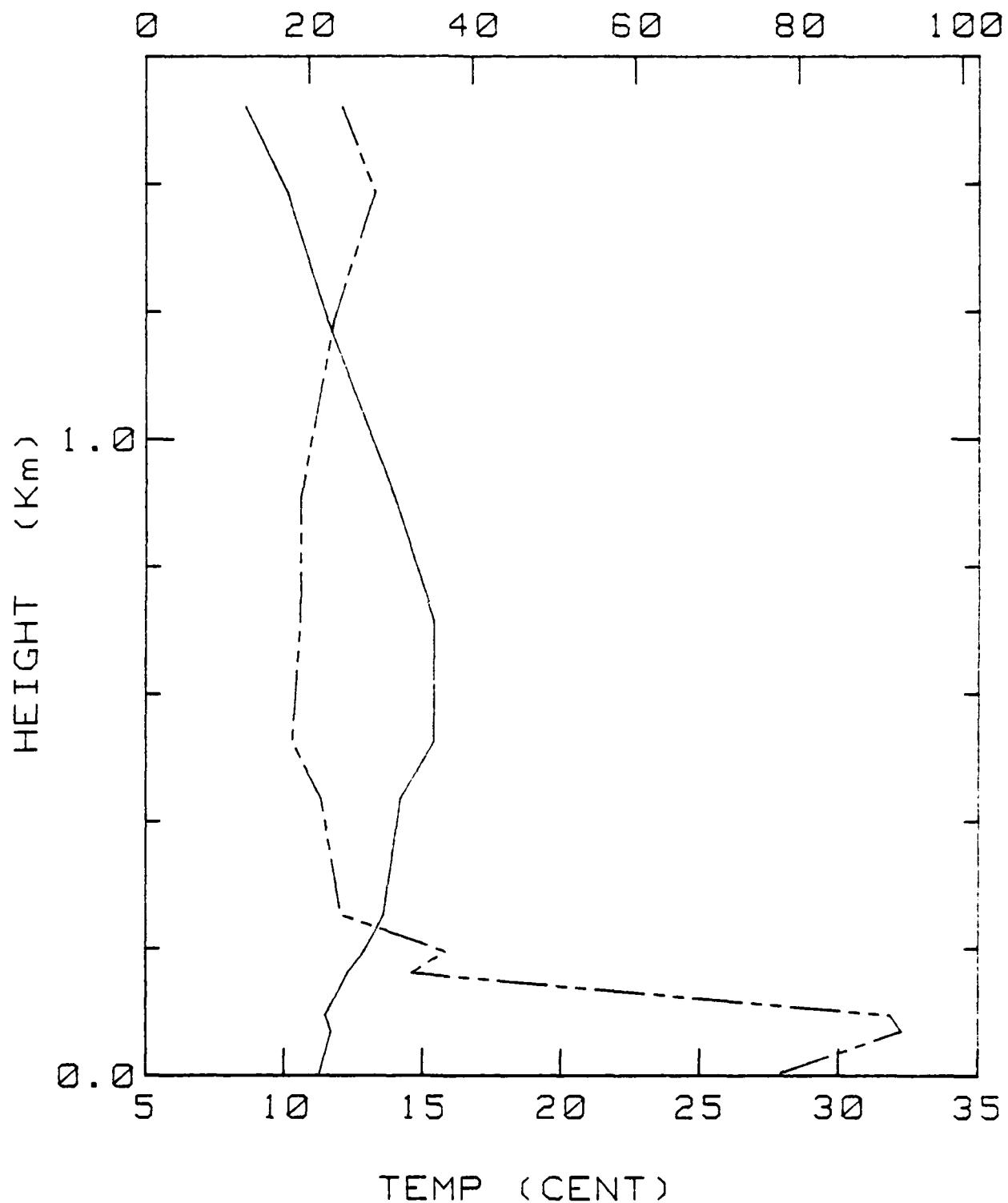
Figure 2g

REL HUMIDITY (%)



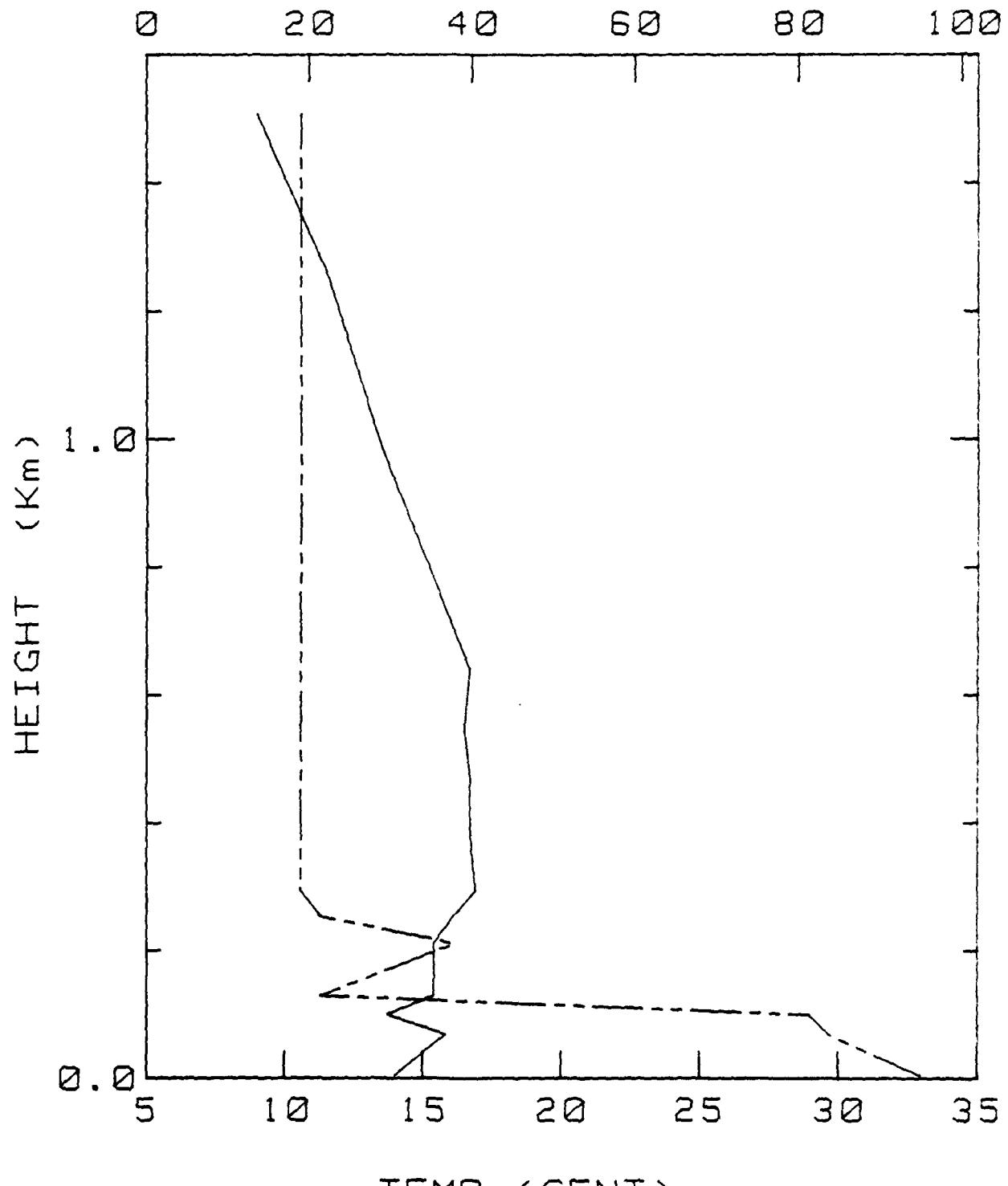
BLM-II 08 TAN 81 1915

Figure 2h
REL HUMIDITY (%)



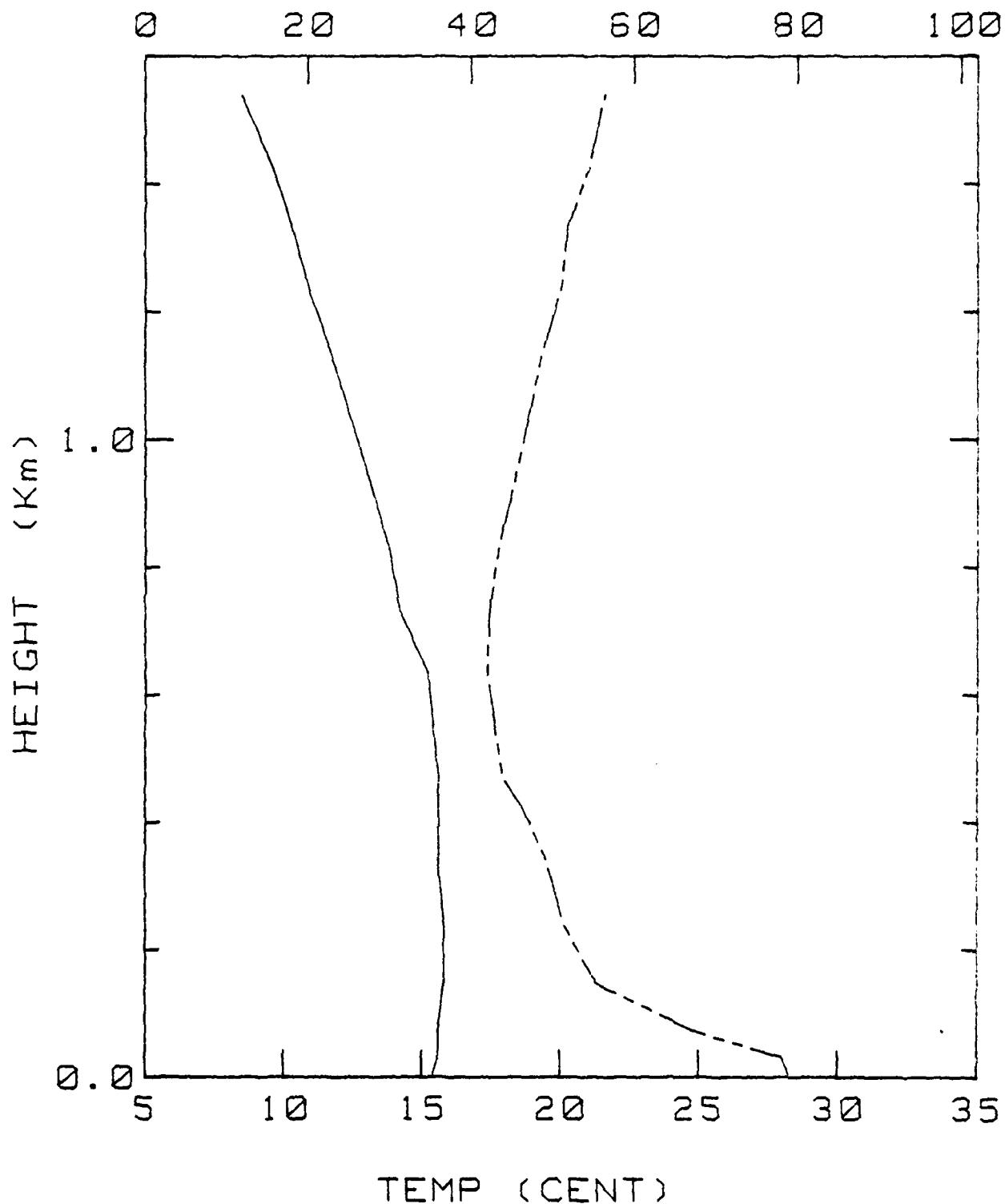
BLM-II 09-JAN 81 810

Figure 2i
REL HUMIDITY (%)



BLM-II 09 JAN 81 1800

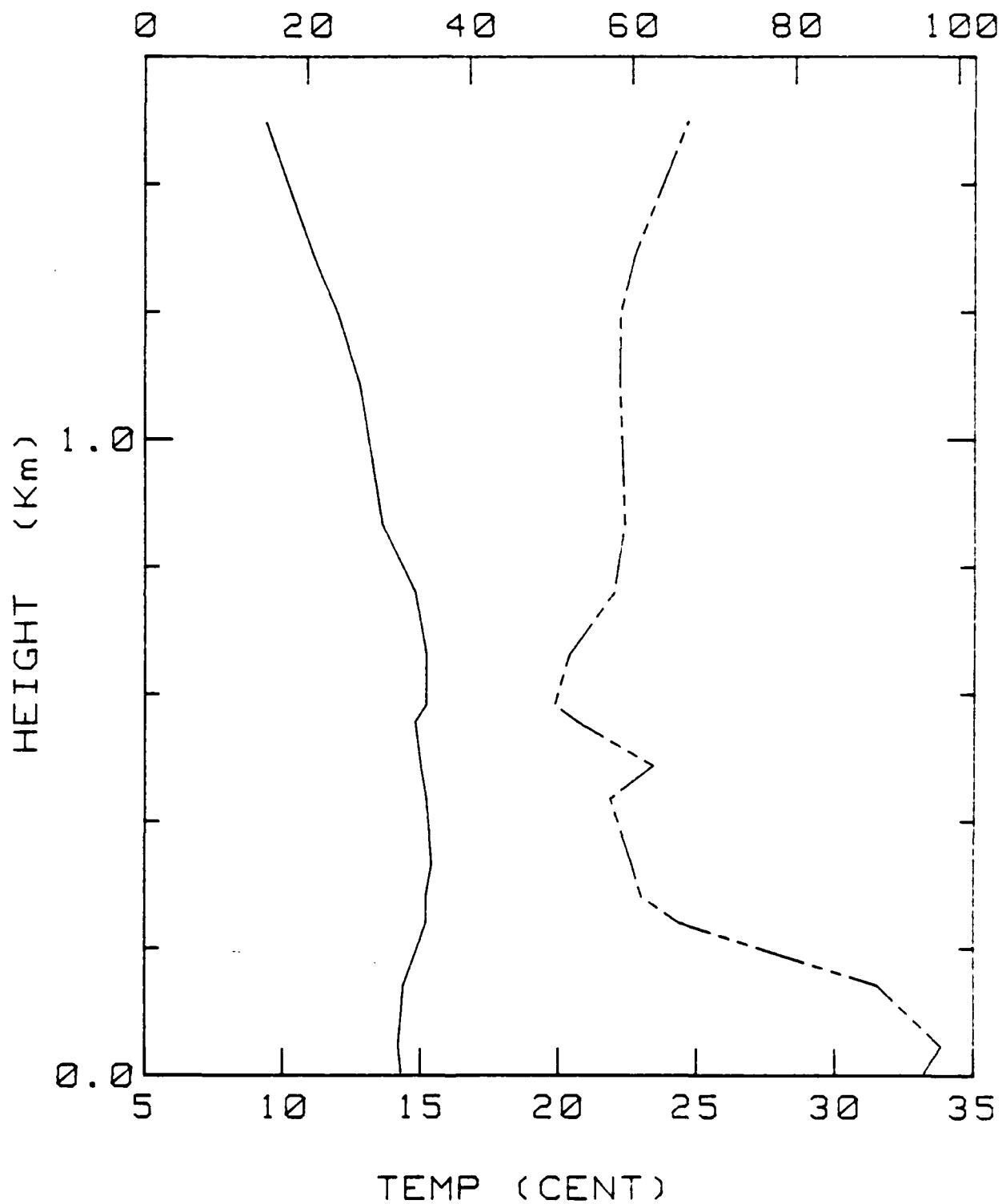
Figure 2j
REL HUMIDITY (%)



BLM-II 15 JAN 81 900

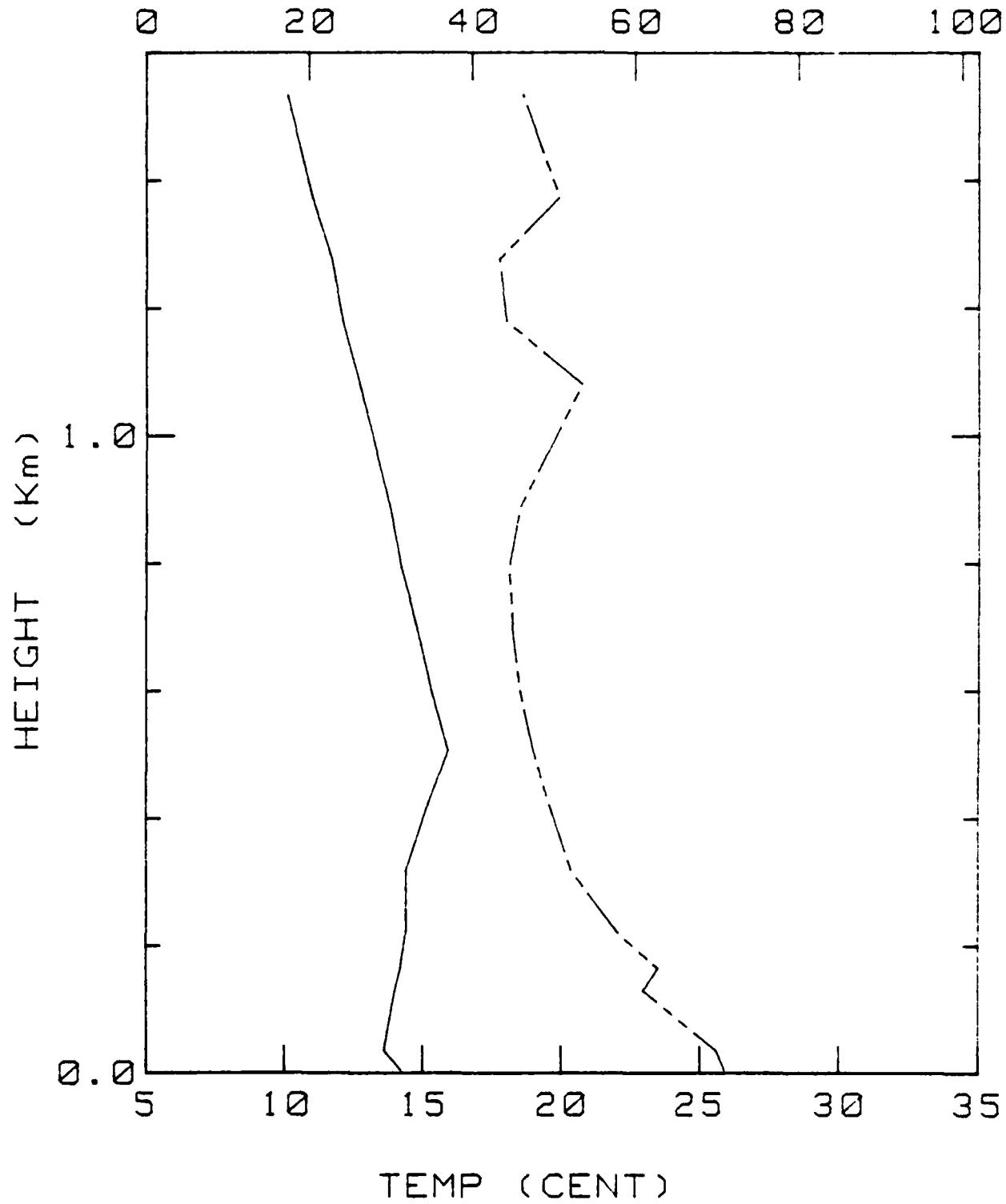
Figure 2k

REL HUMIDITY (%)



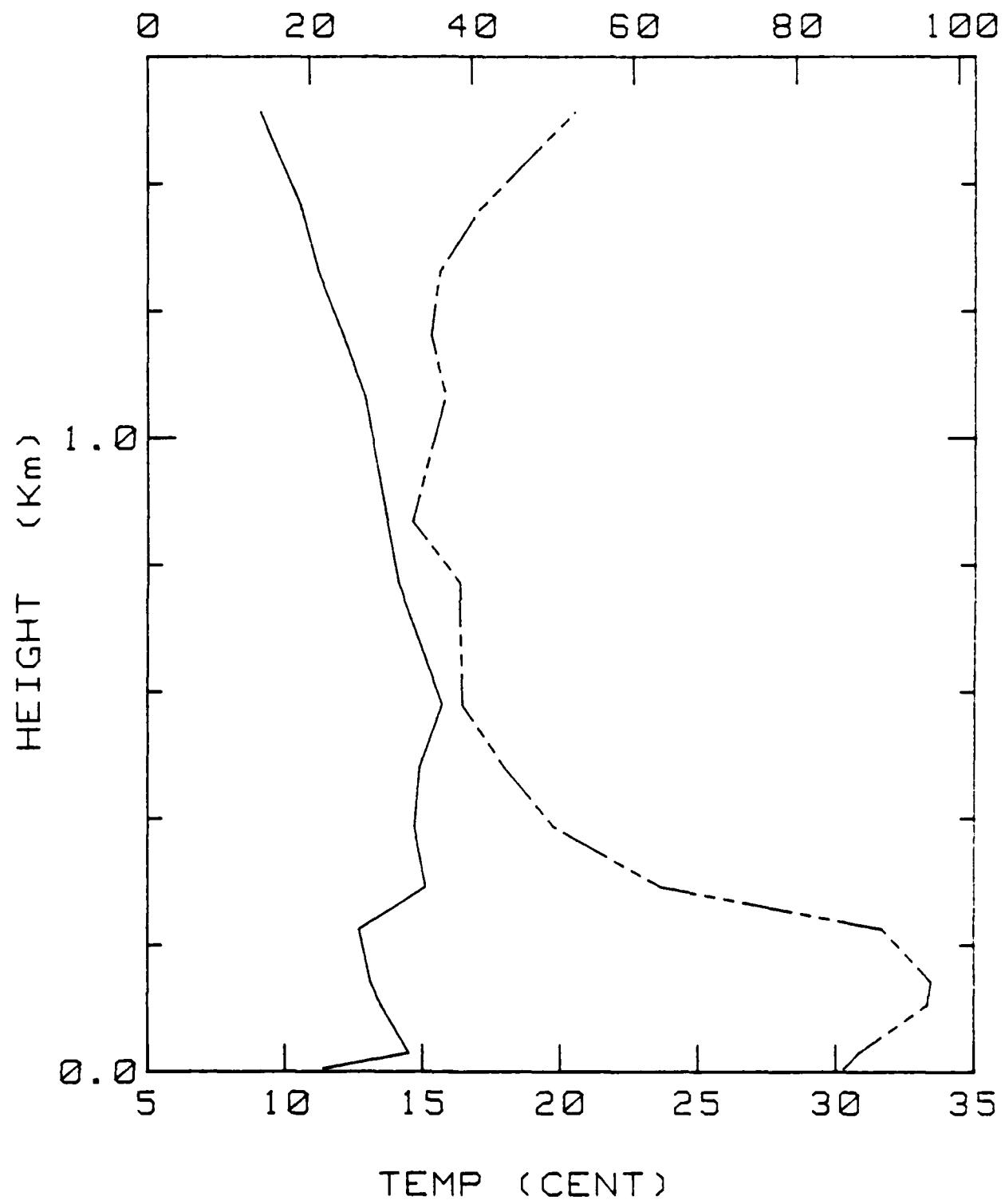
BLM-II 13 JAN 81 1930

Figure 21
REL HUMIDITY (%)



BLM-II 14 JAN 81 755

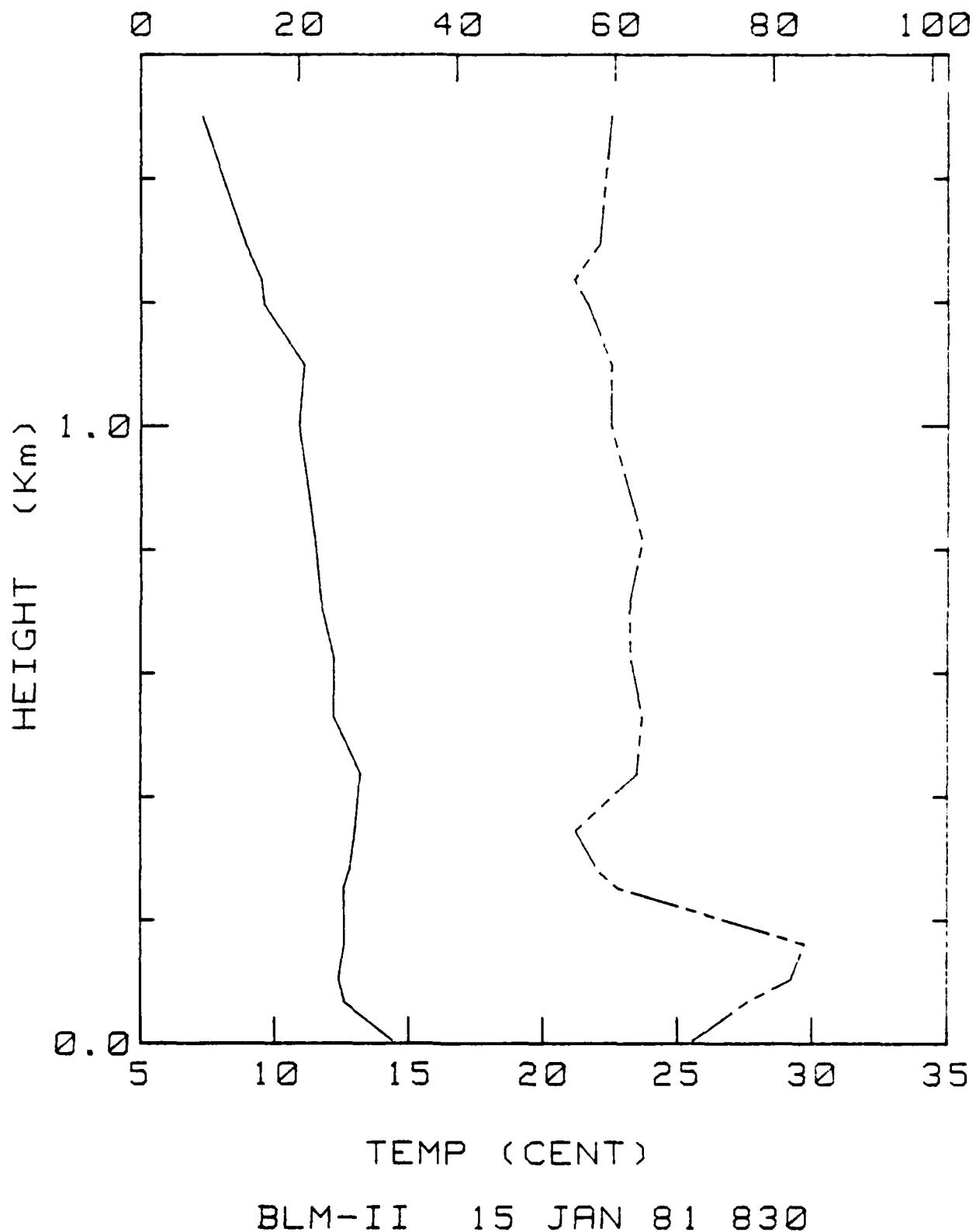
Figure 2m
REL HUMIDITY (%)



BLM-II 14 JAN 81 1920

Figure 2n

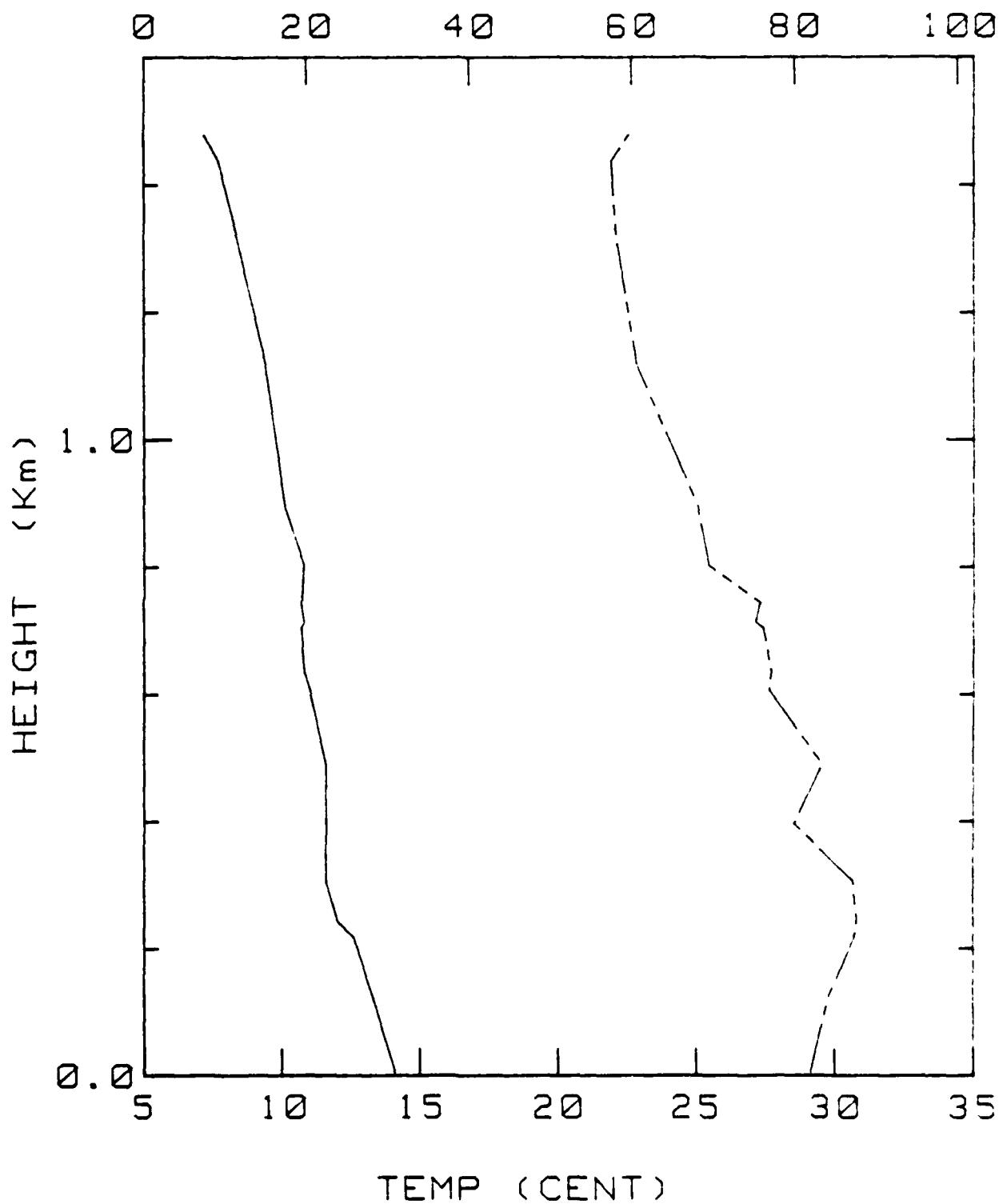
REL HUMIDITY (%)



BLM-II 15 JAN 81 830

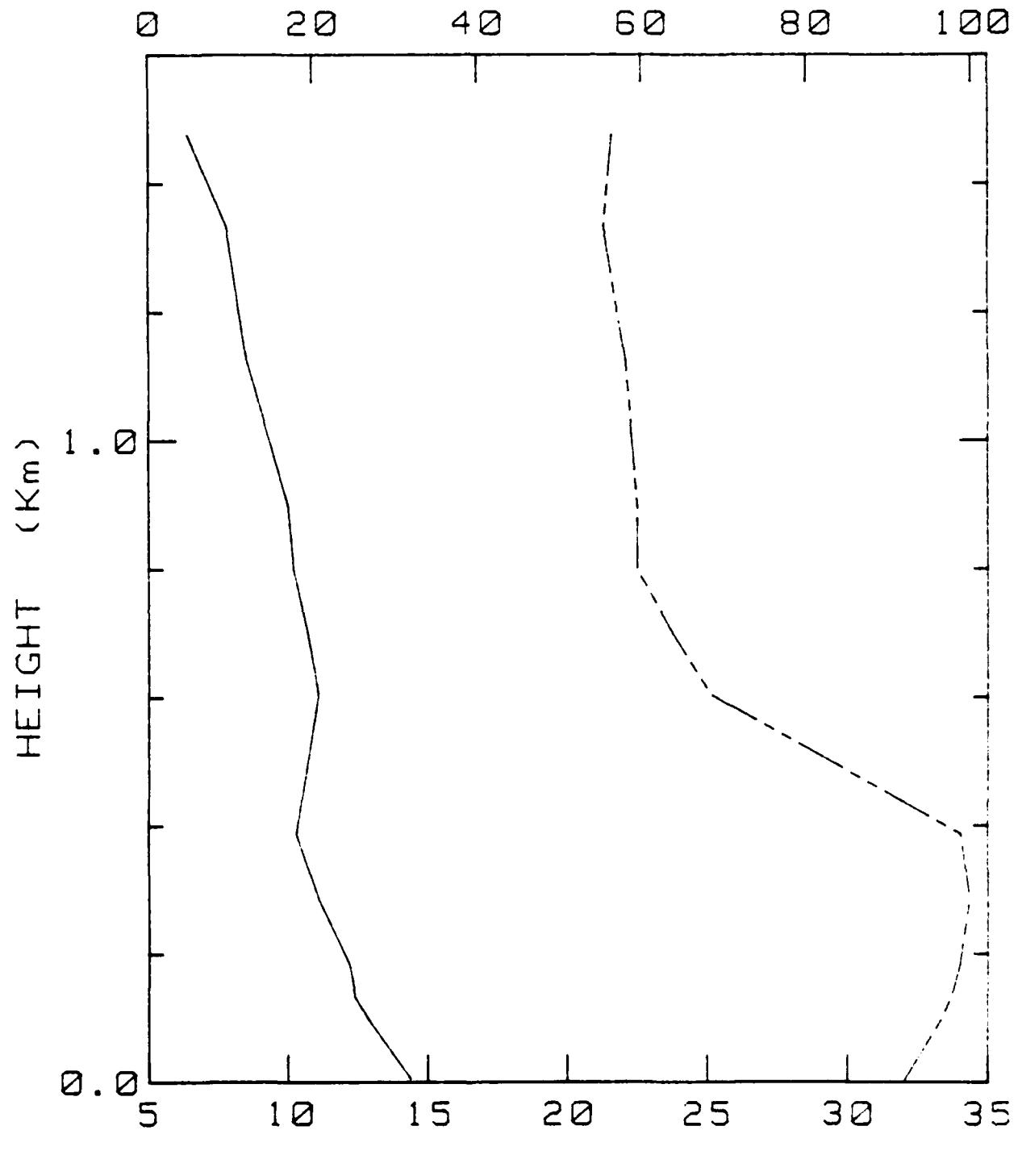
Figure 2o

REL HUMIDITY (%)



BLM-II 15 JAN 81 1950

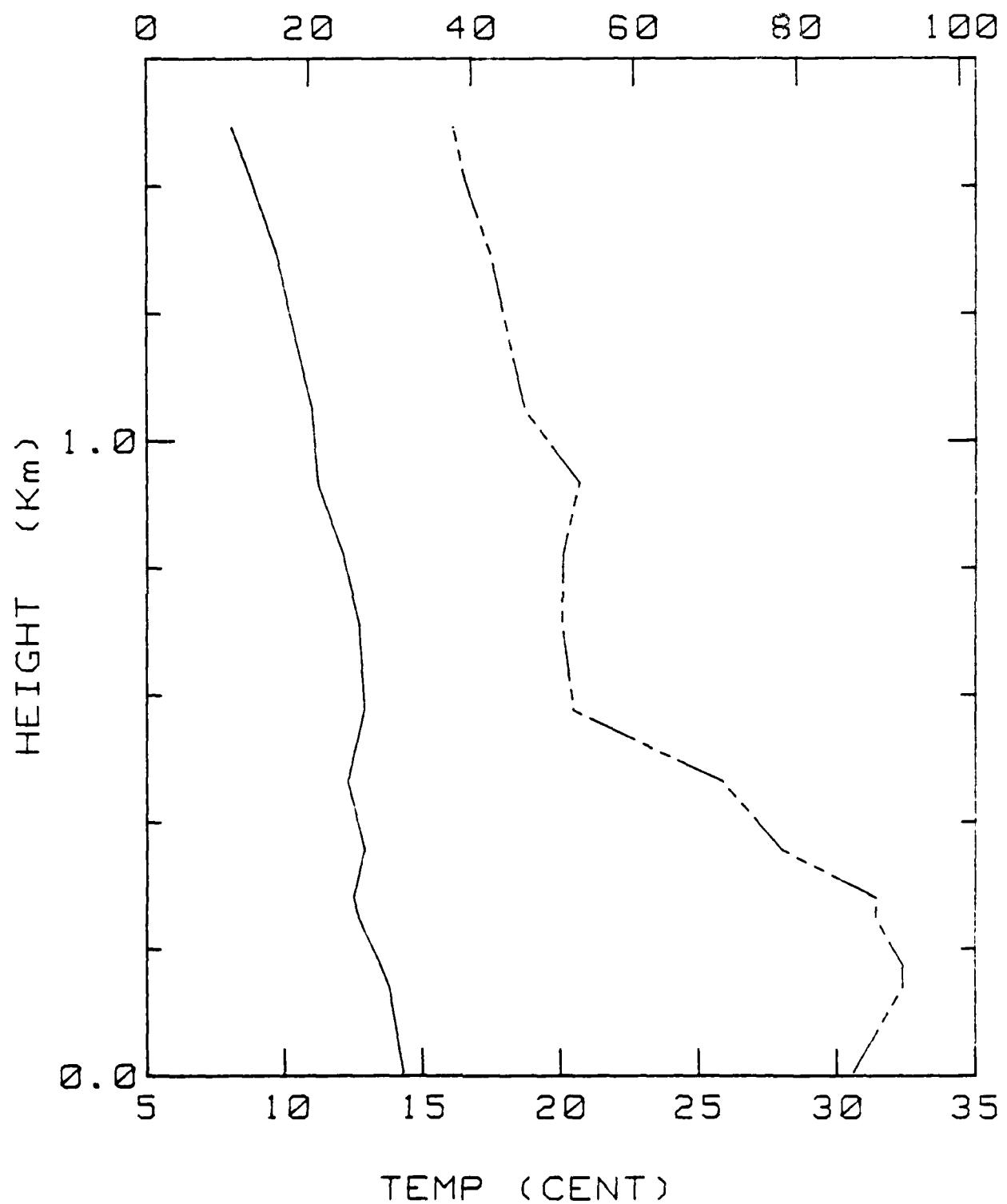
Figure 2p
REL HUMIDITY (%)



BLM-II 16 JAN 81 820

Figure 2q

REL HUMIDITY (%)



BLM-II 16 JAN 81 1935

VII. Acoustic Sounder Results

The acoustic sounder was operated continuously throughout the cruise and Figures 3 are photographs of the strip chart output. As can be seen there was very seldom a well defined return that would allow one to easily determine the boundary layer depth. In Table 5 we list the heights of detectable acoustic returns. In many cases the returns were so weak that one is not certain if they indicate the height of the base of the inversion. Also listed in the table are the heights of the base and top of the temperature inversion as determined from the radiosondes. These are designated with an R in the table. The radiosonde determined heights are listed as an aid since it is very difficult to determine the boundary layer depth from sounder data alone for these cases.

Figure 3a

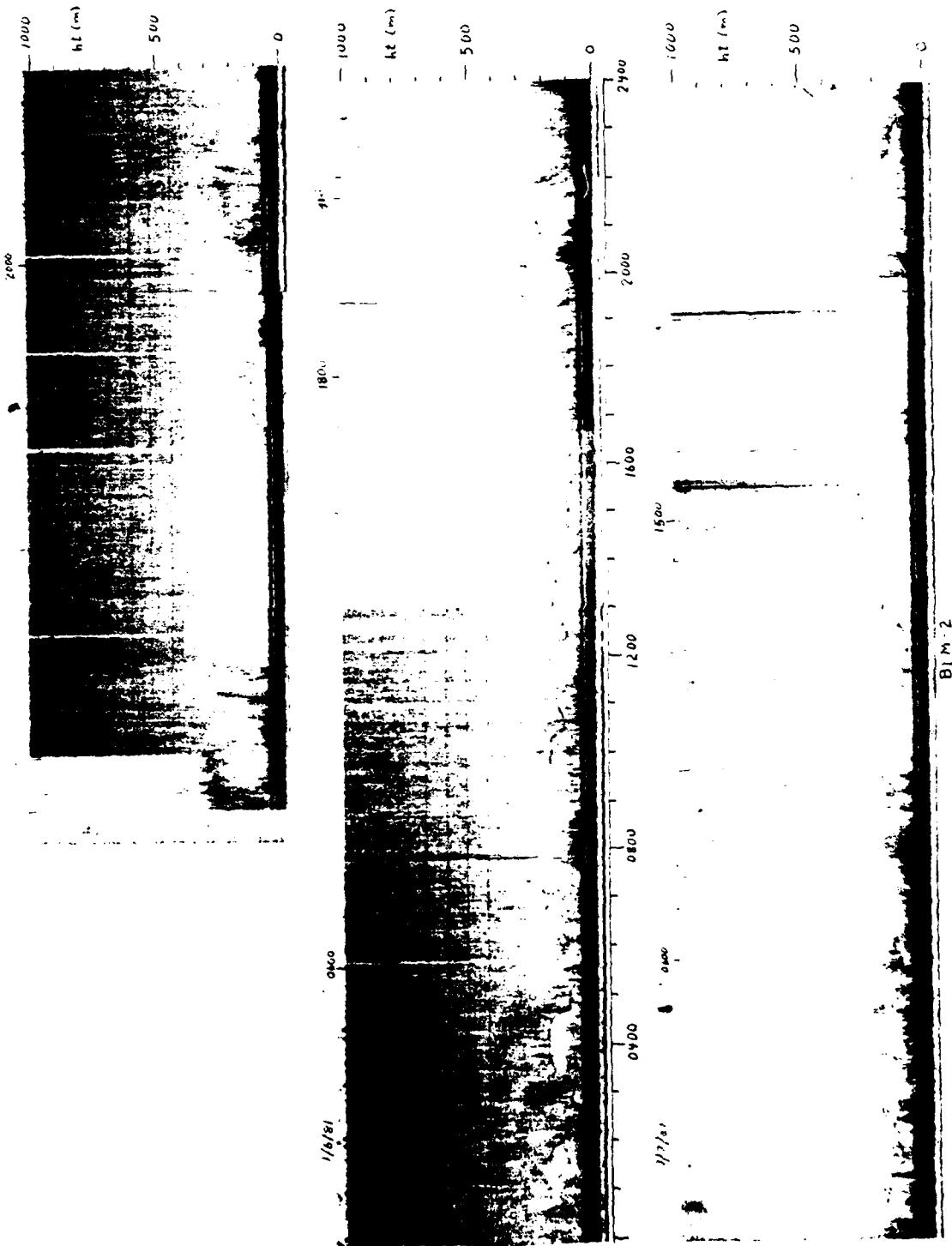


Figure 3b



Figure 3c



Table 5. Heights of acoustic echo return from the acoustic sounder. Also listed, and designated with an R, are the heights of the base and top of the temperature inversion as determined from the radiosondes.

| DATE | TIME | Z(m) | DATE | TIME | Z(m) |
|------|------|------------------|------|------|-------------------|
| 1/6 | 1230 | 120 | 1/8 | 1936 | R 320-600 |
| | 1300 | 140 | | 2000 | 330 |
| | 1330 | 140 | | 2100 | 320 |
| | 1400 | 160 | | 2200 | 320 |
| | 1700 | 180 | | 2230 | 240 |
| | 1730 | 180 | | 2300 | 270 |
| | 1800 | 240 | | 2330 | 360 |
| | 1830 | 160 | | | |
| | 1900 | 300 | 1/9 | 0430 | 200 |
| | 1930 | 280 | | 0500 | 190 |
| | | R 0-200 | | 0530 | 200 |
| | 2000 | 300 | | 0600 | 200 |
| | 2030 | 200 | | 0630 | 160 |
| | 2100 | 200 | | 0730 | 250 |
| | | | | 0800 | 160 |
| | | | | 0830 | 200 |
| | | | | | R 0-200, 200-700 |
| | | | | 0900 | 160 |
| 1/7 | 0200 | 140 | | 1000 | 160 |
| | 0600 | 120 | | 1030 | 100 |
| | | R 0-150 | | 1100 | 100 |
| | 0900 | 120 | | 1130 | 100 |
| | 1100 | 80 | | 1200 | 120 |
| | 1130 | 80 | | 1230 | 140 |
| | 1200 | 80 | | 1430 | 100 |
| | 1230 | 100 | | 1530 | 260 |
| | 1300 | 200 | | 1600 | 360 |
| | 1500 | 250 | | 1630 | 140 |
| | 1530 | 260 | | 1700 | 300 |
| | 1600 | 200 | | 1730 | 340 |
| | 1730 | 160 | | 1800 | 260 |
| | | R 120-650 | | | R 90-160, 220-300 |
| | 1930 | 300 | | 1900 | 80 |
| | 2000 | 300 | | 1930 | 160 |
| | 2130 | 400 | | 2000 | 200 |
| | 2200 | 280 | | 2030 | 160 |
| | 2230 | 160 | | 2100 | 120 |
| | 2300 | 120 | | | |
| | 2330 | 340 | 1/13 | 0200 | 160 |
| | 2400 | 440 | | 0230 | 220 |
| | | | | 0300 | 260 |
| | | | | 0330 | 250 |
| 1/8 | 0030 | 520 | | 0400 | 260 |
| | 0100 | 500 | | 0430 | 240 |
| | 0130 | 540 | | 0500 | 220 |
| | 0200 | 100 | | 0800 | 180 |
| | 0230 | 140 | | 0924 | 500 |
| | 0300 | 80 | | | R 0-170 weak |
| | 0330 | 100 | | 1800 | 100 |
| | 0400 | 100 | | 1830 | 130 |
| | 0530 | 260 | | 1900 | 120 |
| | 0830 | 180 | | 1930 | 100 |
| | 0845 | R70-160, 560-900 | | 2000 | 140 |
| | | | | | R 150-350 |

| DATE | TIME | Z(m) | | DATE | TIME | Z(m) | |
|------|------------------|----------|-----|------|------|-----------|-----|
| 1/13 | 2030 | 160 | | 1/15 | 1200 | 120 | |
| | 2100 | 200 | | | 1230 | 160 | |
| | 2130 | 180 | | | 1300 | 200 | |
| | 2330 | 180 | | | 1530 | 100 | |
| 1/14 | 0130 | 100 | | | 1600 | 350 | |
| | 0200 | 180 | | | 1630 | 260 | |
| | 0230 | 180 | | | 1700 | 150 | |
| | 0300 | 160 | | | 2018 | R Nore | |
| | 0400 | 80 | | 1/16 | 0845 | R 400-620 | |
| | 0500 | 100 | | | 1000 | 550 | |
| | 0630 | 160 | | | 1130 | 400 | |
| | 0823 | R 30-420 | | | 1330 | 360 | |
| | 1000 | 200 | | | 2005 | R 480-700 | |
| | 1100 | 170 | | | 2200 | 220 | |
| | 1130 | 160 | | | 2230 | 160 | 260 |
| | 1200 | 100 | | | 2300 | 100 | |
| | 1230 | 80 | | | 2330 | 180 | |
| | 1300 | 100 | | | | | |
| | 1400 | 180 | | | | | |
| | 1500 | 200 | | | | | |
| | 1600 | 160 | | | | | |
| | 1700 | 80 | | | | | |
| | 1730 | 80 | | | | | |
| | 1800 | 160 | | | | | |
| | 1830 | 120 | | | | | |
| | 1900 | 160 | | | | | |
| | R 0-150, 230-480 | | | | | | |
| | 2000 | 200 | | | | | |
| | 2030 | 230 | | | | | |
| | 2100 | 220 | | | | | |
| | 2130 | 160 | 240 | | | | |
| | 2200 | 200 | 300 | | | | |
| | 2230 | 210 | 300 | | | | |
| | 2300 | 300 | | | | | |
| | 2330 | 190 | | | | | |
| 1/15 | 0100 | 350 | | | | | |
| | 0130 | 260 | | | | | |
| | 0200 | 180 | | | | | |
| | 0230 | 160 | | | | | |
| | 0300 | 100 | 300 | | | | |
| | 0330 | 300 | | | | | |
| | 0400 | 420 | | | | | |
| | 0500 | 420 | | | | | |
| | 0530 | 360 | | | | | |
| | 0600 | 400 | | | | | |
| | 0700 | 460 | | | | | |
| | 0730 | 450 | | | | | |
| | 0800 | 380 | | | | | |
| | 0830 | 340 | | | | | |
| | 0930 | 140 | | | | | |

VIII. Meteorological Data

Table 6 presents the basic meteorological data and calculated parameters. Only data taken during the tracer gas release periods are included. Wind speed, relative humidity, and air temperature values are those measured at the upper level (20.5 m). All calculated parameters were determined using the bulk aerodynamic method.

The boundary layer mixing rate and mixing height depend on the boundary layer depth, Z_i . We have already mentioned the difficulty in determining the depth for these data. We have used a combination of the radiosonde data and the acoustic sounder data to find Z_i , and, unless a radiosonde was launched close to the time of interest, the value used was only an estimate. Thus, most of the mixing rate values, w_* , and the mixing times, t , are suspect.

Table 6. Meteorological Data

BLM II-81
Release #1

| Date/Time | U (m/sec) | RH (%) | T (C) | WS (C) | Zi (m) | U* (m/sec) | T* (m/sec) | 10^3 w* (m/sec) | r/L | w* (m/sec) | t (min) |
|------------|--------------|-----------|----------|-----------|-----------|---------------|---------------|--------------------|-----------|---------------|------------|
| 01/06 1355 | 5.6 | 66 | 16.7 | 15.6 | 160 | 0.175 | -0.039 | -18.6 | 7.40E-02 | 0.3 | 8.0 |
| 01/06 1425 | 5.3 | 66 | 16.8 | 15.6 | 160 | 0.163 | -0.041 | -21.5 | 9.79E-02 | 0.3 | 6.0 |
| 01/06 1455 | 4.3 | 60 | 17.3 | 15.7 | 160 | 0.118 | -0.051 | -30.6 | 2.65E-01 | 0.3 | 8.3 |
| 01/06 1542 | 2.6 | 64 | 17.1 | 15.8 | 160 | 0.057 | -0.036 | -19.6 | 7.39E-01 | 0.2 | 11.9 |
| 01/06 1612 | 5.4 | 53 | 17.7 | 15.7 | 170 | 0.157 | -0.068 | -42.2 | 2.05E-01 | 0.4 | 7.2 |
| 01/06 1642 | 4.7 | 58 | 17.3 | 15.6 | 170 | 0.132 | -0.056 | -34.1 | 2.35E-01 | 0.4 | 8.1 |
| 01/06 1712 | 5.3 | 61 | 17.1 | 15.6 | 180 | 0.159 | -0.051 | -29.4 | 1.40E-01 | 0.4 | 8.2 |
| 01/06 1742 | 4.5 | 61 | 17.2 | 15.6 | 180 | 0.128 | -0.050 | -30.5 | 2.24E-01 | 0.3 | 8.8 |
| 01/06 1812 | 4.8 | 52 | 18.0 | 15.5 | 160 | 0.137 | -0.064 | -42.2 | 2.72E-01 | 0.4 | 7.4 |
| 01/06 1842 | 3.7 | 66 | 16.7 | 15.5 | 160 | 0.101 | -0.041 | -22.5 | 2.65E-01 | 0.3 | 9.5 |
| 01/06 1912 | 2.7 | 69 | 16.5 | 15.5 | 140 | 0.066 | -0.032 | -16.9 | 4.74E-01 | 0.2 | 10.8 |
| 01/06 1942 | 1.6 | 55 | 16.0 | 15.4 | 140 | 0.053 | -0.015 | 18.7 | -7.62E-01 | 0.2 | 14.9 |

BLM 11-81
Release #2

| Date/Take | U (m/sec) | RH (%) | T (C) | T _S (C) | z _i (m) | U* (m/sec) | T* (C) | 10 ⁴ 3*Q _O (m/sec) | z/L | w* (m/sec) | t (min) |
|------------|--------------|-----------|----------|-----------------------|-----------------------|---------------|-----------|---|-----------|---------------|------------|
| 01/09 1149 | 3.7 | 79 | 14.0 | 15.4 | 80 | 0.122 | 0.046 | 68.9 | -5.49E-01 | 0.2 | 5.4 |
| 01/09 1221 | 4.1 | 84 | 14.0 | 15.3 | 180 | 0.134 | 0.042 | 59.9 | -3.94E-01 | 0.3 | 9.2 |
| 01/09 1309 | 4.1 | 85 | 14.1 | 15.3 | 200 | 0.137 | 0.037 | 54.2 | -3.42E-01 | 0.3 | 10.2 |
| 01/09 1339 | 4.6 | 87 | 14.2 | 15.3 | 240 | 0.154 | 0.036 | 51.0 | -2.53E-01 | 0.4 | 11.2 |
| 01/09 1409 | 4.7 | 88 | 14.2 | 15.3 | 240 | 0.156 | 0.033 | 47.1 | -2.30E-01 | 0.3 | 11.5 |
| 01/09 1439 | 4.6 | 87 | 14.4 | 15.3 | 250 | 0.153 | 0.028 | 42.0 | -2.13E-01 | 0.3 | 12.6 |
| 01/09 1509 | 5.0 | 84 | 14.6 | 15.3 | 260 | 0.166 | 0.019 | 34.0 | -1.45E-01 | 0.3 | 14.2 |
| 01/09 1539 | 4.2 | 85 | 14.8 | 15.4 | 260 | 0.136 | 0.014 | 28.2 | -1.79E-01 | 0.3 | 15.7 |
| 01/09 1609 | 3.2 | 85 | 15.0 | 15.3 | 200 | 0.101 | 0.008 | 21.0 | -2.43E-01 | 0.2 | 16.9 |
| 01/09 1619 | 2.9 | 83 | 15.2 | 15.3 | 180 | 0.091 | 0.001 | 15.0 | -2.10E-01 | 0.1 | 32.2 |
| 01/09 1709 | 4.1 | 87 | 15.1 | 15.3 | 160 | 0.131 | 0.004 | 15.7 | -1.07E-01 | 0.1 | 18.3 |
| 01/09 1739 | 4.7 | 88 | 15.0 | 15.3 | 120 | 0.154 | 0.008 | 18.6 | -9.16E-02 | 0.2 | 11.9 |
| 01/09 1809 | 5.2 | 85 | 15.0 | 15.3 | 100 | 0.170 | 0.005 | 17.8 | -7.25E-02 | 0.1 | 11.5 |

BLI III-81
Release #3

| Date/Time | g (m/sec) | RJ (s) | T (C) | T _s (C) | Zi (m) | U* (m/sec) | r* (C) | 10 ⁴ J* ₂₀ (m/sec ²) | z/L | w* (m/sec) | t (min) |
|------------|--------------|-----------|----------|-----------------------|-----------|---------------|-----------|---|-----------|---------------|------------|
| 01/13 0852 | 3.9 | 70 | 14.4 | 15.0 | 180 | 0.129 | 0.021 | 44.1 | -3.14E-01 | 0.3 | 11.7 |
| 01/13 0948 | 3.0 | 79 | 15.1 | 15.0 | 100 | 0.090 | -0.007 | 7.5 | -1.06E-01 | 0.1 | 13.0 |
| 01/13 1049 | 3.3 | 67 | 16.0 | 15.2 | 100 | 0.096 | -0.024 | -6.2 | 8.59E-02 | 0.2 | 8.4 |
| 01/13 1119 | 4.5 | 78 | 15.5 | 15.2 | 100 | 0.141 | -0.014 | -0.2 | 2.68E-03 | 0.2 | 8.9 |
| 01/13 1239 | 4.9 | 73 | 16.0 | 15.3 | 100 | 0.152 | -0.024 | -9.0 | 4.79E-02 | 0.2 | 7.2 |
| 01/13 1369 | 5.4 | 77 | 15.9 | 15.4 | 100 | 0.172 | -0.022 | -8.2 | 3.42E-02 | 0.2 | 7.1 |
| 01/13 1339 | 5.3 | 71 | 16.3 | 15.4 | 100 | 0.167 | -0.030 | -14.3 | 6.49E-02 | 0.3 | 5.5 |
| 01/13 1409 | 6.1 | 61 | 17.0 | 15.4 | 100 | 0.194 | -0.046 | -27.5 | 8.83E-02 | 0.3 | 5.3 |
| 01/13 1439 | 5.5 | 64 | 16.9 | 15.5 | 100 | 0.171 | -0.045 | -26.6 | 1.10E-01 | 0.3 | 5.6 |
| 01/13 1503 | 5.6 | 71 | 16.5 | 15.5 | 100 | 0.176 | -0.036 | -20.5 | 8.02E-02 | 0.3 | 5.0 |
| 01/13 1521 | 5.1 | 81 | 16.1 | 15.4 | 100 | 0.157 | -0.027 | -16.4 | 8.07E-02 | 0.2 | 5.9 |
| 01/13 1559 | 5.4 | 83 | 15.9 | 15.3 | 130 | 0.169 | -0.023 | -13.2 | 5.58E-02 | 0.3 | 6.4 |
| 01/13 1629 | 4.0 | 87 | 15.7 | 15.4 | 130 | 0.120 | -0.015 | -6.8 | 5.71E-02 | 0.2 | 10.9 |
| 01/13 1659 | 4.3 | 83 | 15.8 | 15.4 | 130 | 0.132 | -0.014 | -4.7 | 3.32E-02 | 0.2 | 10.7 |
| 01/13 1729 | 4.4 | 83 | 15.7 | 15.4 | 130 | 0.137 | -0.013 | -2.2 | 1.52E-02 | 0.2 | 11.0 |

B.L.T. II-81
release #4

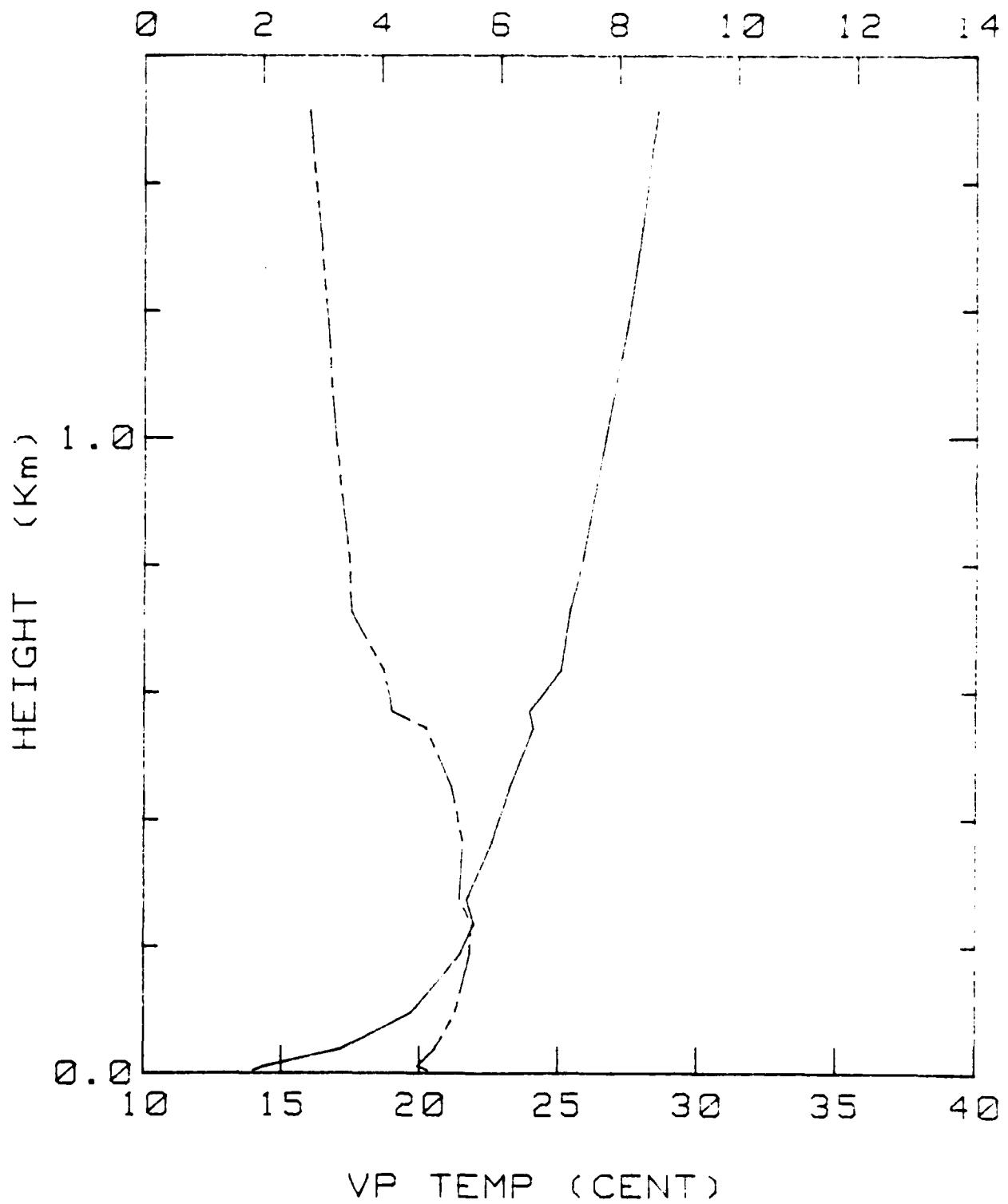
| Date/tire | U (m/sec) | R_H (\pm) | T (C) | T_{ξ} (C) | Z_i (m) | U^* (m/sec) | T^* (C) | $10^{4.3} \times \zeta_{CO}$ (m/secK) | Z/L | w^* (m/secC) | t (min) |
|------------|----------------|--------------------|------------|------------------|--------------|------------------|--------------|--|-----------|-------------------|--------------|
| 01/15 1441 | 3.3 | 86 | 14.8 | 15.7 | 150 | 0.106 | 0.026 | 40.2 | -4.23E-01 | 0.2 | 10.4 |
| 01/15 1500 | 4.6 | 84 | 14.8 | 15.7 | 200 | 0.160 | 0.026 | 41.1 | -1.90E-01 | 0.3 | 10.9 |
| 01/15 1552 | 4.0 | 84 | 15.1 | 15.6 | 100 | 0.128 | 0.013 | 26.2 | -1.87E-01 | 0.2 | 9.4 |
| 01/15 1622 | 5.3 | 85 | 14.9 | 15.6 | 360 | 0.176 | 0.021 | 34.6 | -1.32E-01 | 0.4 | 16.8 |
| 01/15 1652 | 6.2 | 85 | 14.8 | 15.6 | 260 | 0.210 | 0.022 | 35.6 | -9.56E-02 | 0.3 | 12.6 |
| 01/15 1722 | 5.9 | 85 | 14.8 | 15.5 | 120 | 0.200 | 0.021 | 34.9 | -1.02E-01 | 0.3 | 7.6 |

IX. Mixed Layer Parameters

It is very important in understanding transport and dispersion to determine whether the boundary layer is well mixed. We do this by examining the virtual potential temperature and water vapor mixing ratio. These parameters will be well mixed in the well mixed boundary layer and will, then, be constant with height. The two parameters have been determined from the radiosonde results and are shown in Figures 4a-q. Again note that the lowest point for each sounding is not reliable. These results can be easily used to determine if the boundary layer is well mixed.

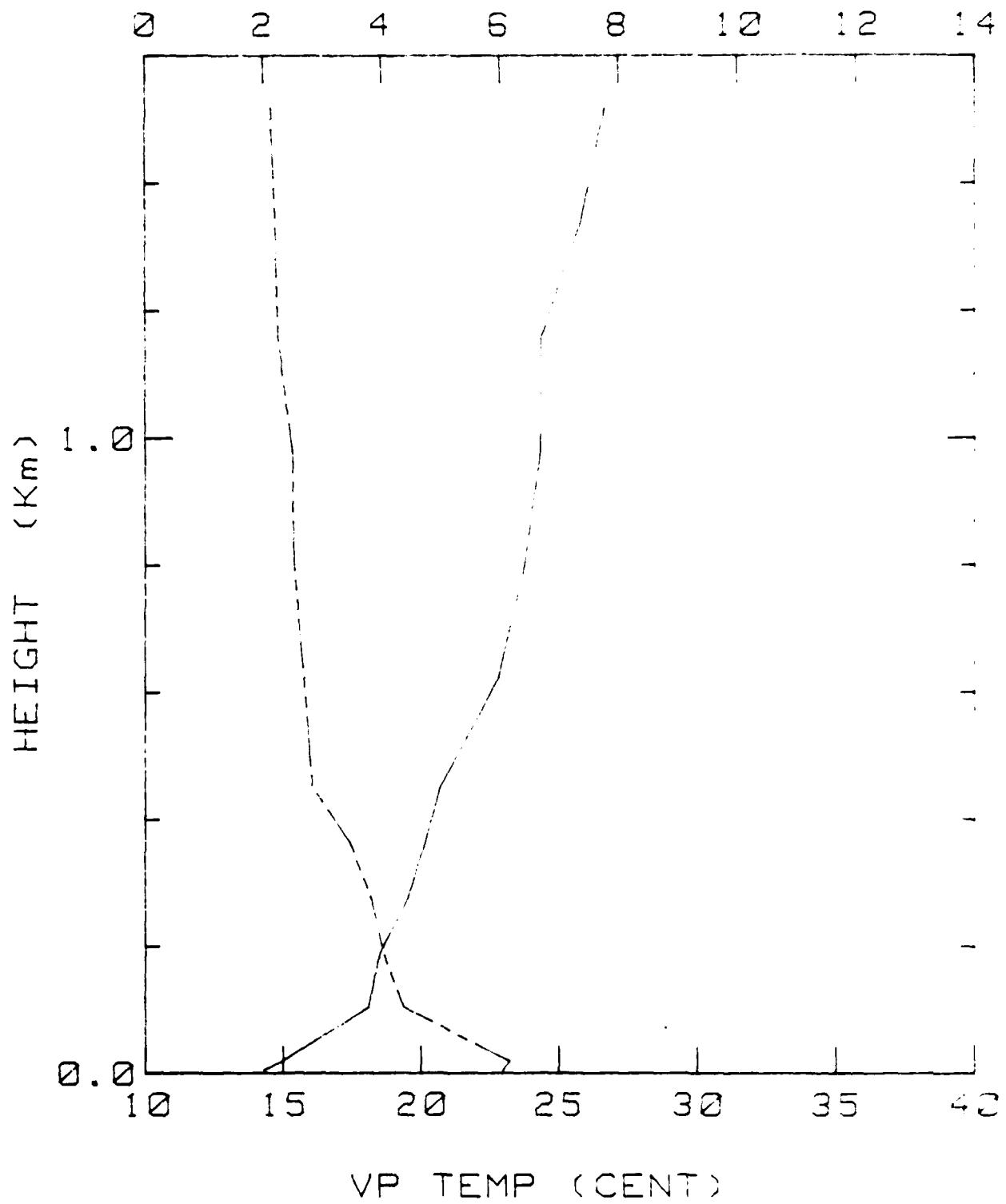
Figure 4a

MIX RATIO (G/KG)



BLM-II 05 JAN 81 1953

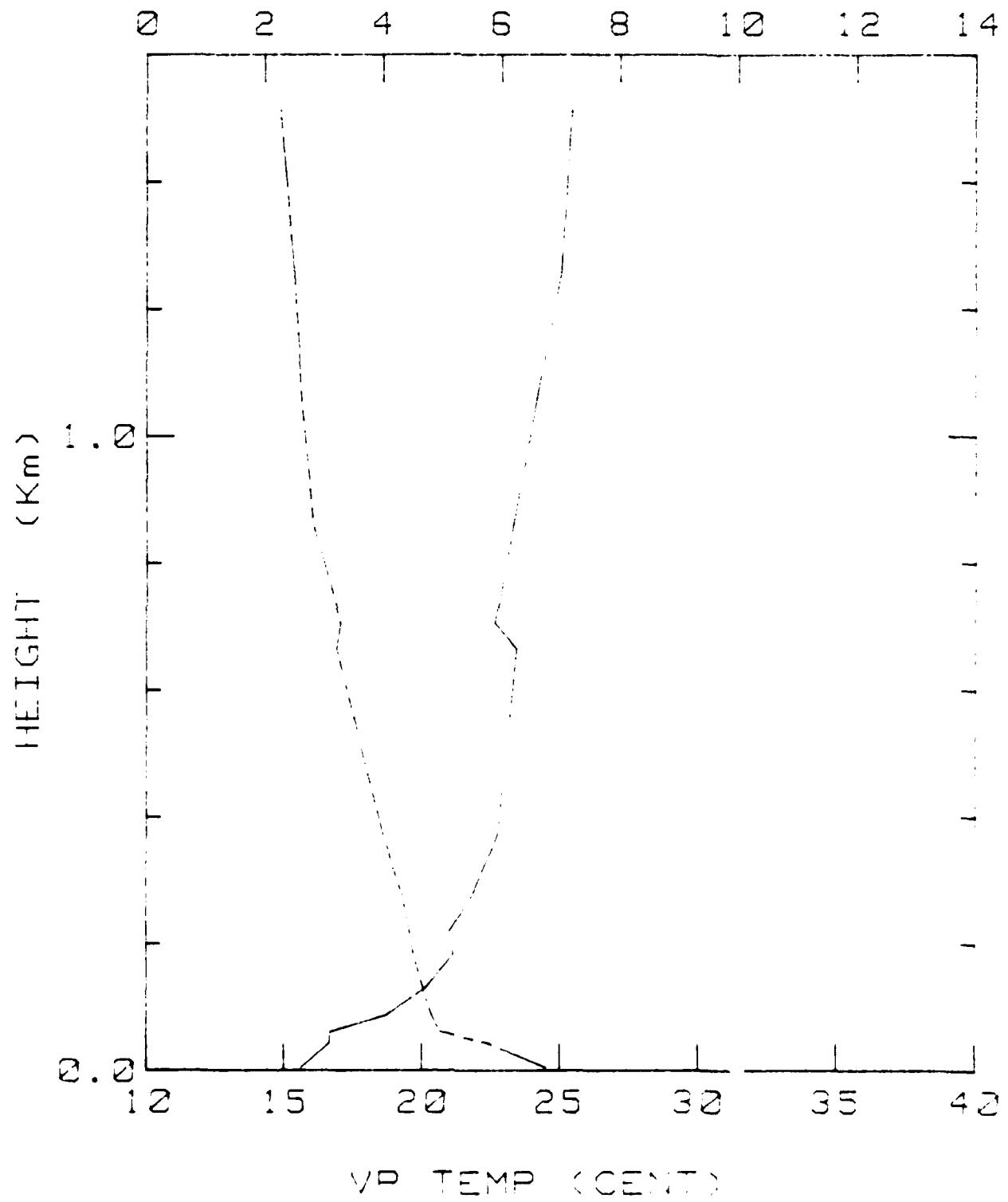
Figure 4b
MIX RATIO (G/KG)



VP TEMP (CENT)

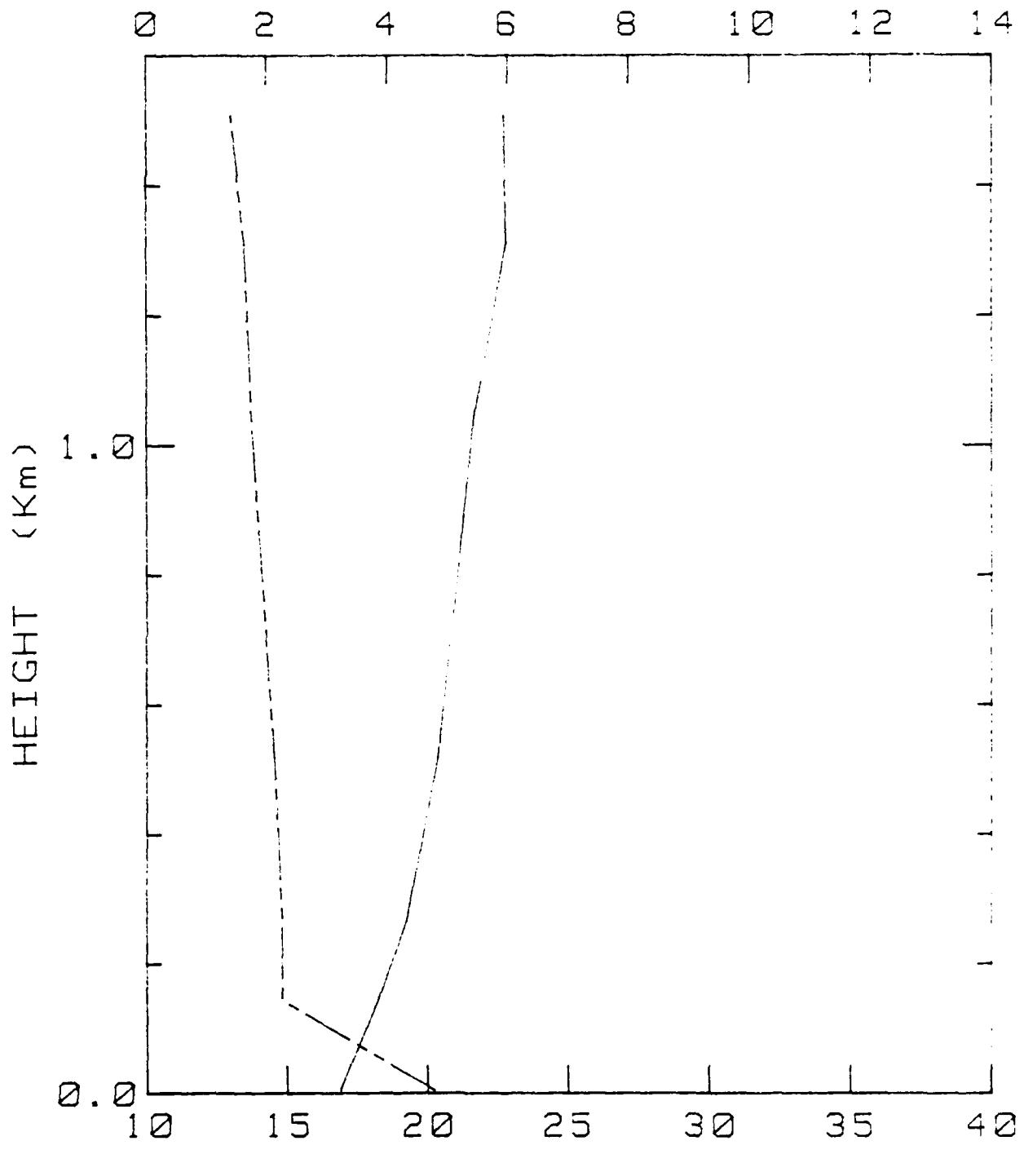
BLM-II 06 JAN 81 740

Figure 4c
MIX RATIO (G/KG)



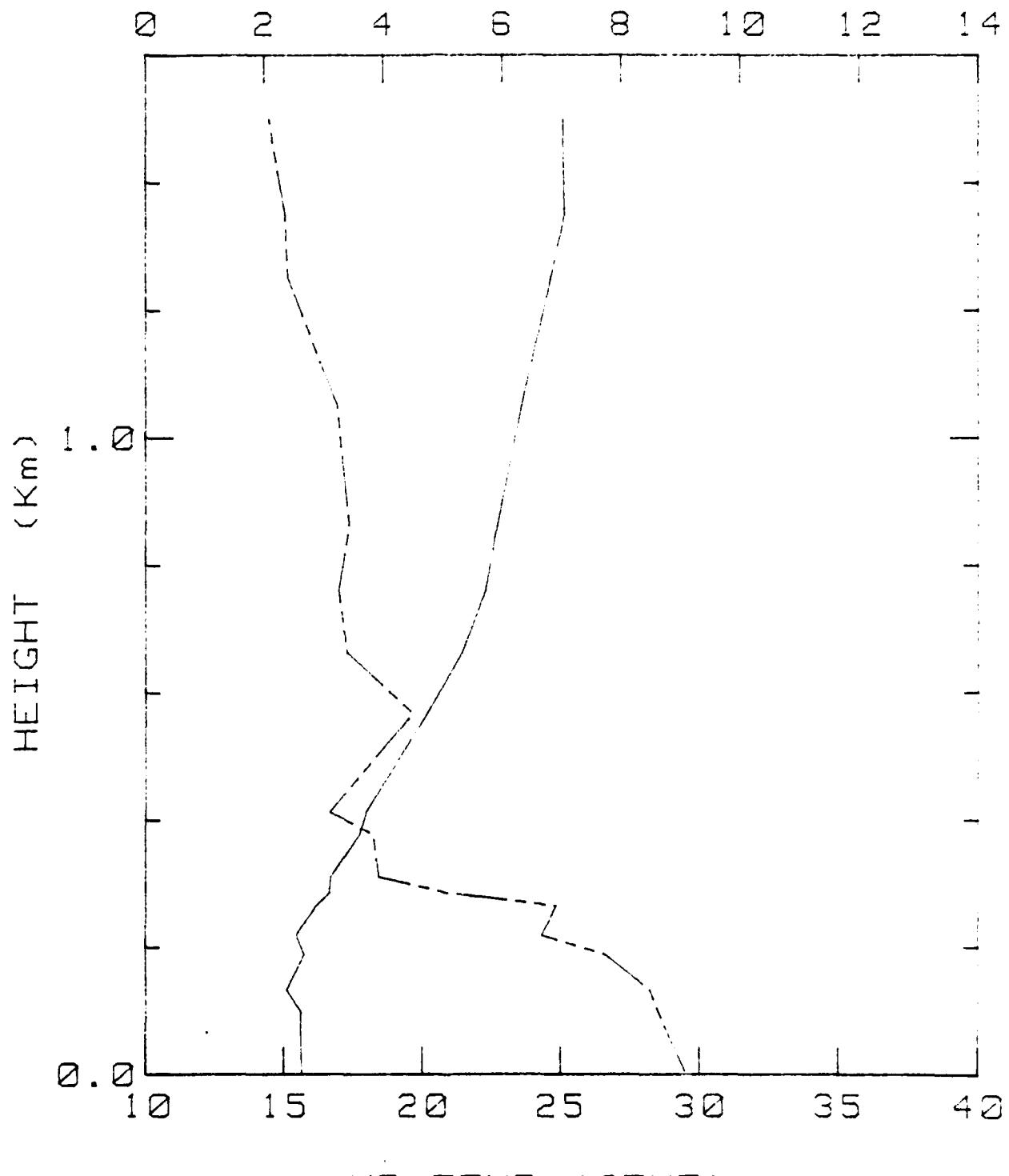
BLM-II 06 JAN 81 1925

Figure 4d
MIX RATIO (G/KG)



VP TEMP (CENT)
BLM-II 07 JAN 81 800

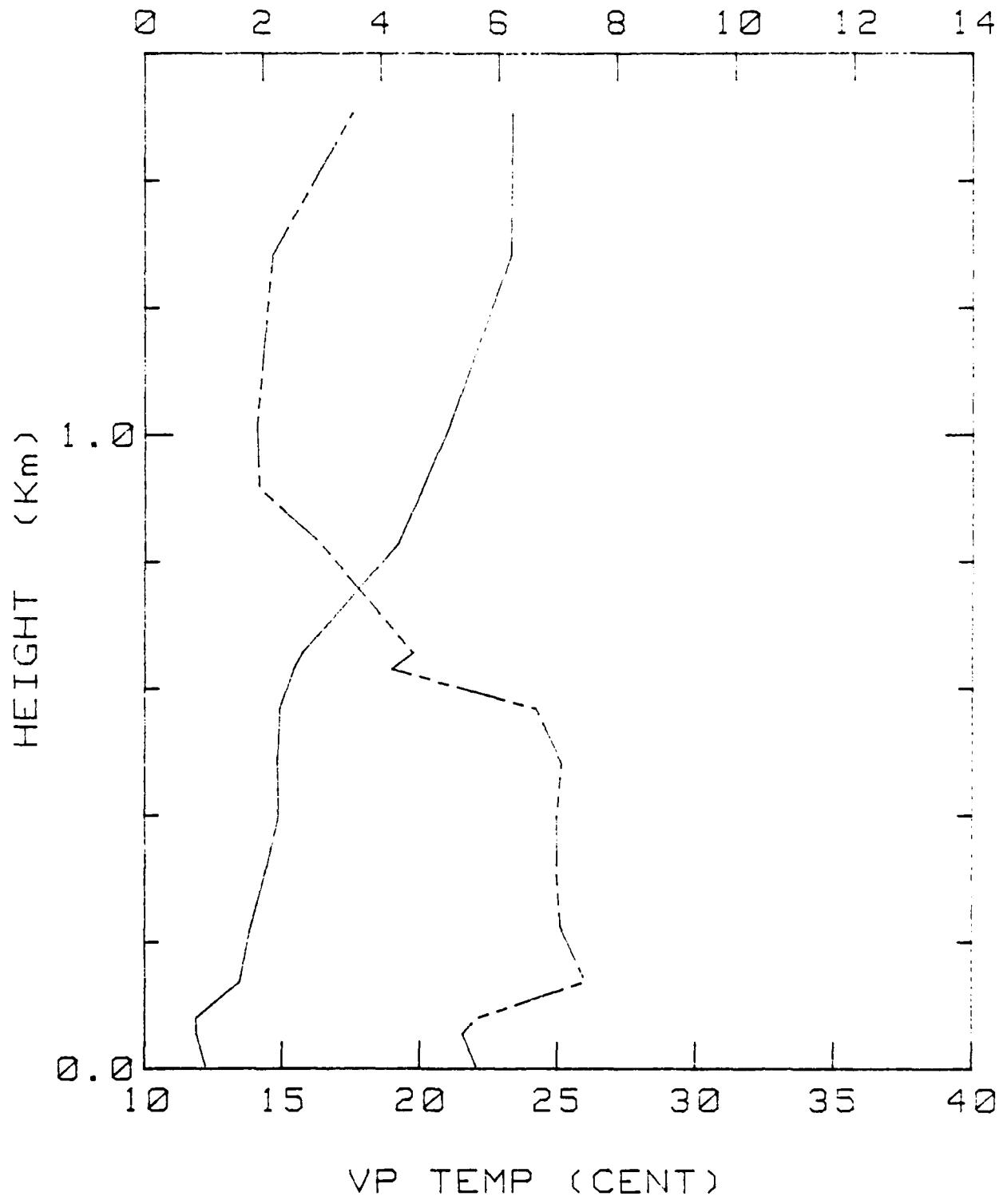
Figure 4e
MIX RATIO (G/KG)



VP TEMP (CENT)
BLM-II 07 JAN 81 1850

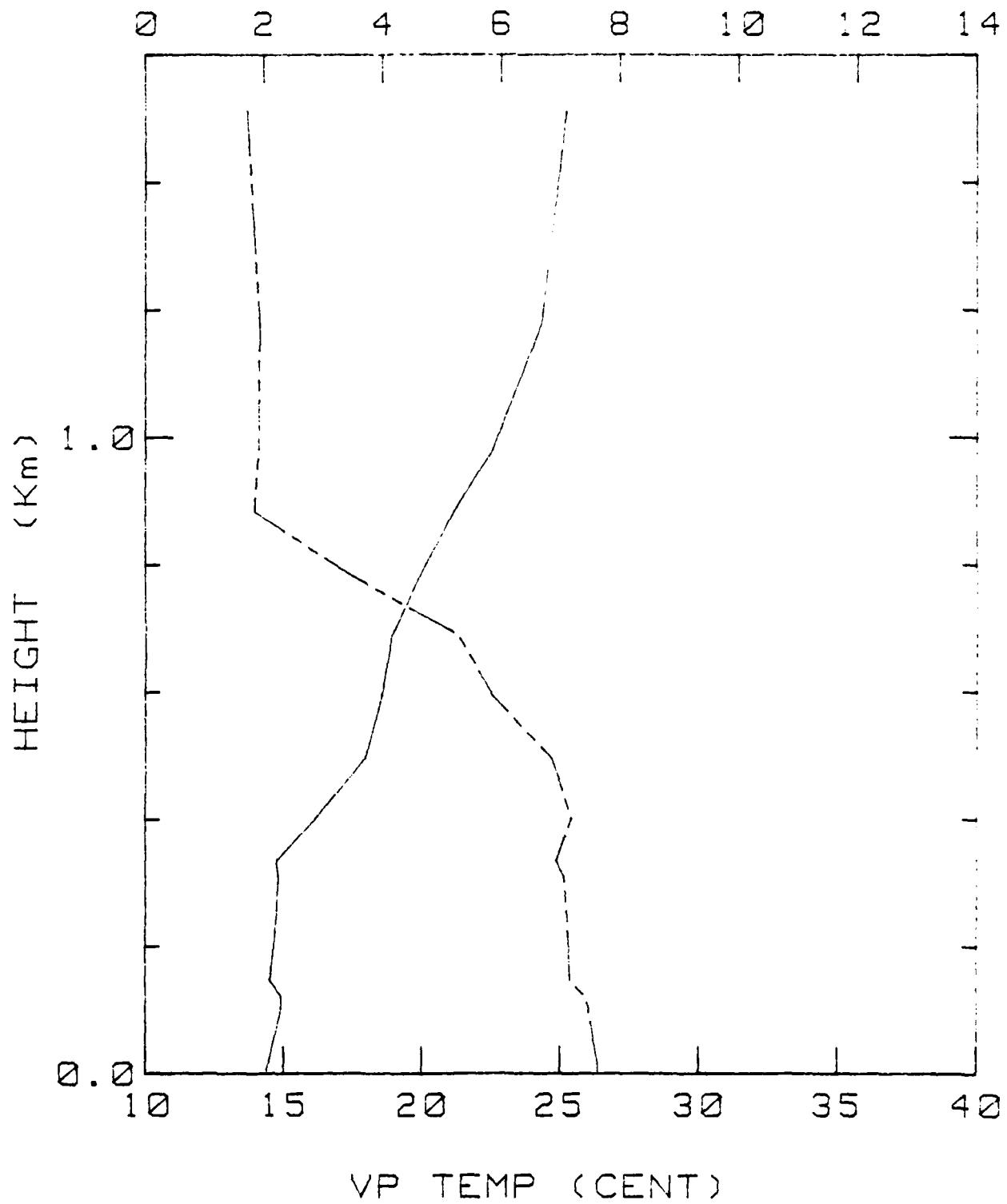
Figure 4f

MIX RATIO (G/KG)



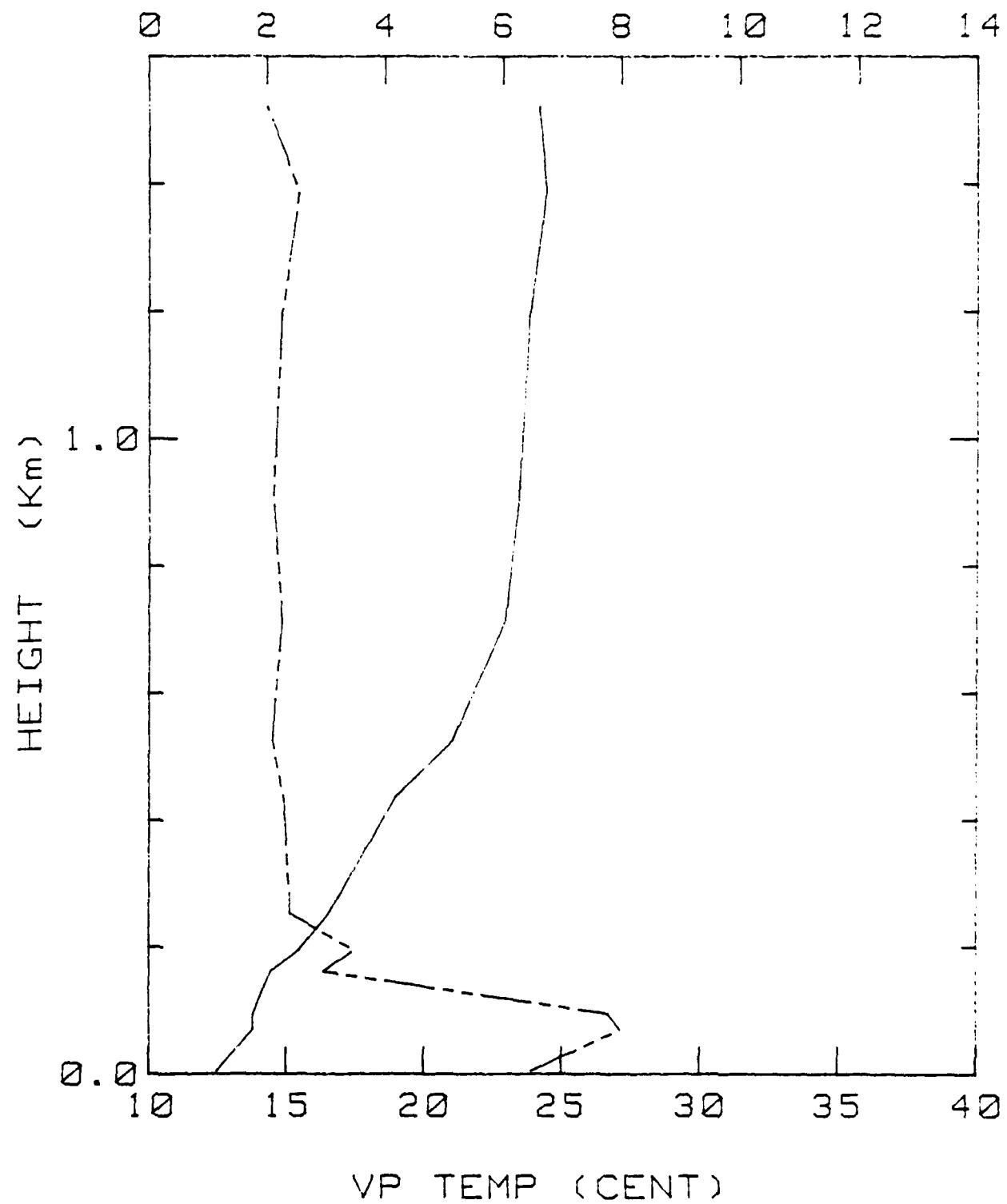
BLM-II 08 JAN 81 815

Figure 4g
MIX RATIO (G/KG)



BLM-II 08 JAN 81 1915

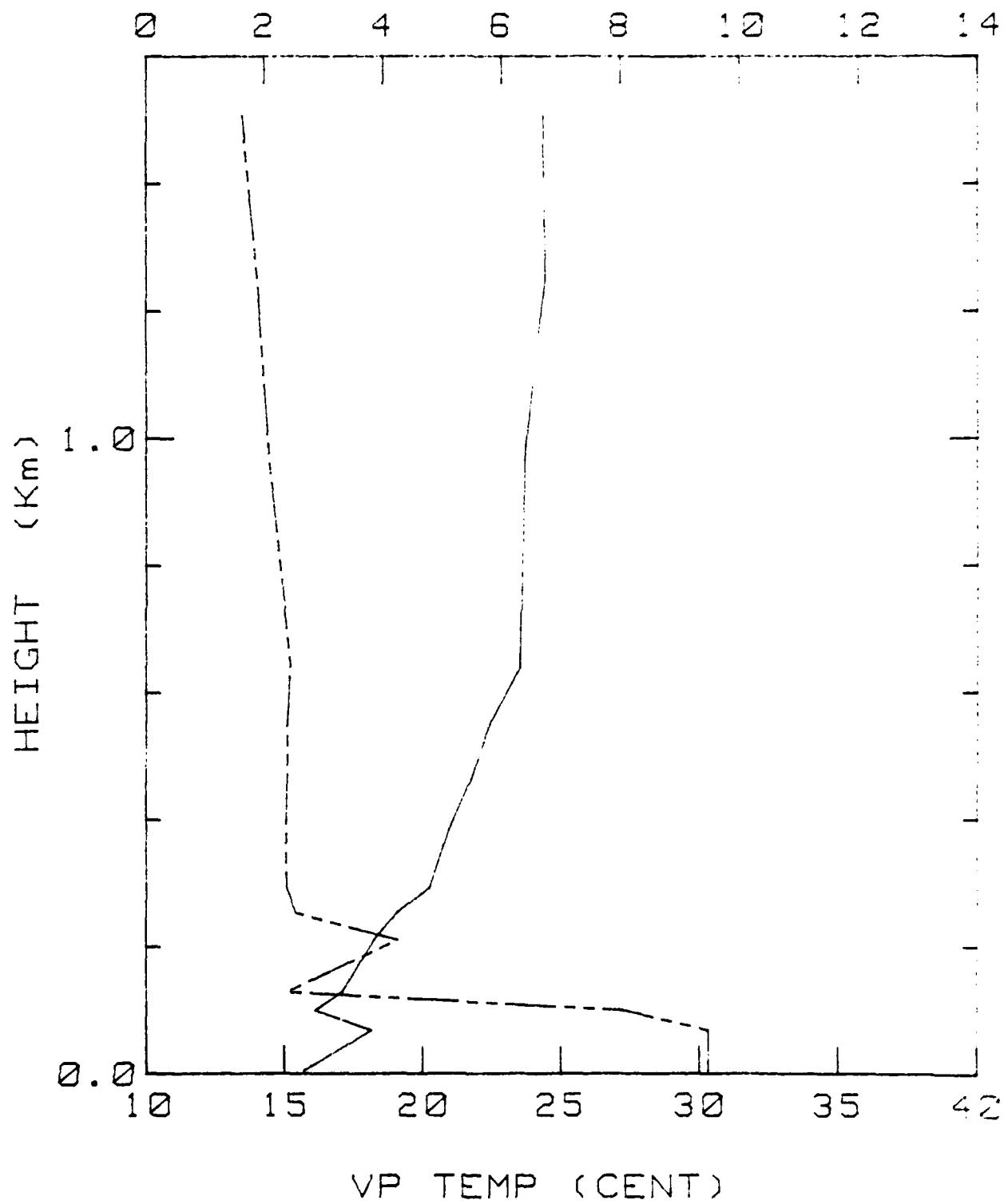
Figure 4h
MIX RATIO (G/KG)



BLM-II 09 JAN 81 810

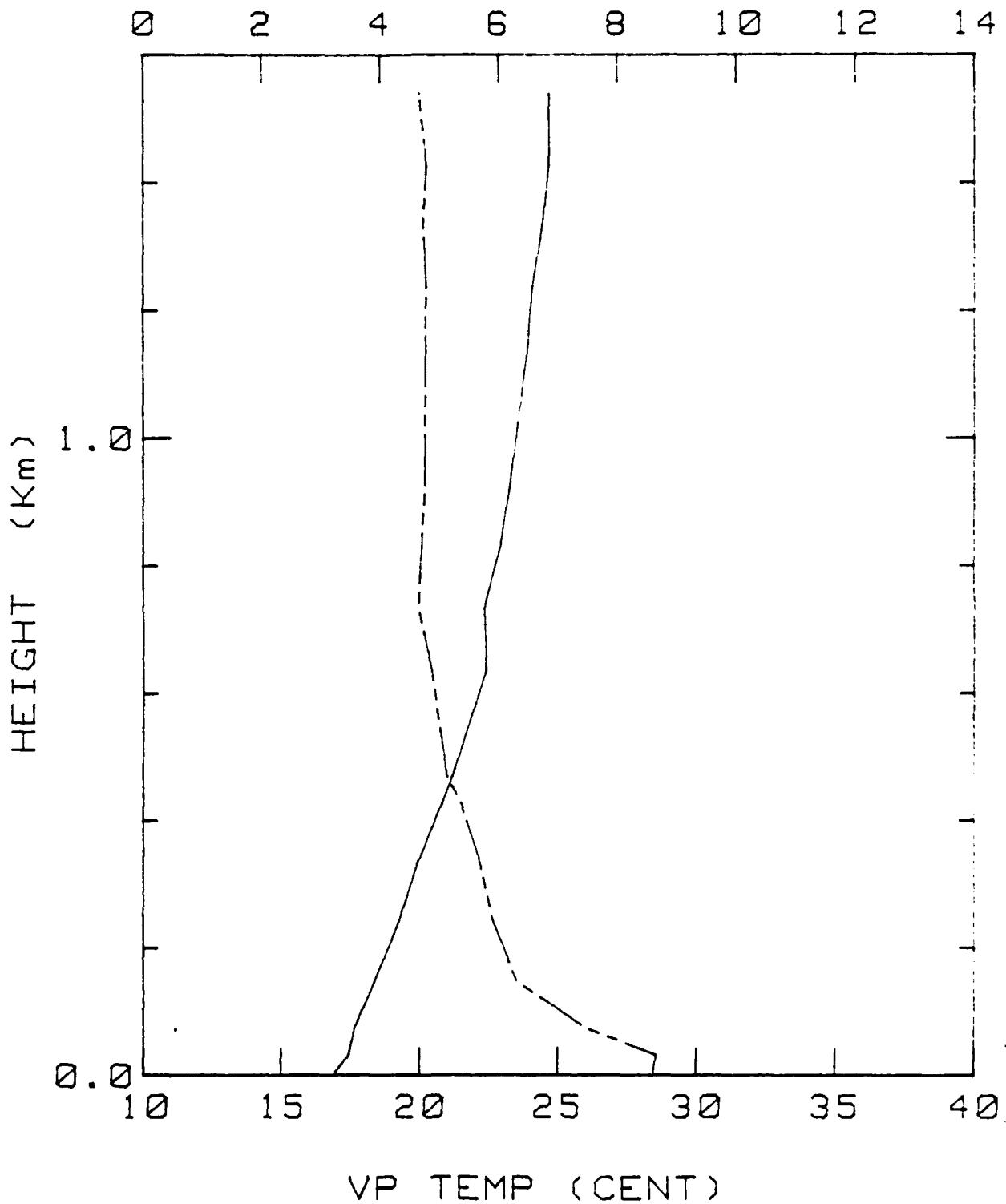
Figure 4i

MIX RATIO (G/KG)



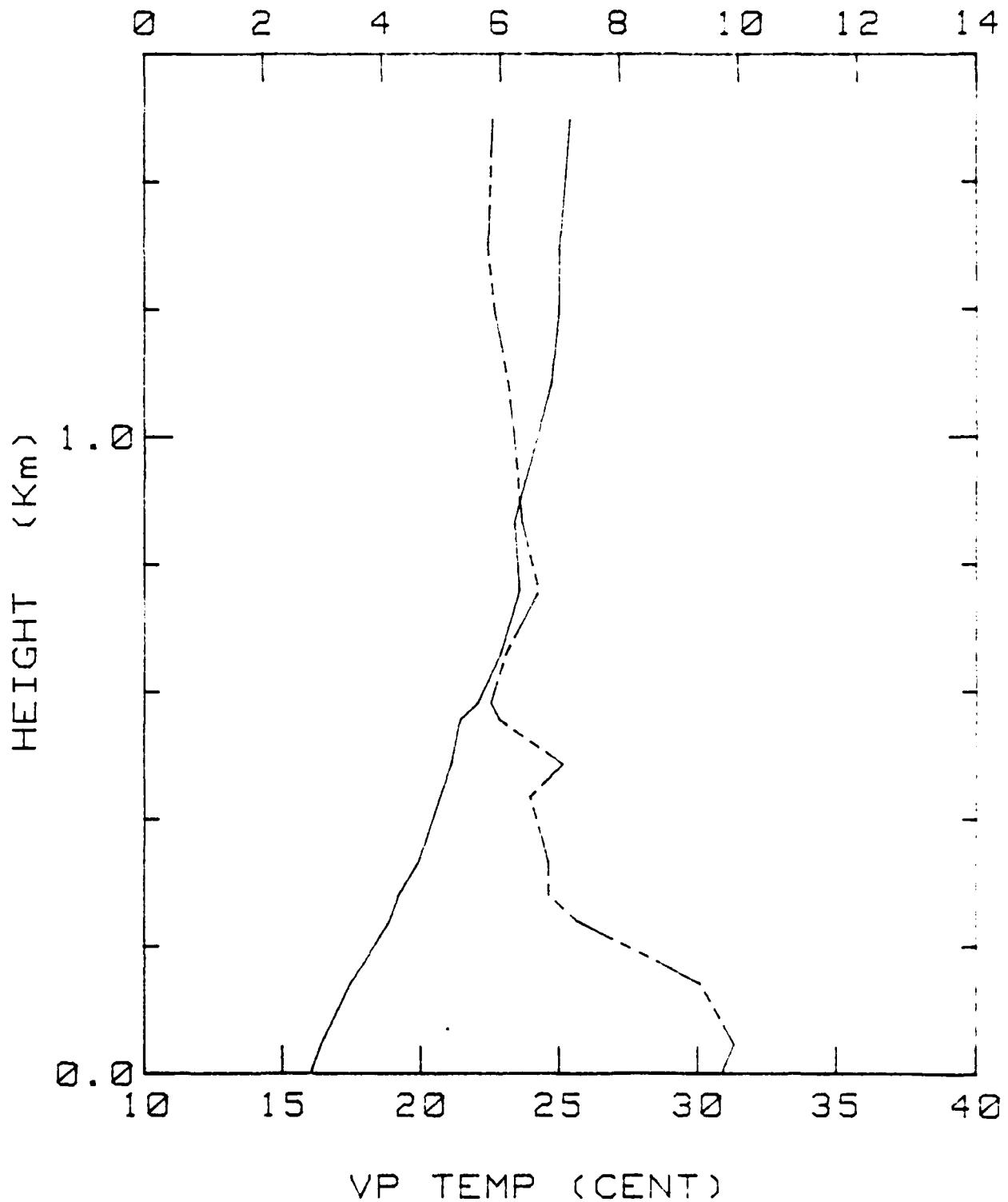
BLM-II 09 JAN 81 1800

Figure 4j
MIX RATIO (G/KG)



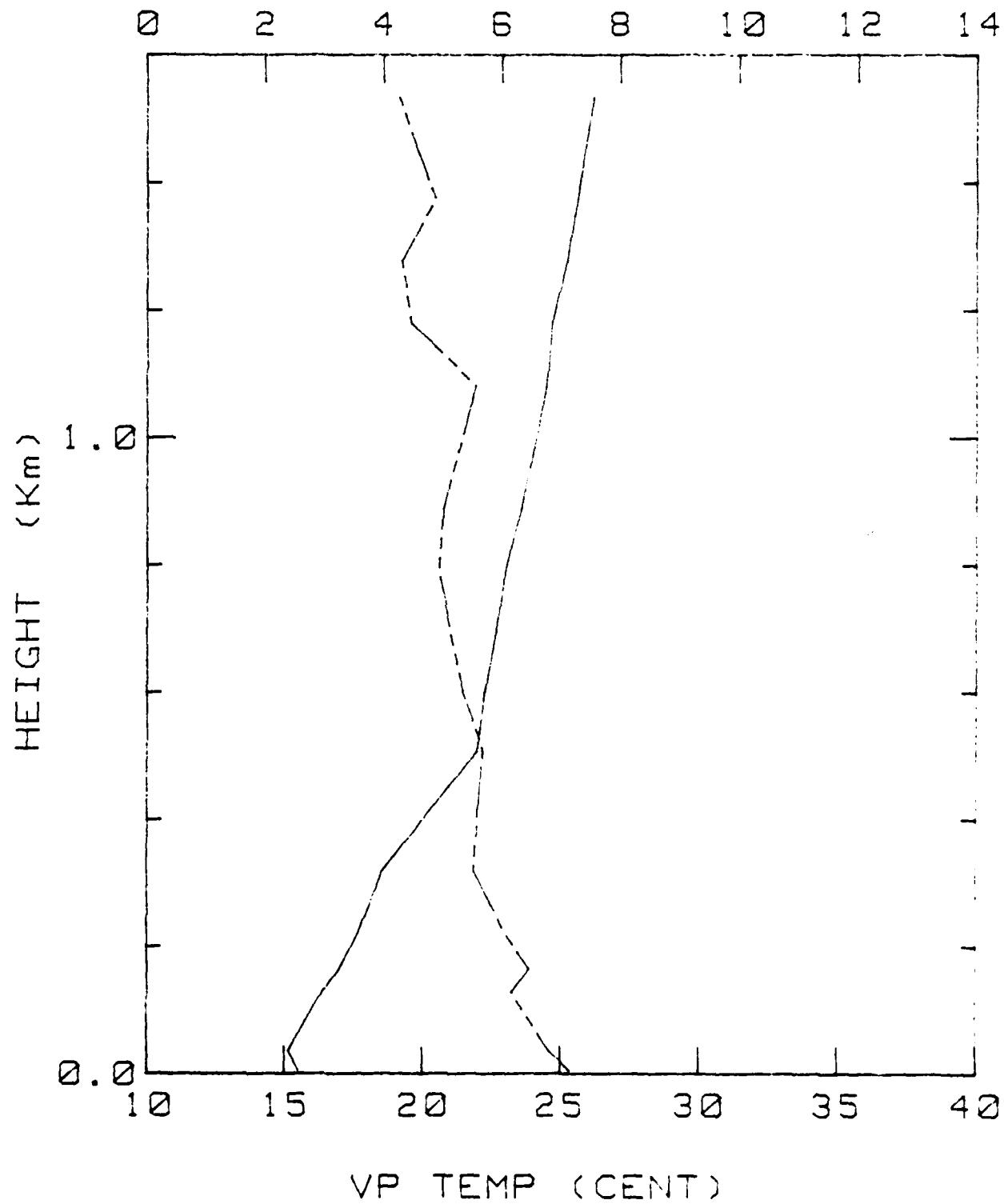
BLM-II 15 JAN 81 900

Figure 4k
MIX RATIO (G/KG)



BLM-II 13 JAN 81 1930

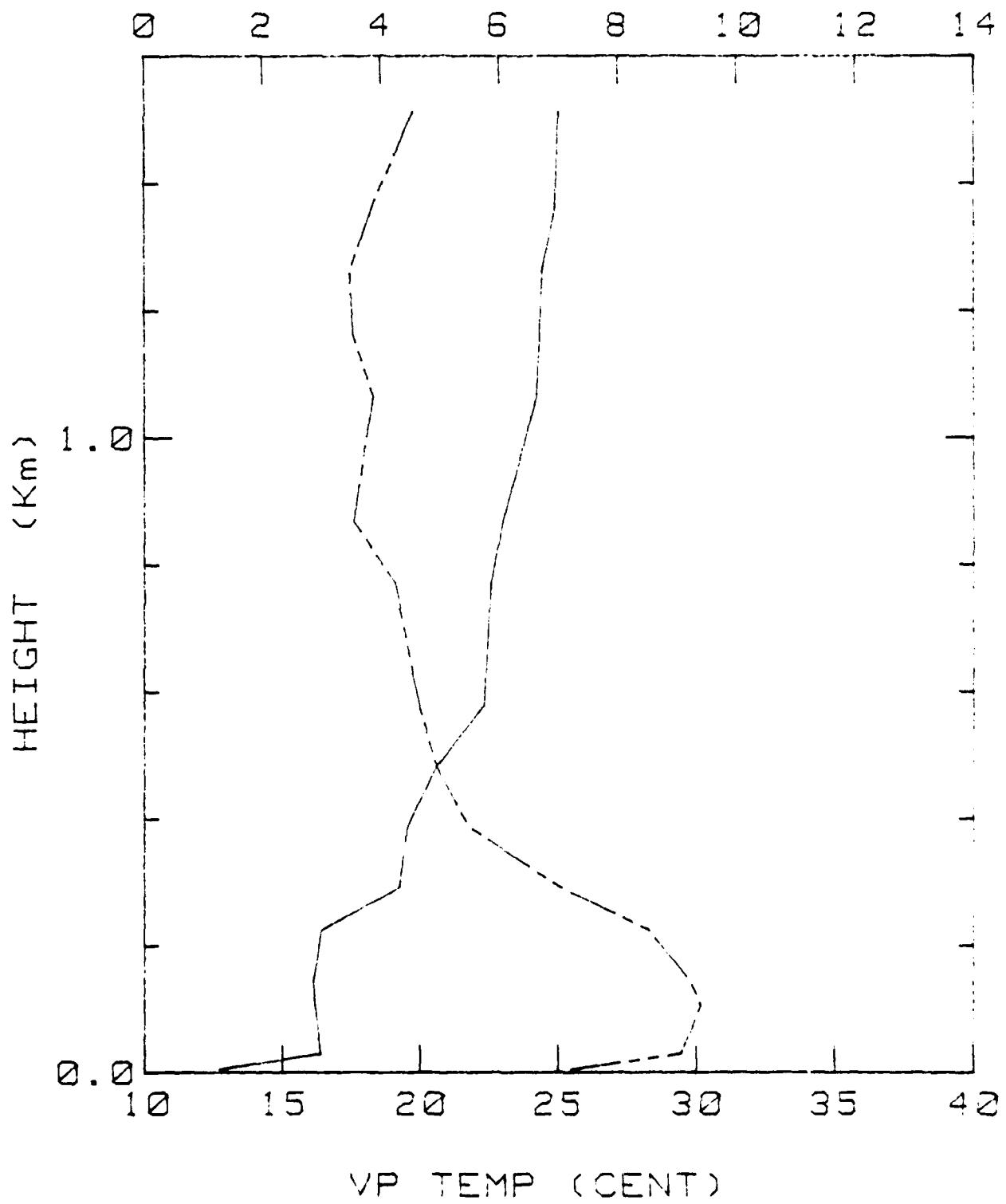
Figure 41
MIX RATIO (G/KG)



BLM-II 14 JAN 81 755

Figure 4m

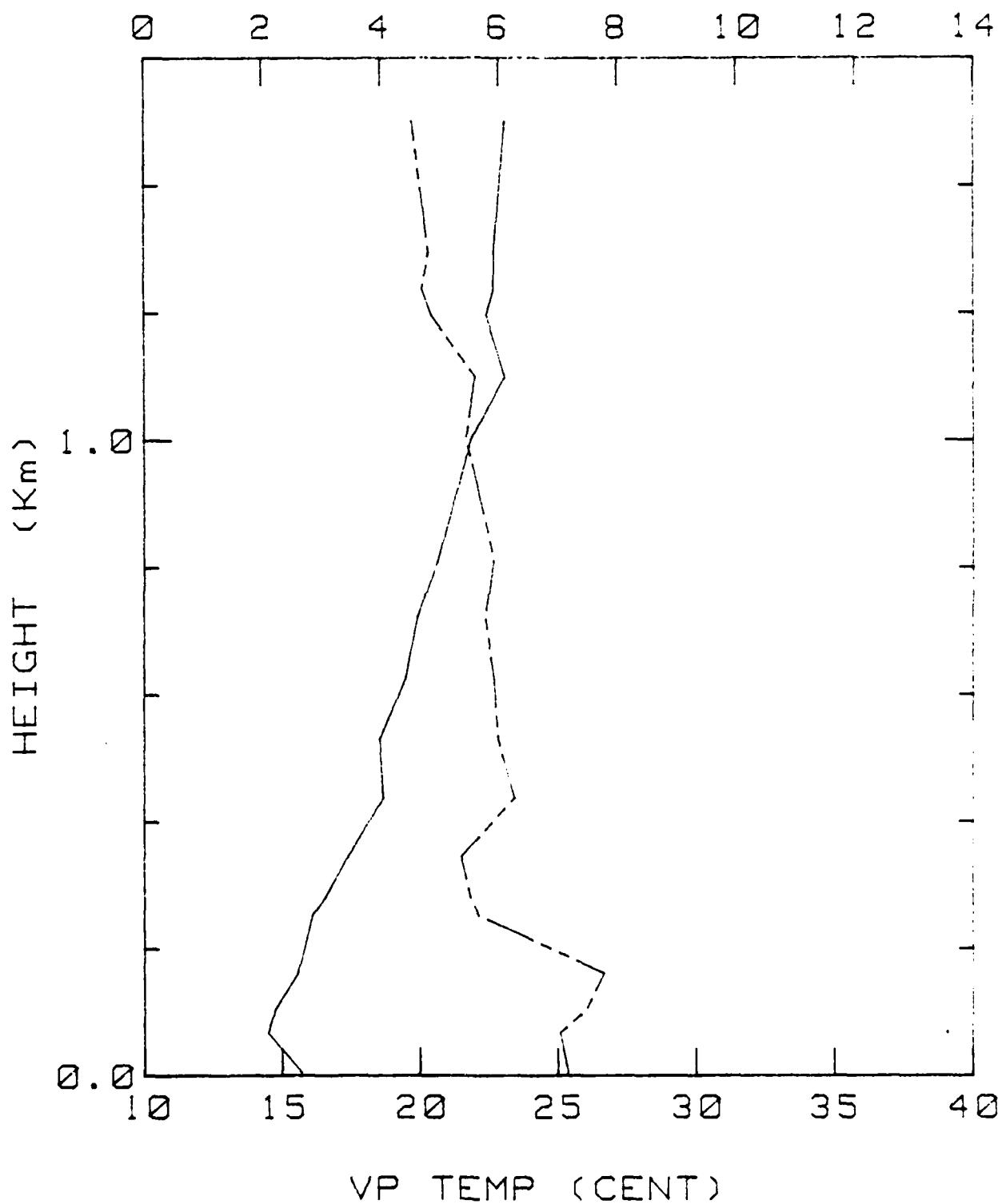
MIX RATIO (G/KG)



BLM-II 14 JAN 81 1920

Figure 4n

MIX RATIO (G/KG)

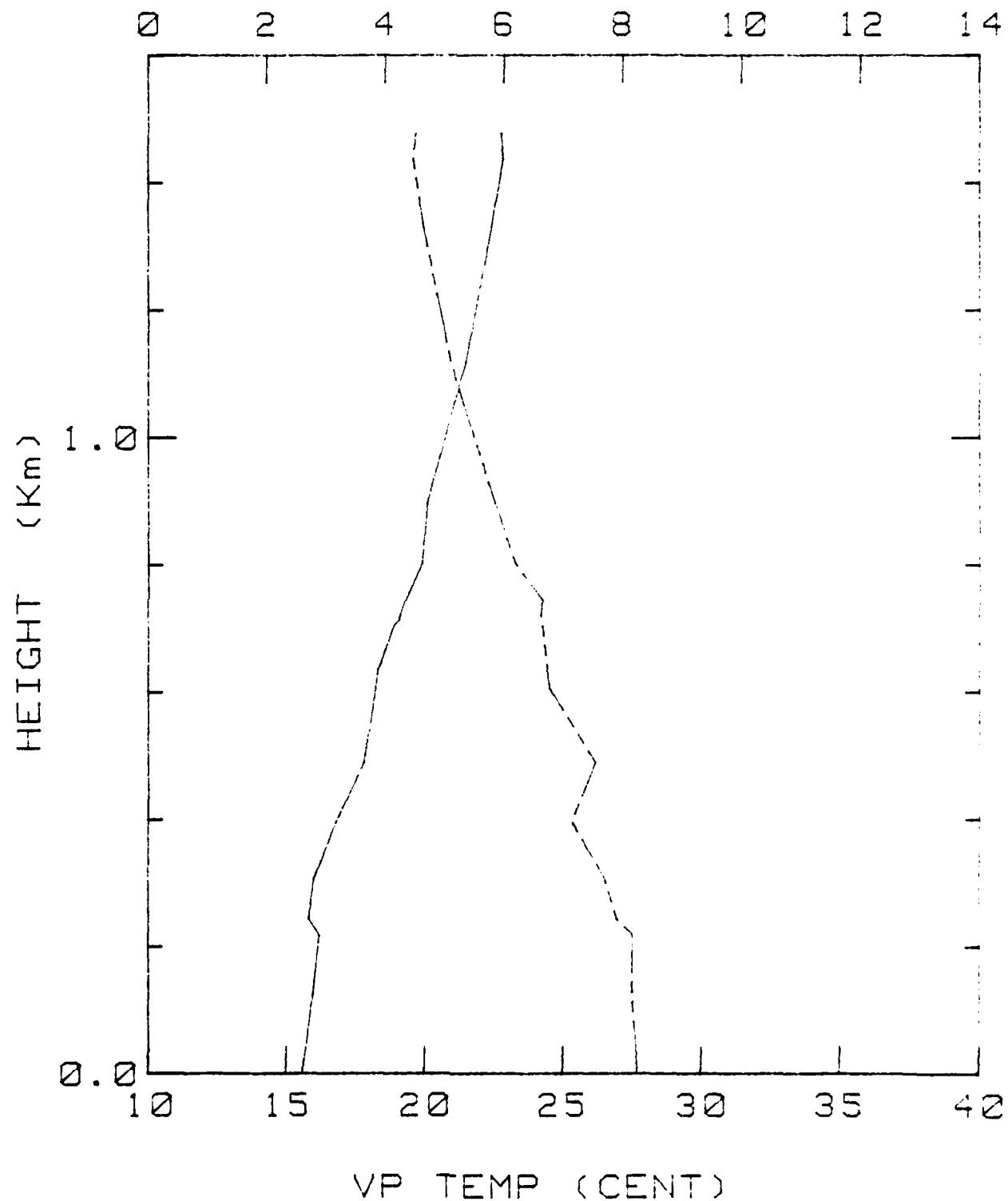


VP TEMP (CENT)

BLM-II 15 JAN 81 830

Figure 4o

MIX RATIO (G/KG)



BLM-II 15 JAN 81 1950

Figure 4p
MIX RATIO (G/KG)

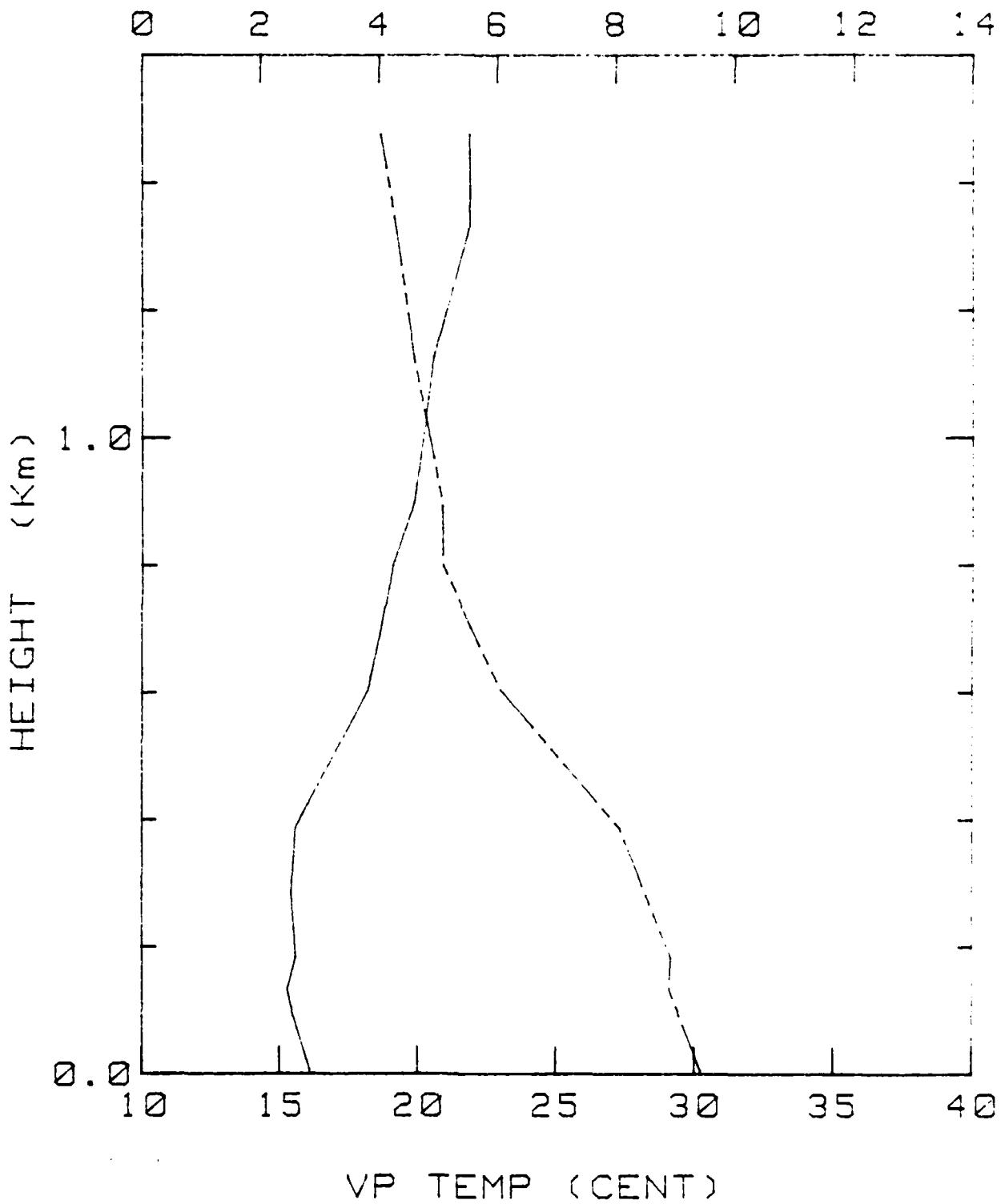
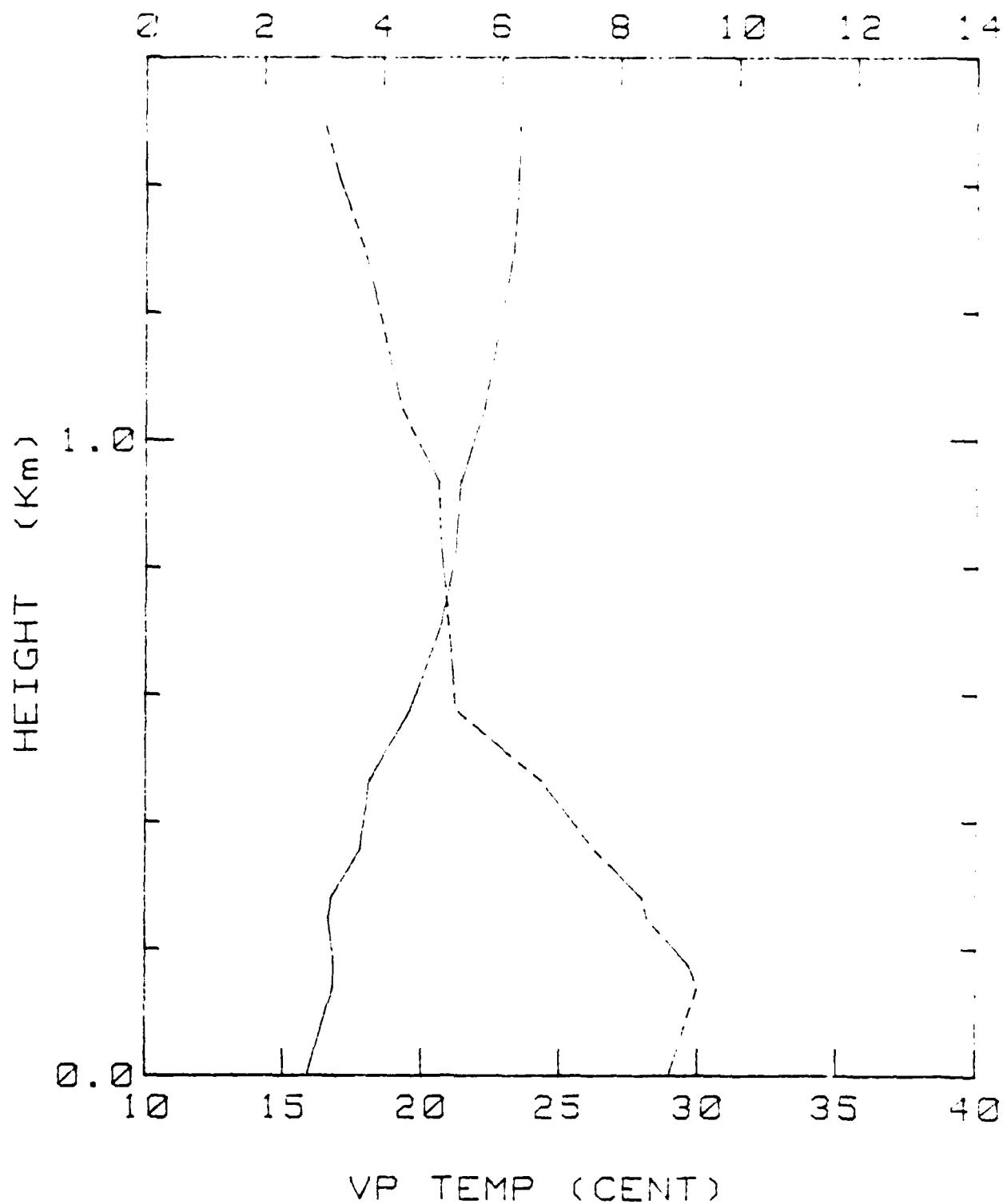


Figure 4q
MIX RATIO (G/G)



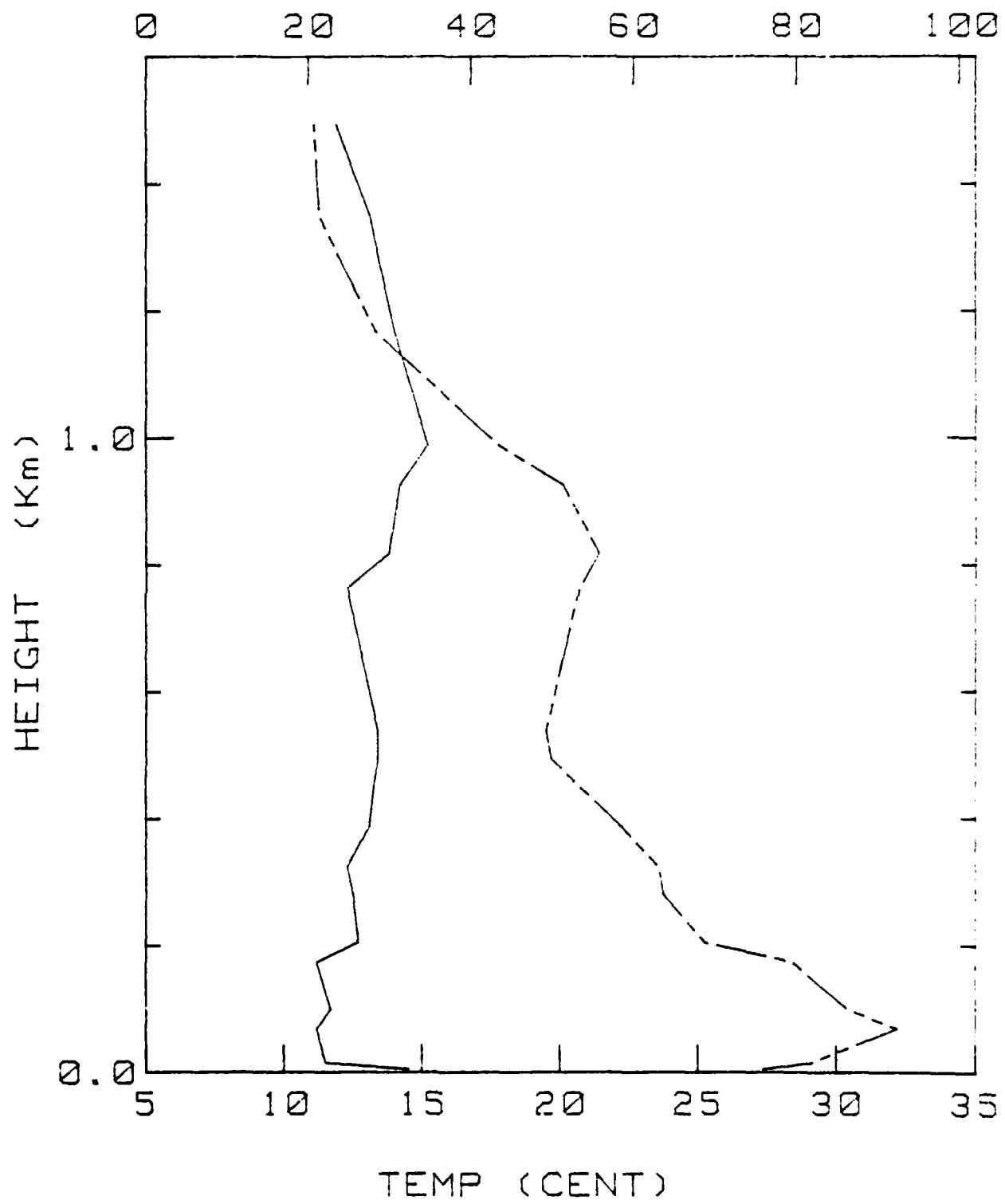
BLM-II 16 JAN 81 1935

Appendix A. BLM-1 Radiosonde and Mixed Layer Parameter Results

The radiosonde results for BLM-1 have been reprocessed by computer in order to put them in the same format as used here for BLM-II results. Also the mixed layer parameters have been calculated. These results are shown in Figures 5.

Figure 5a1

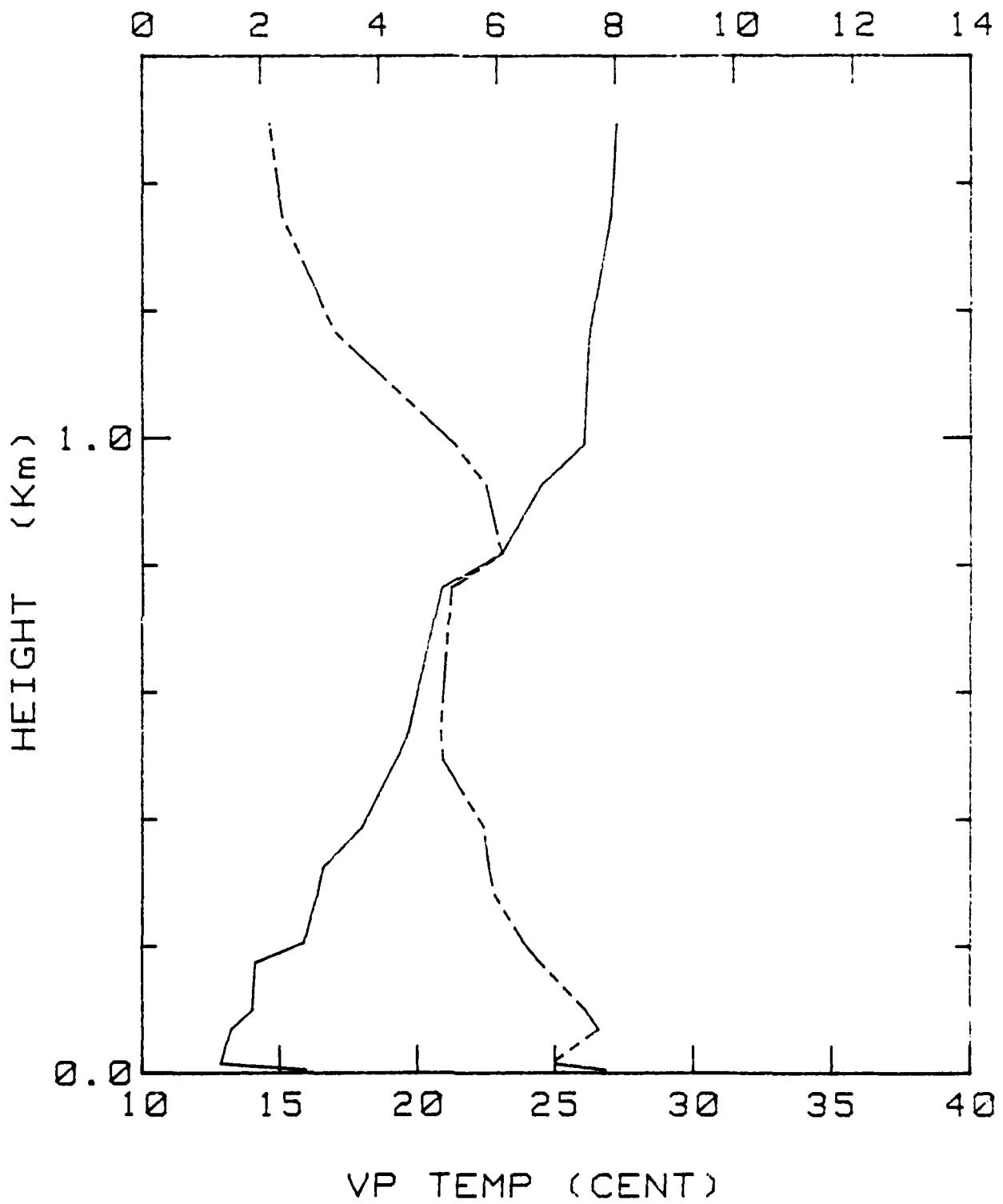
REL HUMIDITY (%)



BLM-I 21 SEPT 80 1205

Figure 5a2

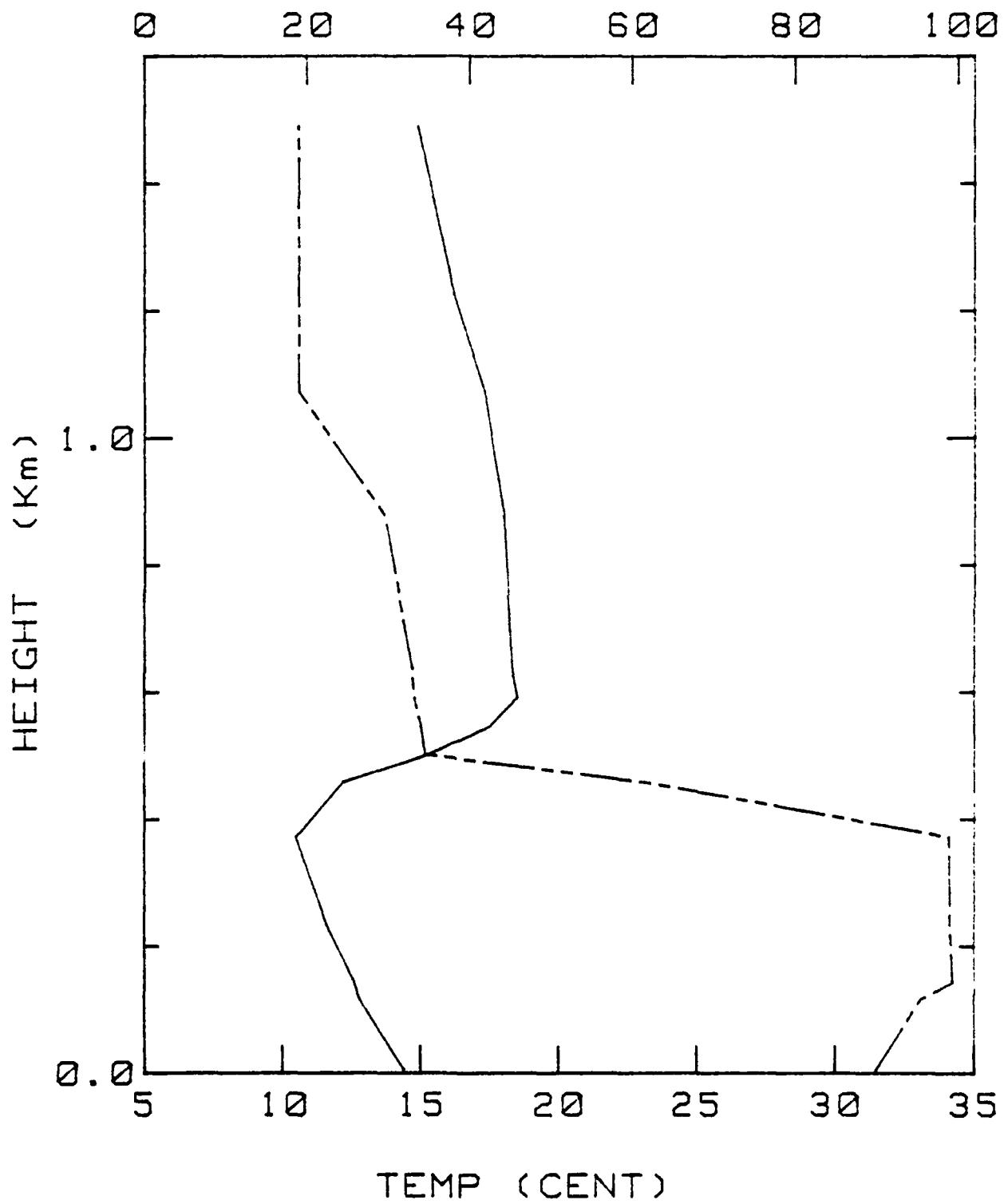
MIX RATIO (G/KG)



BLM-I 21 SEPT 80 1205

Figure 5b1

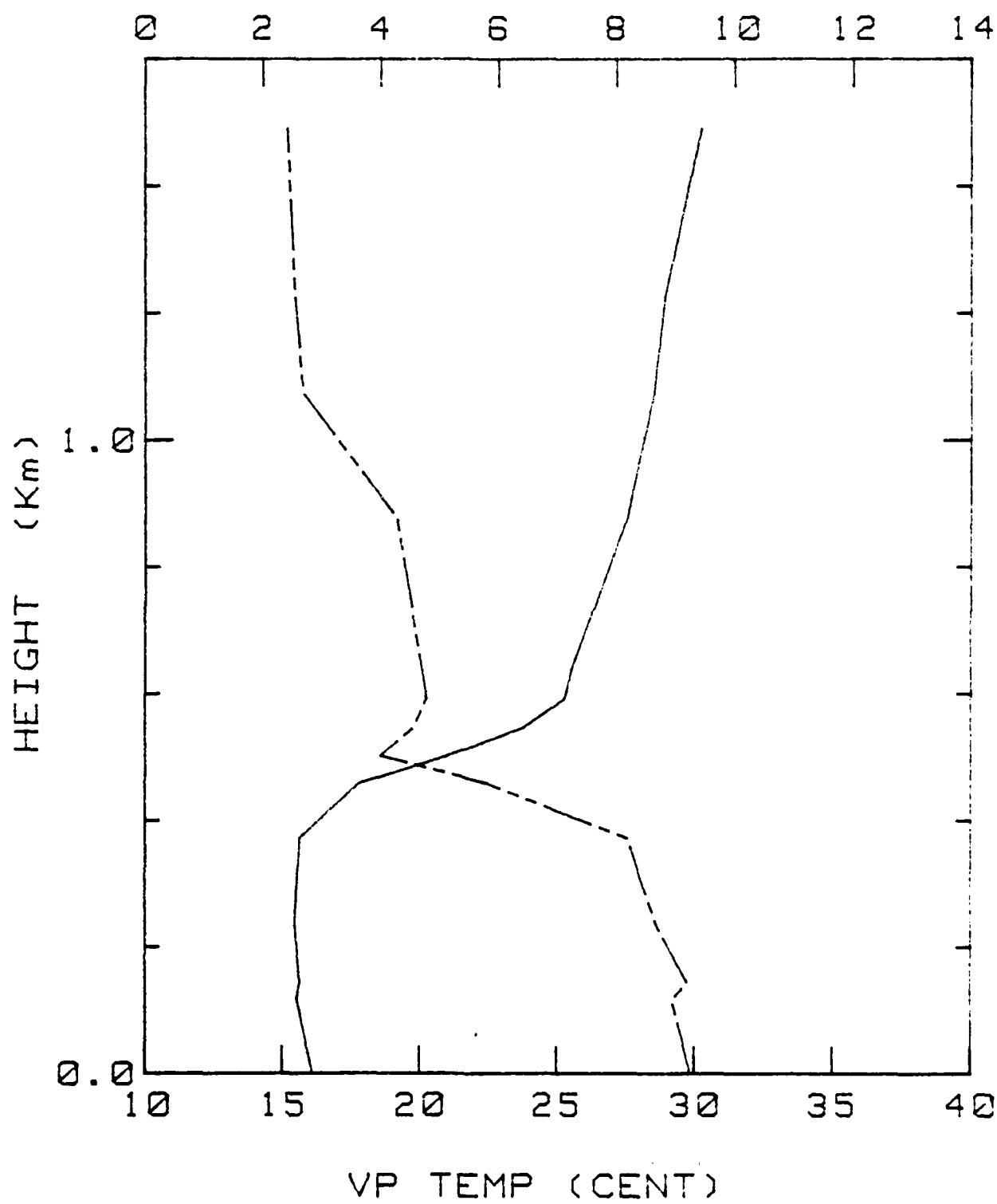
REL HUMIDITY (%)



BLM-I 22 SEPT 80 15

Figure 5b2

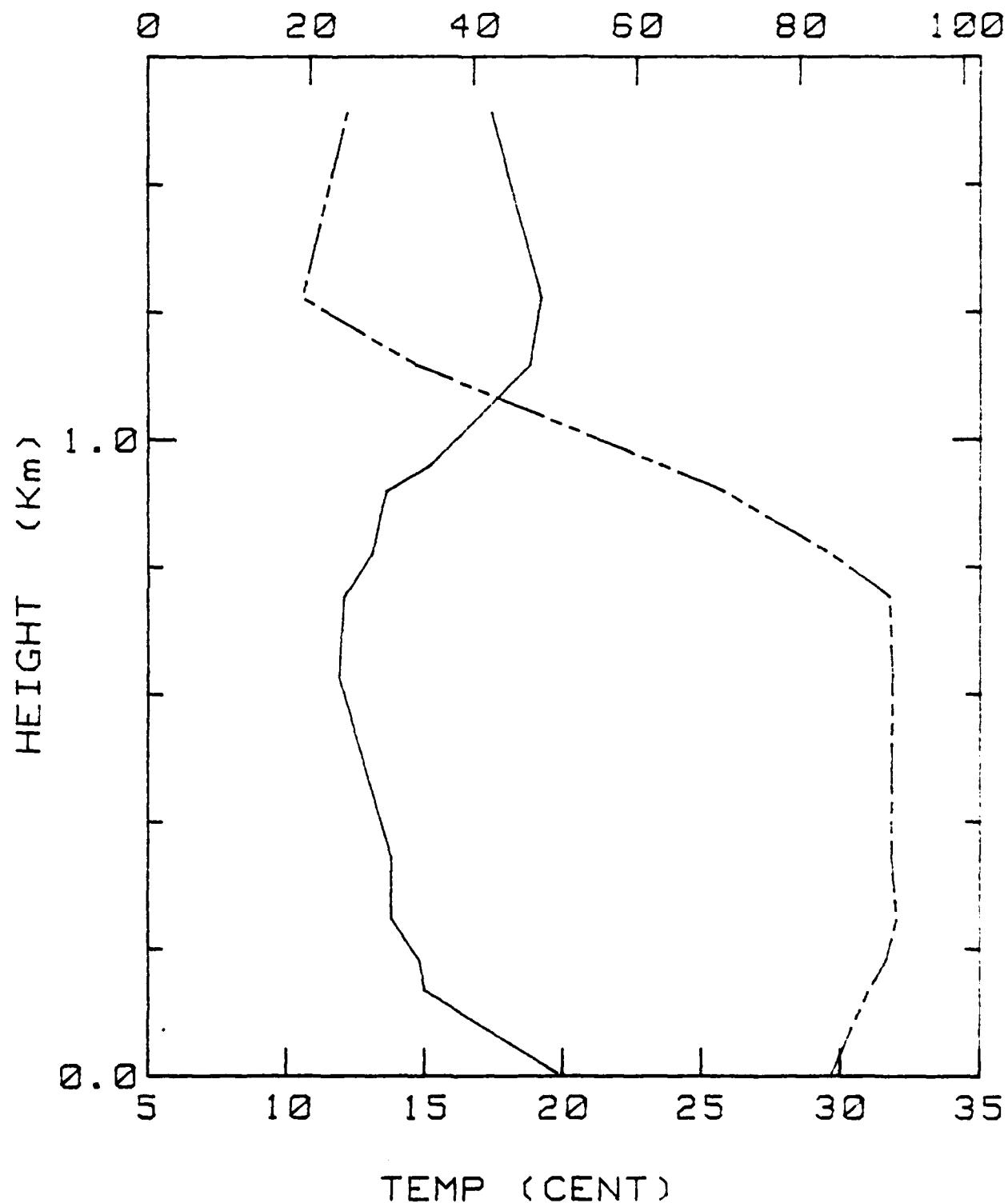
MIX RATIO (G/KG)



BLM-I 22 SEPT 80 15

Figure 5cl

REL HUMIDITY (%)



BLM-I 22 SEPT 80 1215

Figure 5c2

MIX RATIO (G/KG)

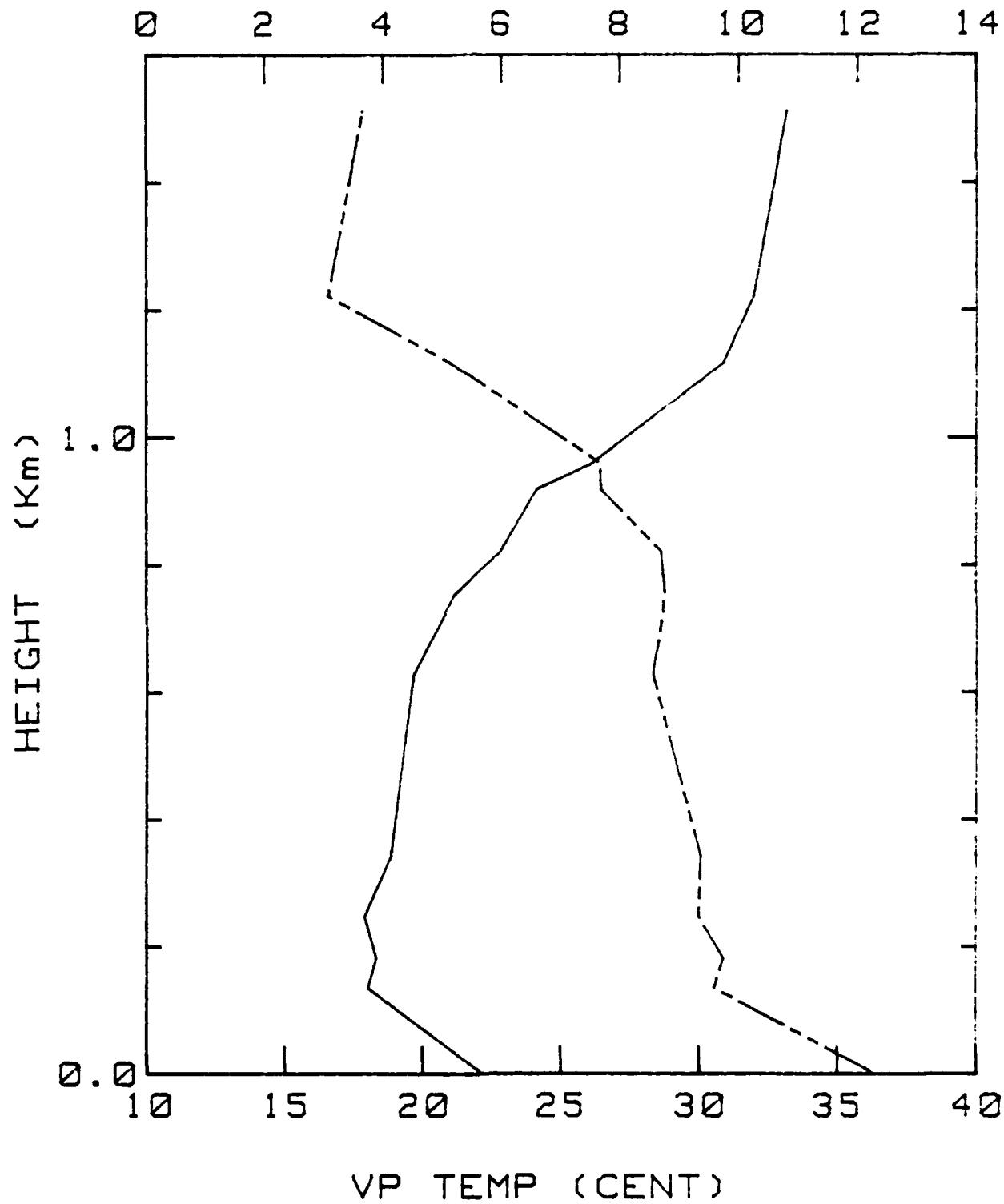
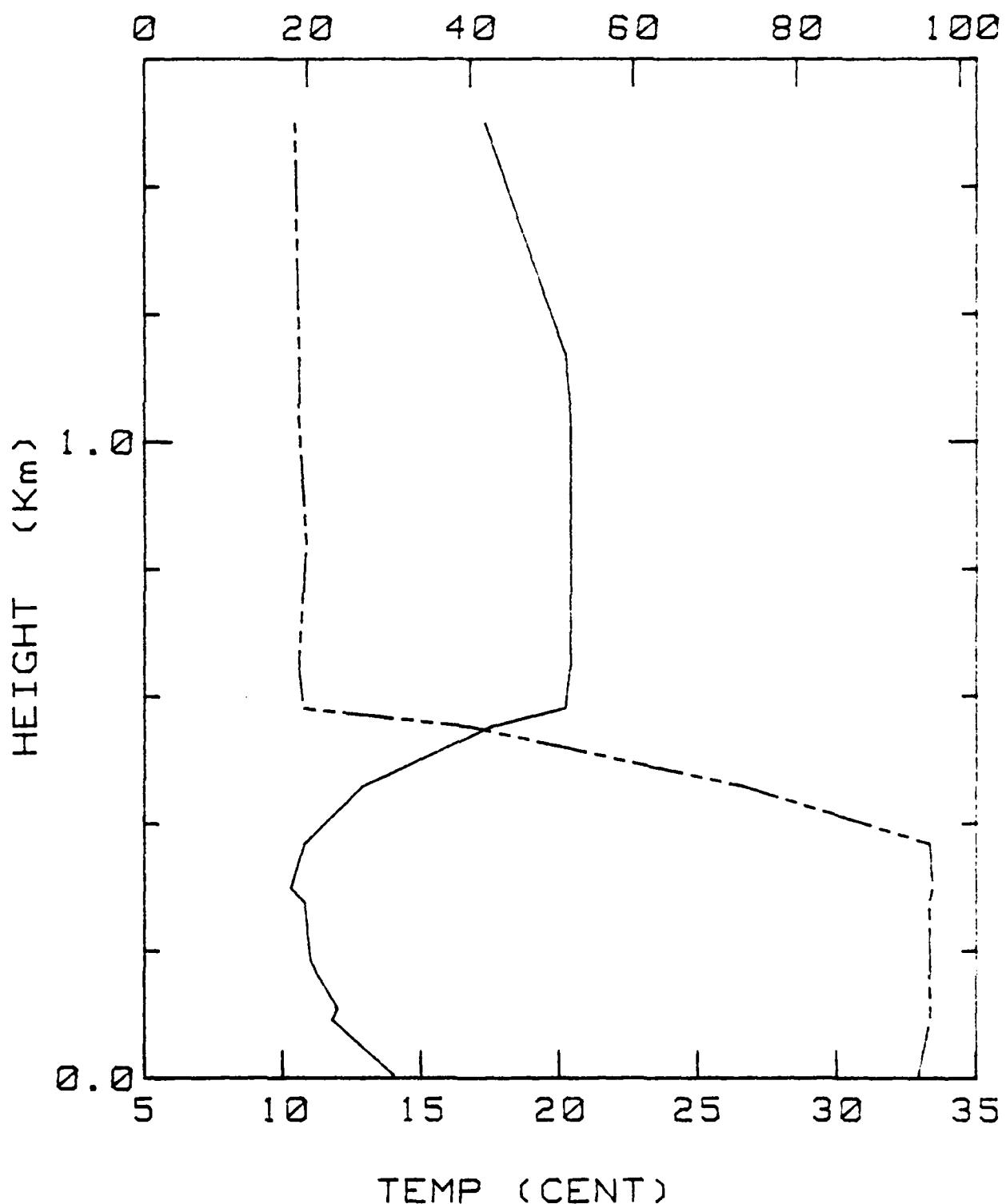


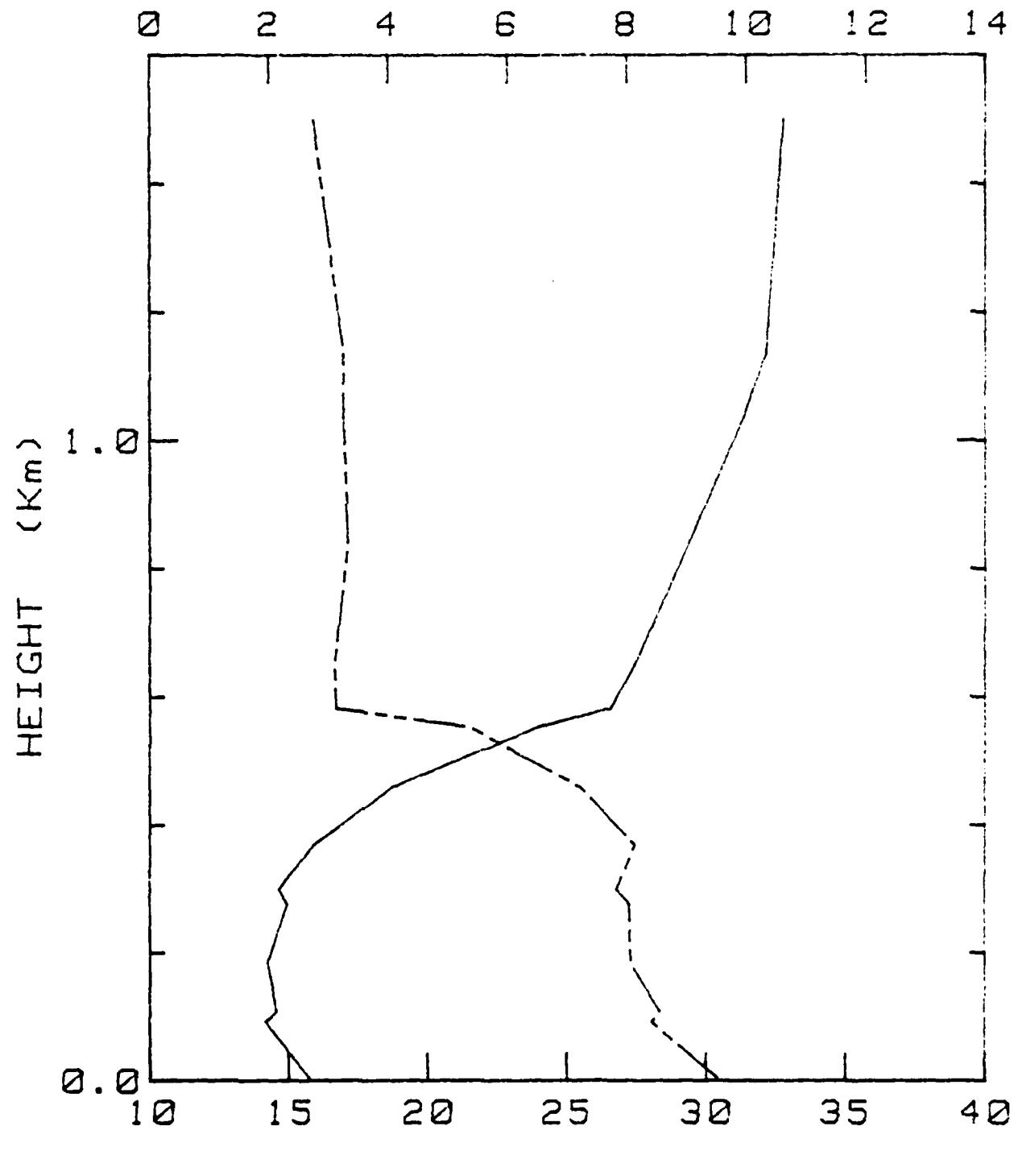
Figure 5d1

REL HUMIDITY (%)



BLM-I 23 SEPT 80 715

Figure 5d2
MIX RATIO (G/KG)



BLM-I 23 SEPT 80 715

Figure 5el

REL HUMIDITY (%)

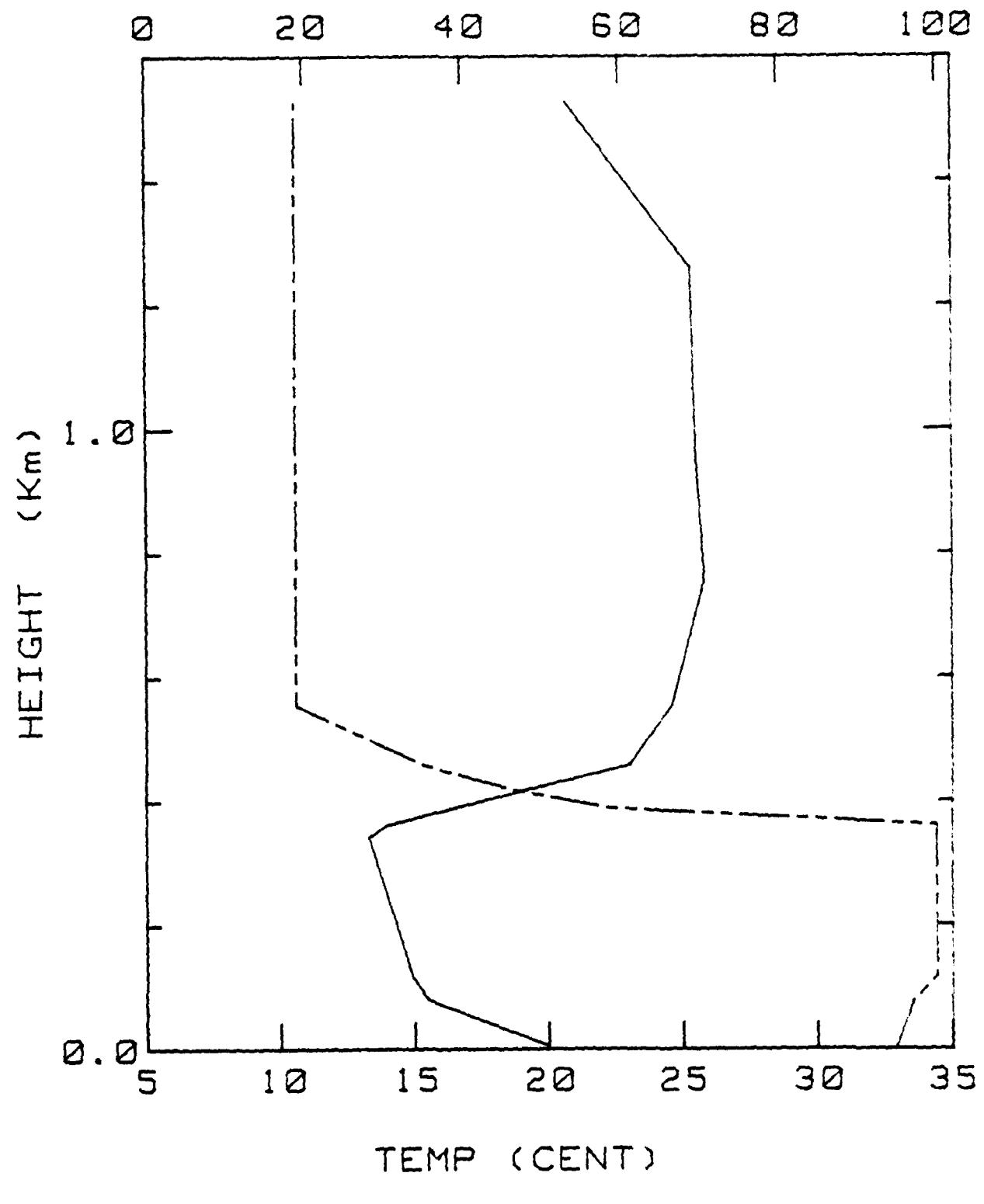


Figure 5e2

MIX RATIO (G/KG)

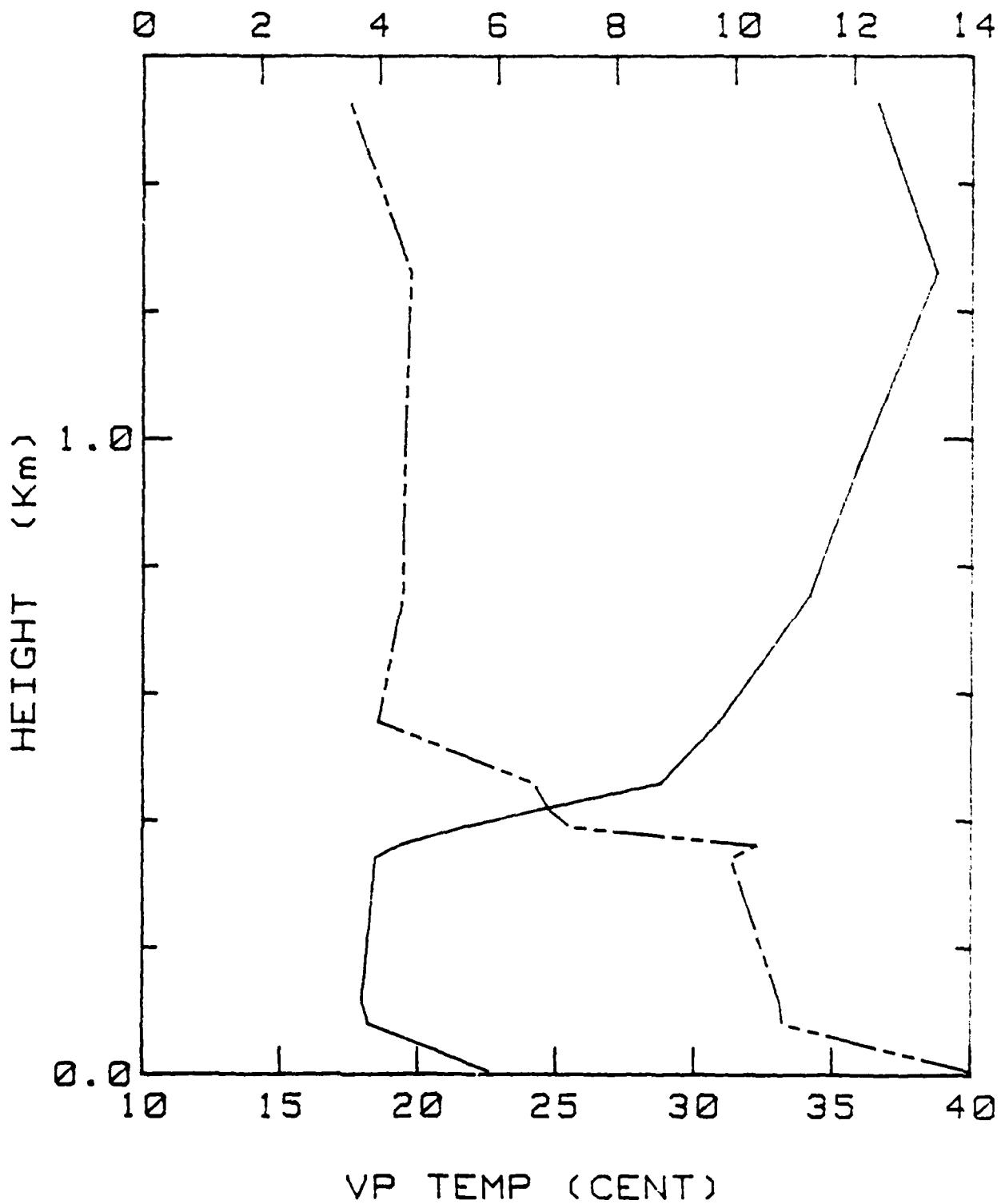
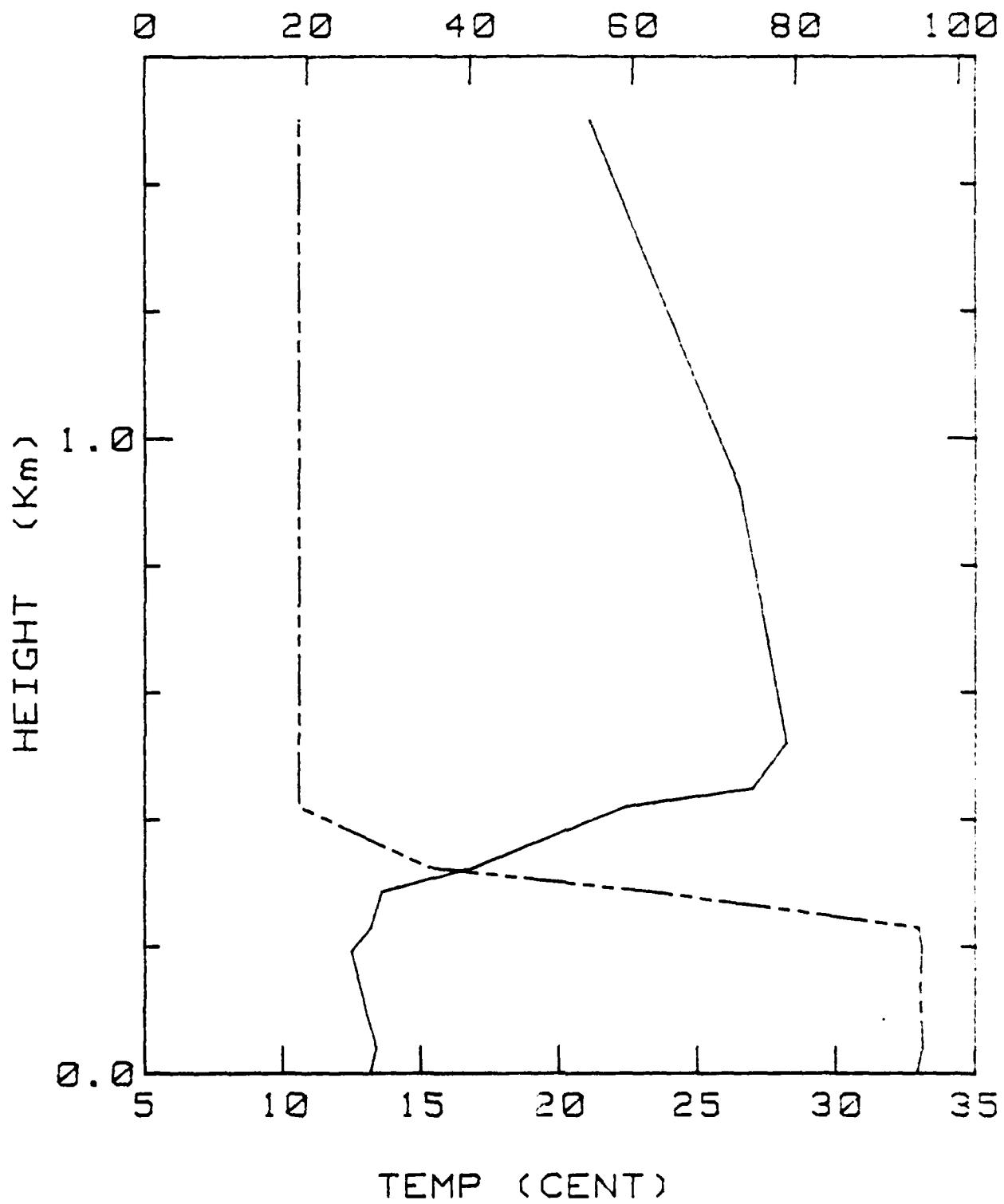


Figure 5f1

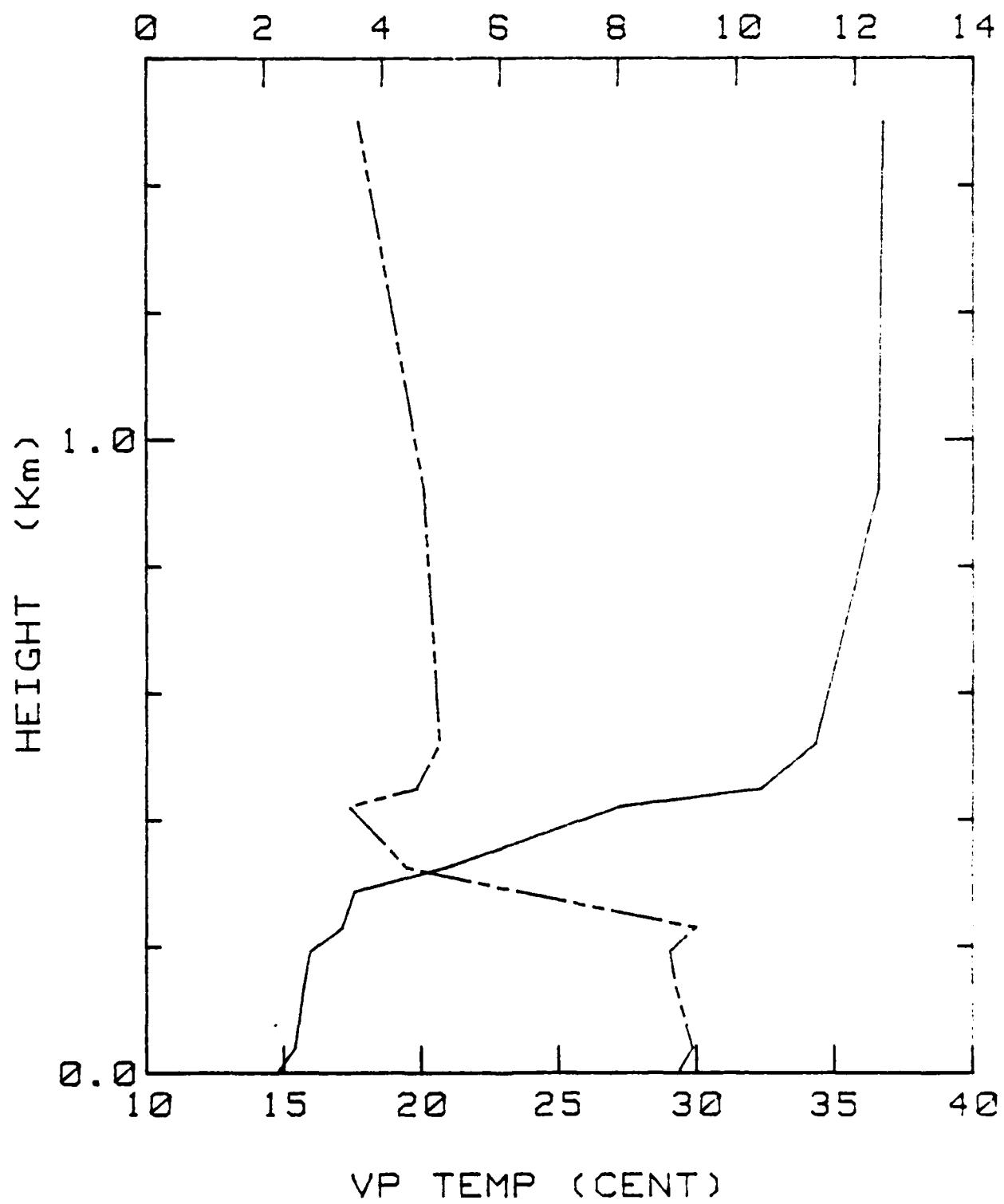
REL HUMIDITY (%)



BLM-I 24 SEPT 80 10

Figure 5f2

MIX RATIO (G/KG)

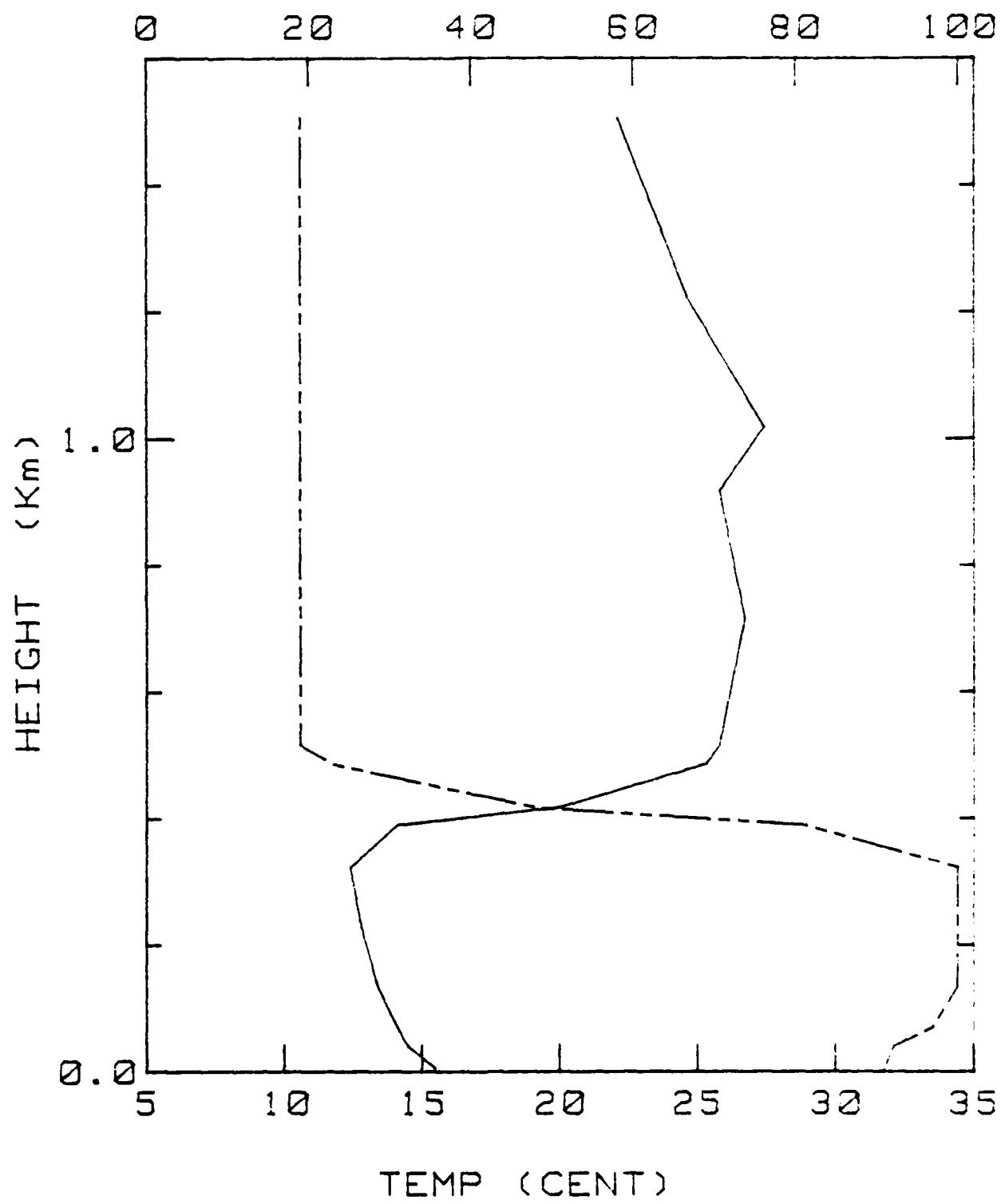


VP TEMP (CENT)

BLM-I 24 SEPT 80 10

Figure 5g1

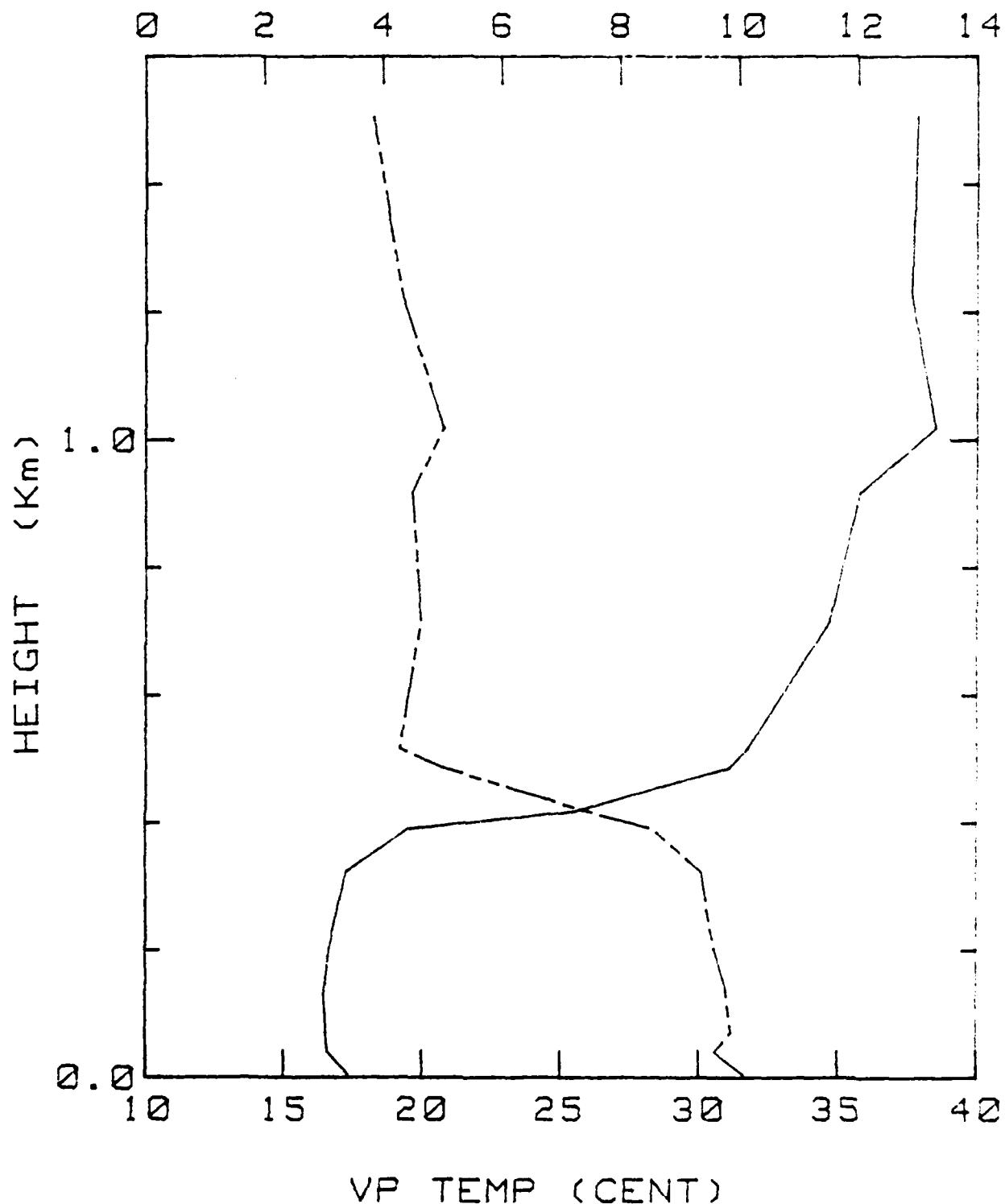
REL HUMIDITY (%)



BLM-I 24 SEPT 80 1215

Figure 5g2

MIX RATIO (G/KG)



BLM-I 24 SEPT 80 1215

Figure 5hl

REL HUMIDITY (%)

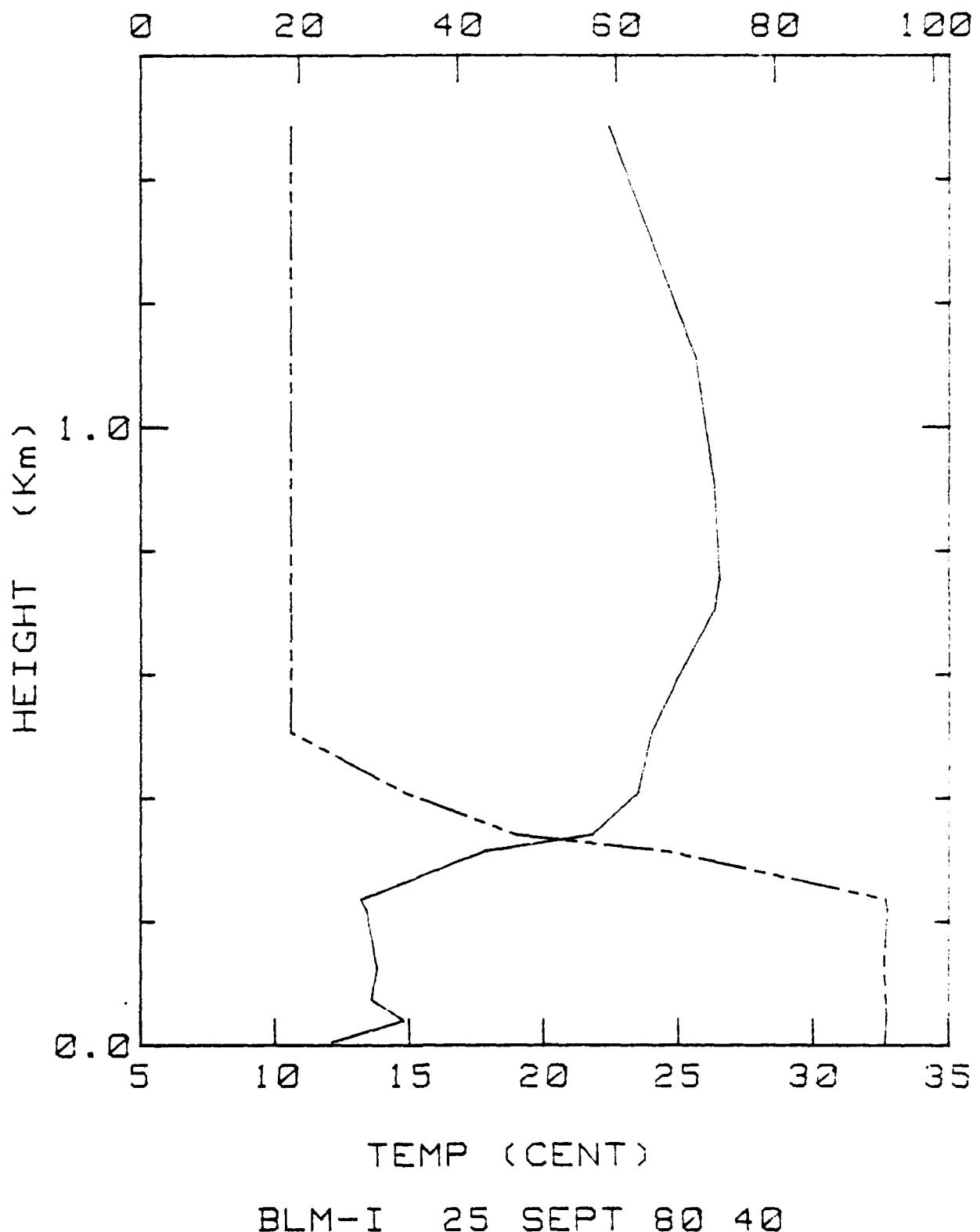
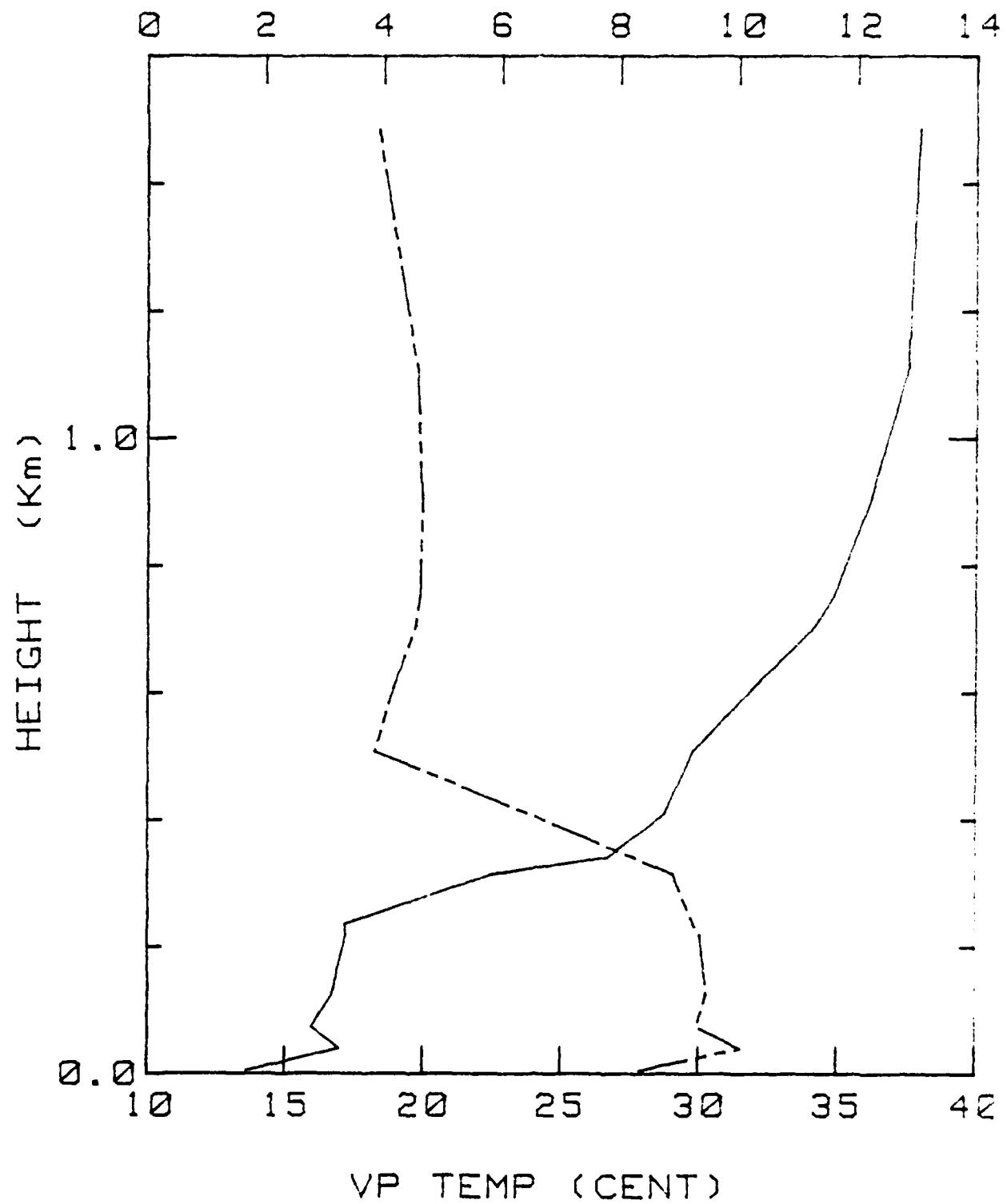


Figure 5h2

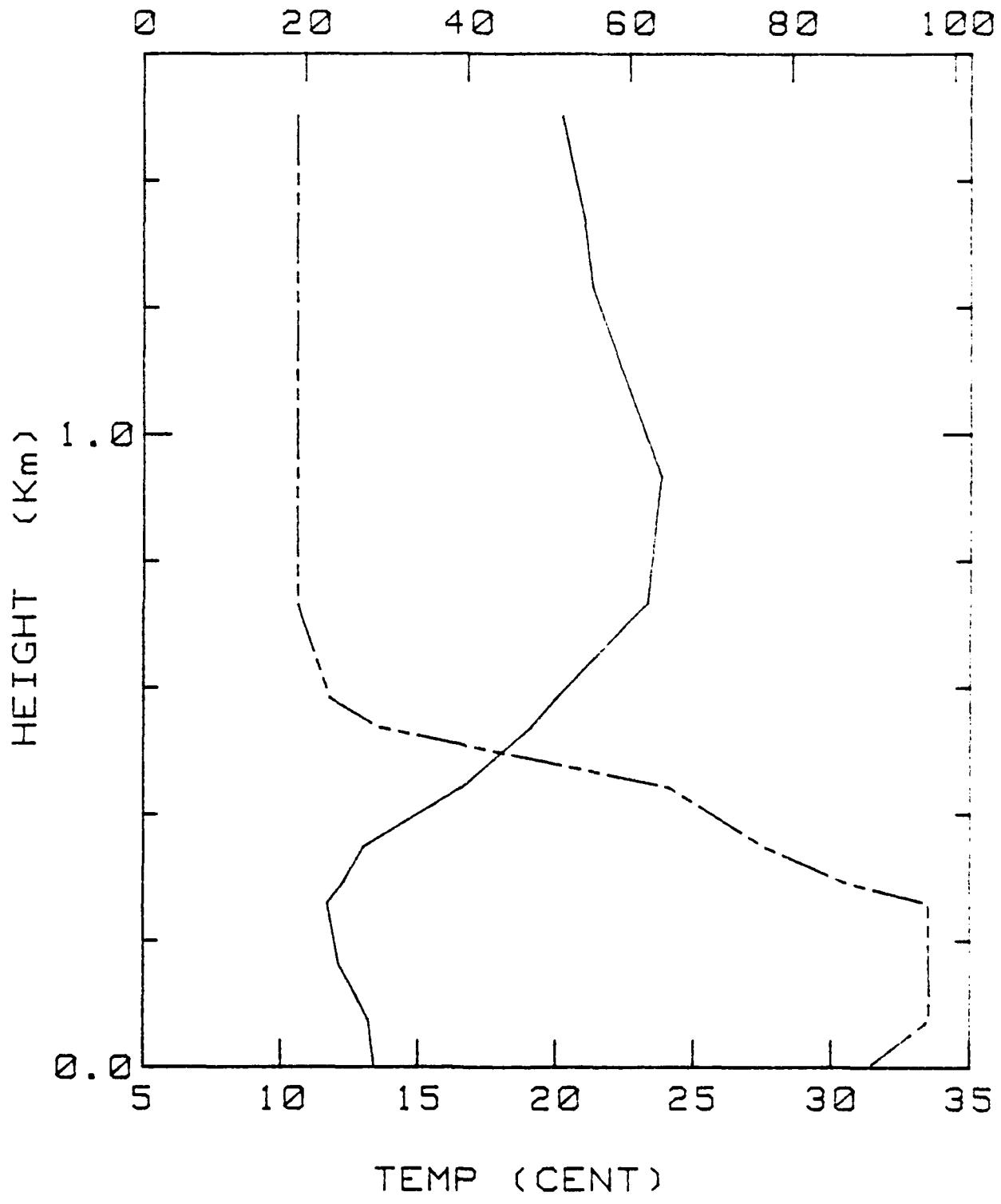
MIX RATIO (G/KG)



BLM-I 25 SEPT 80 40

Figure 5i1

REL HUMIDITY (%)



BLM-I 27 SEPT 80 607

Figure 5i2

MIX RATIO (G/KG)

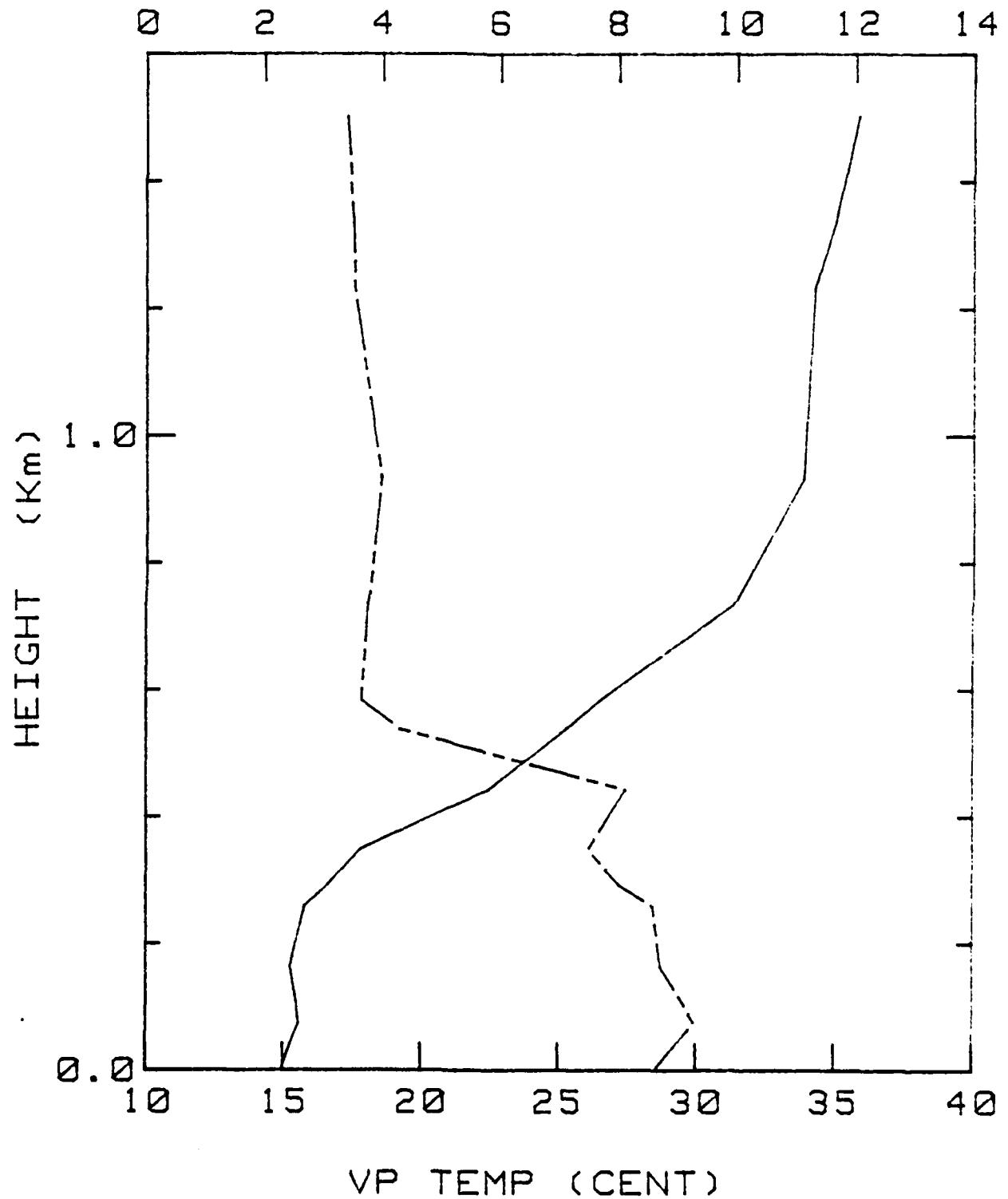
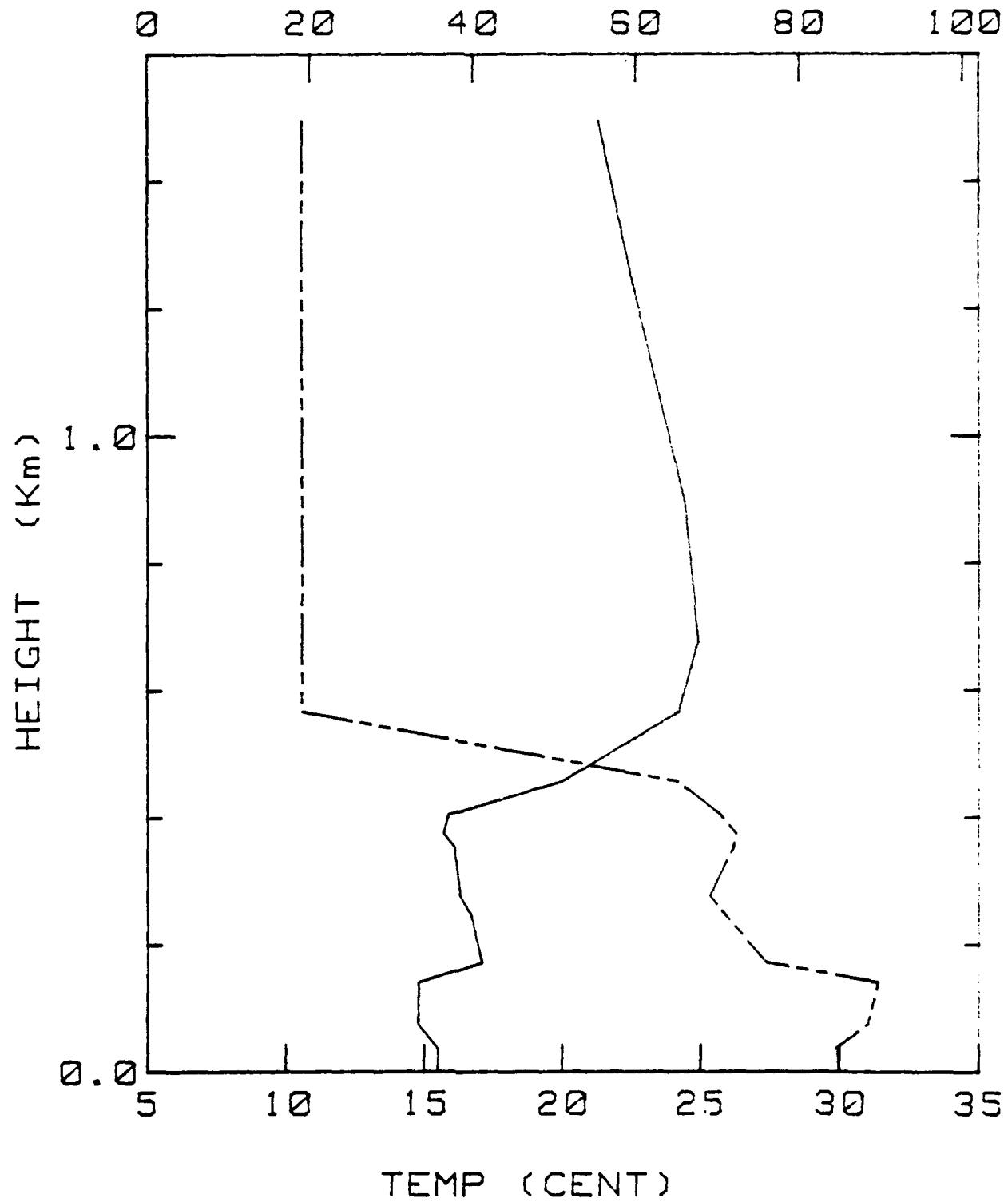


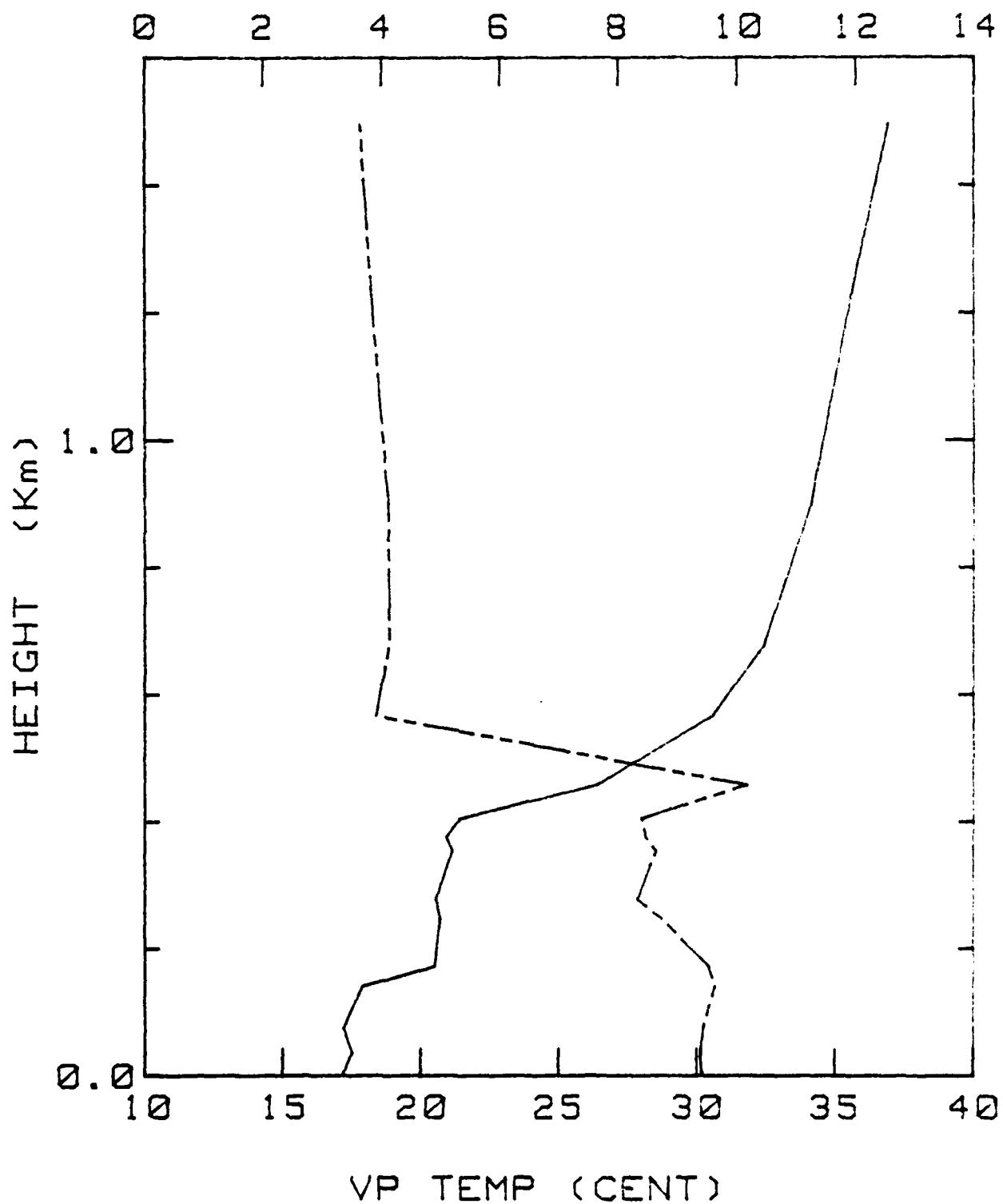
Figure 5j1
REL HUMIDITY (%)



BLM-I 27 SEPT 80 1820

Figure 5j2

MIX RATIO (G/KG)

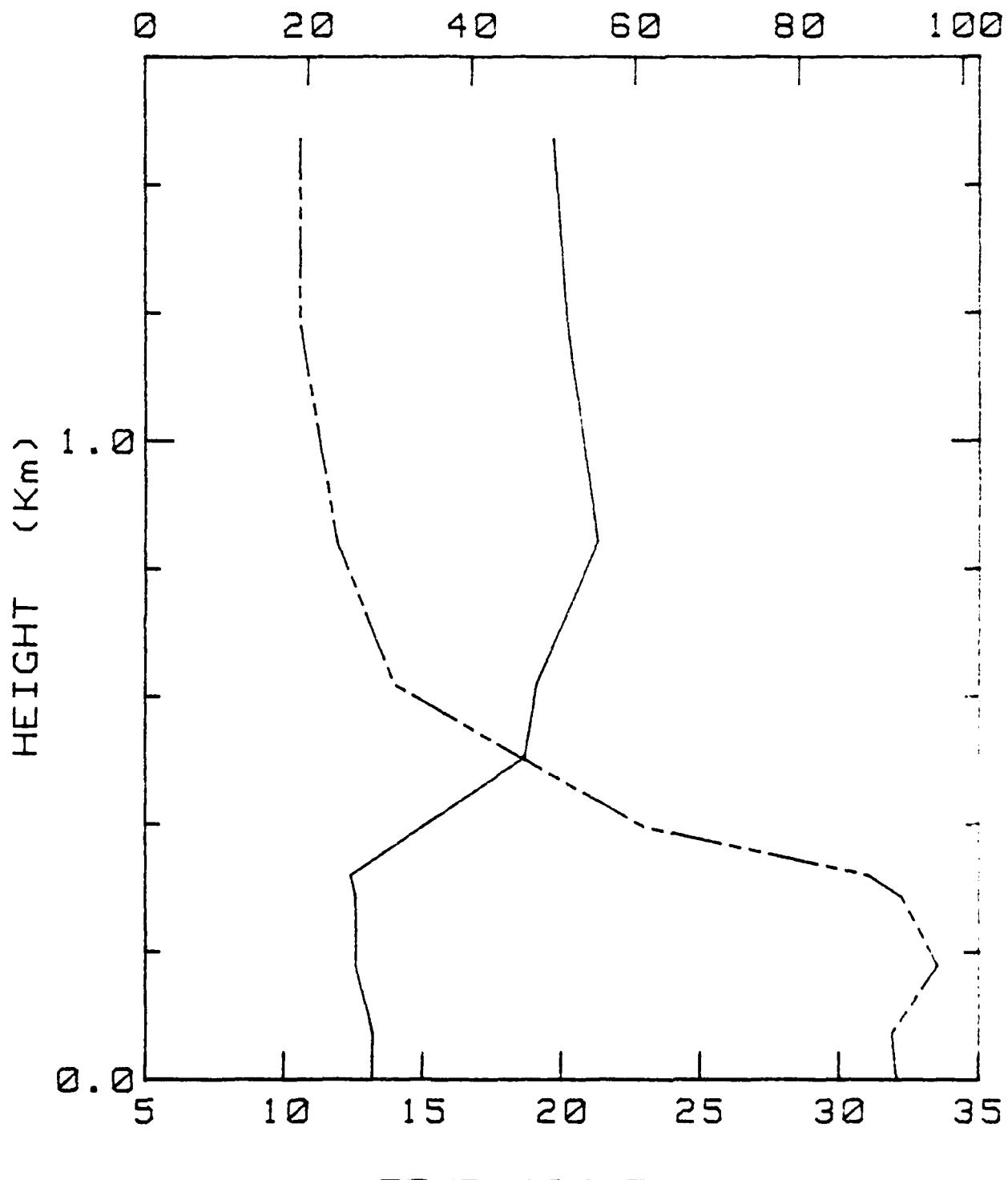


VP TEMP (CENT)

BLM-I 27 SEPT 80 1820

Figure 5k1

REL HUMIDITY (%)



BLM-I 28 SEPT 80 740

Figure 5k2

MIX RATIO (G/KG)

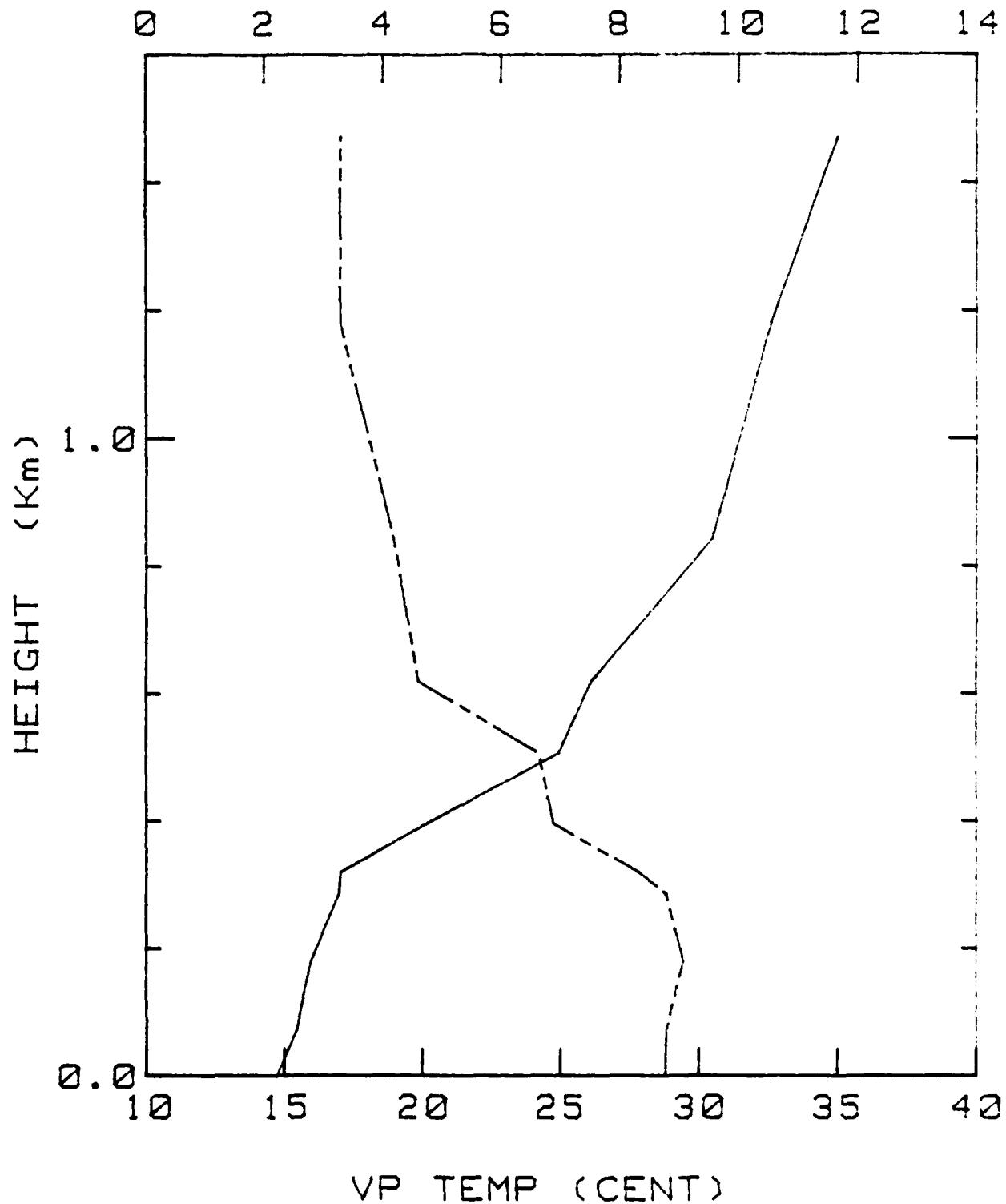
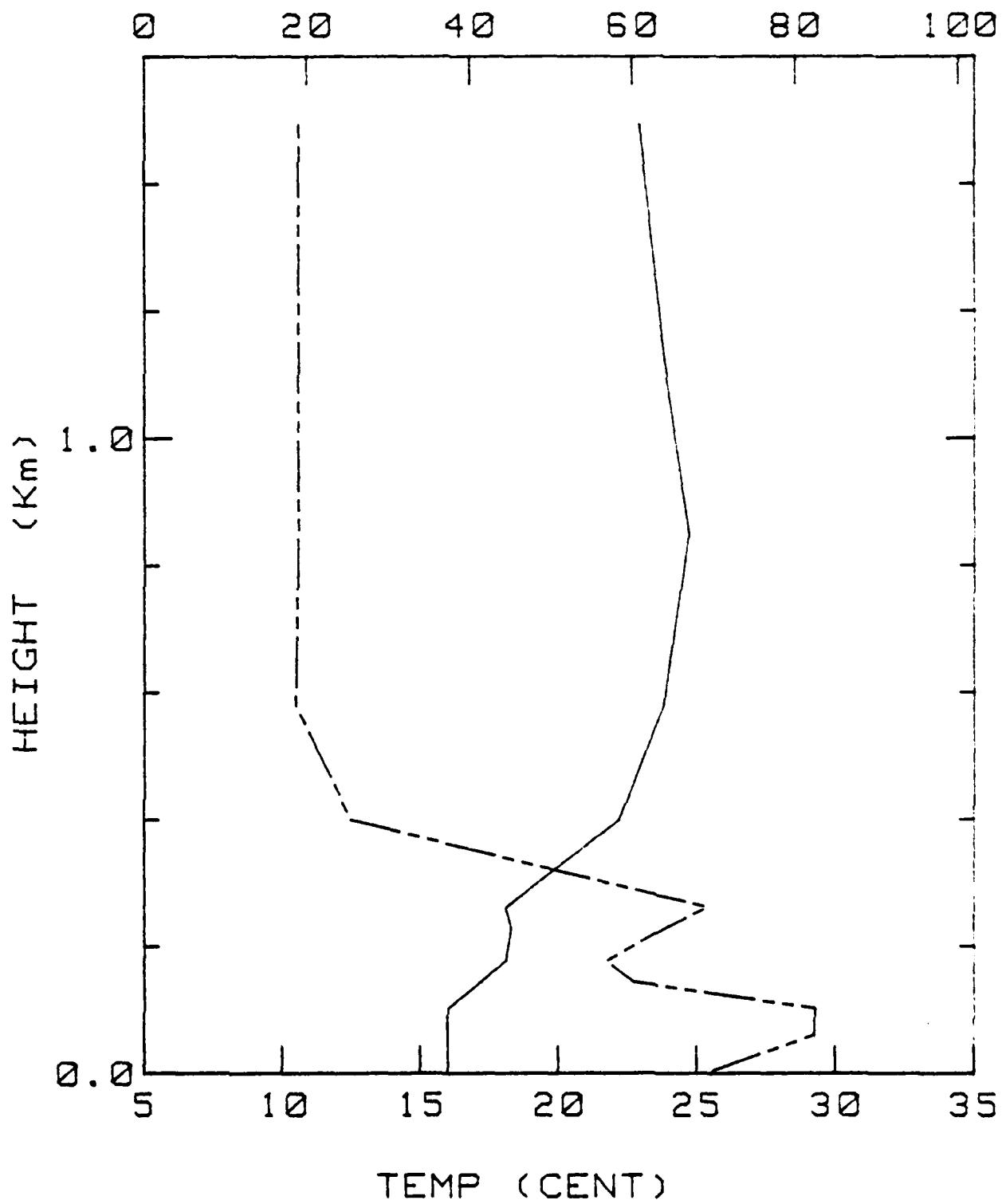


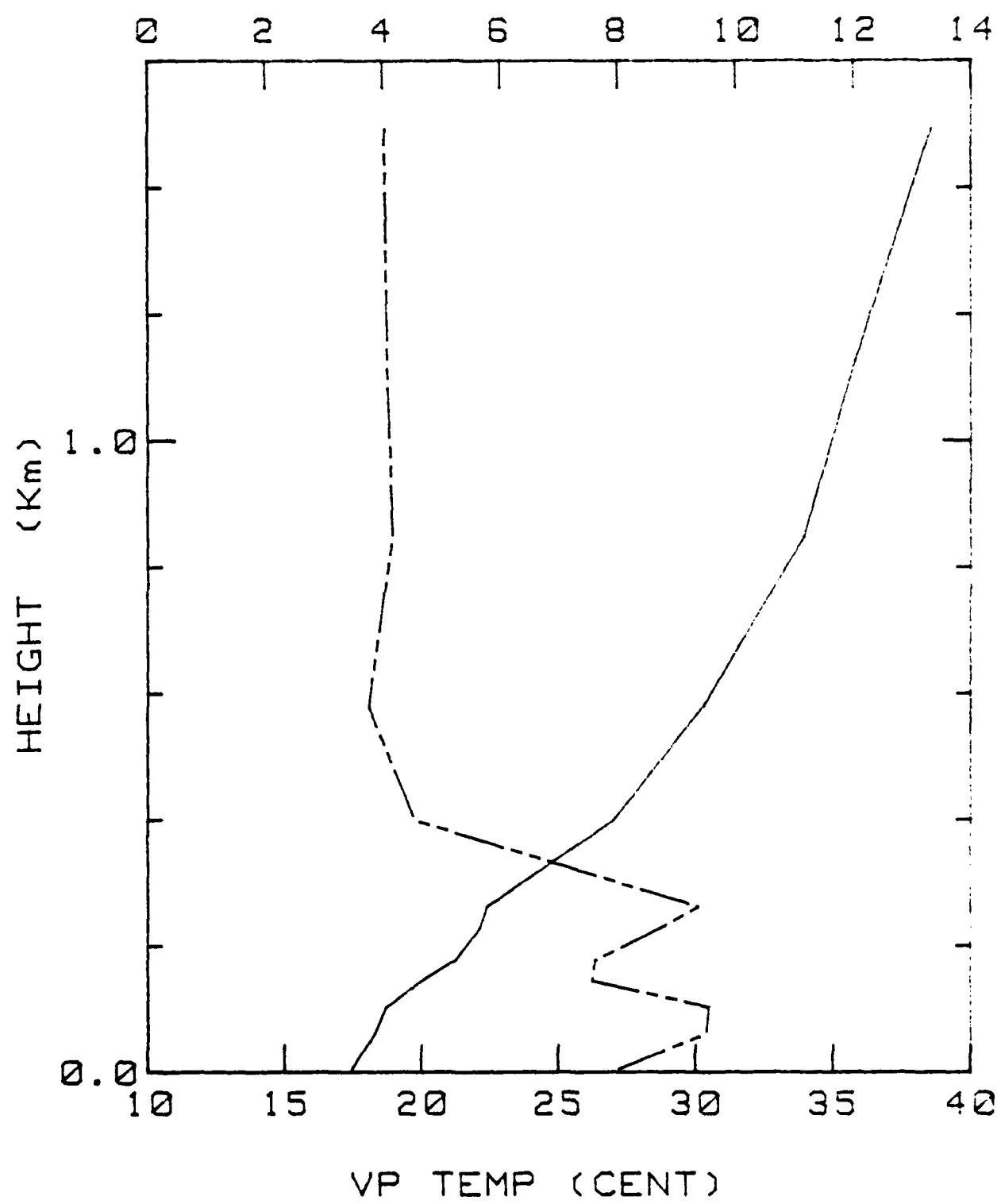
Figure 511
REL HUMIDITY (%)



BLM-I 28 SEPT 80 1705

Figure 512

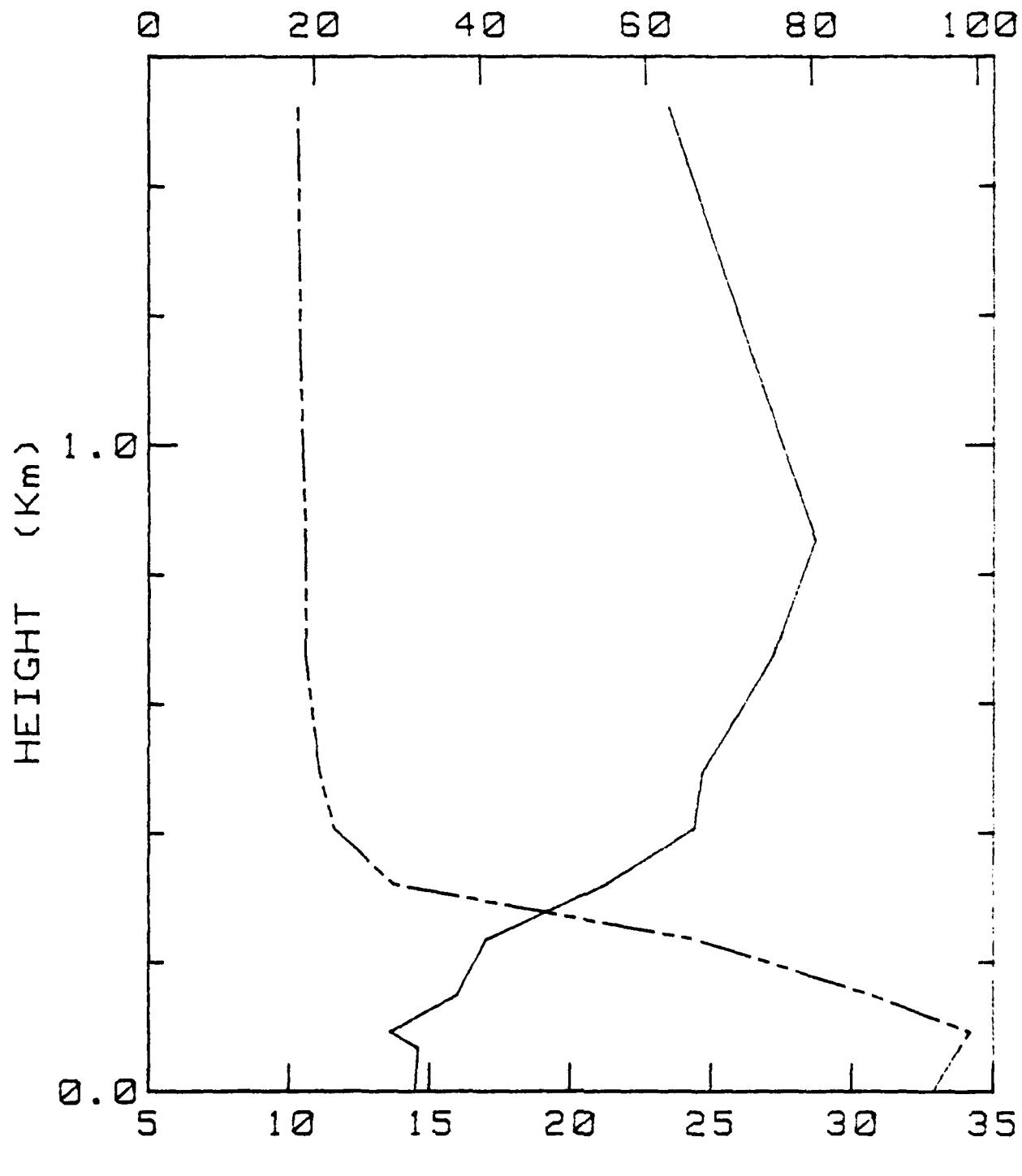
MIX RATIO (G/KG)



BLM-I 28 SEPT 80 1705

Figure 5ml

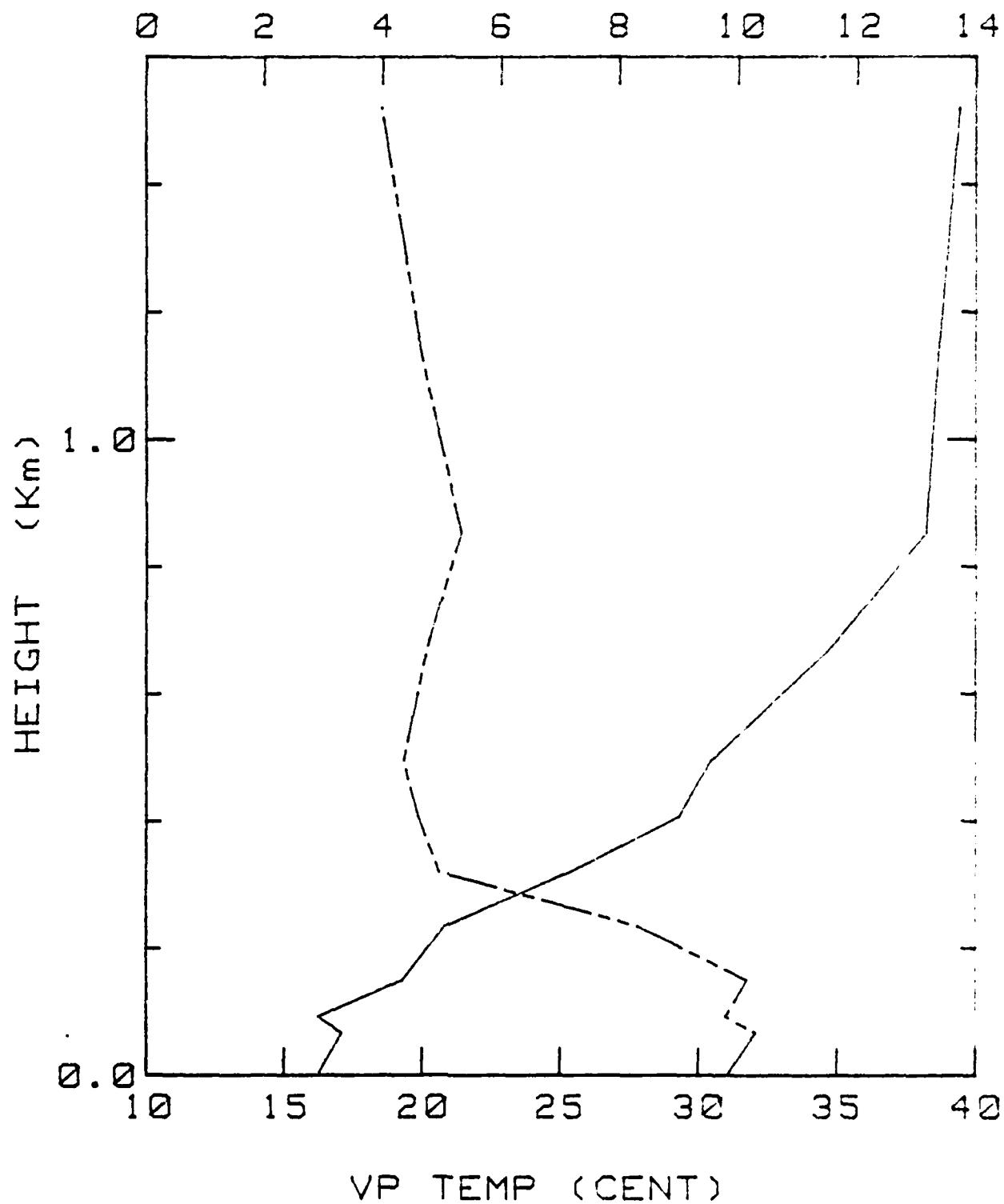
REL HUMIDITY (%)



BLM-I 29 SEPT 80 630

Figure 5m2

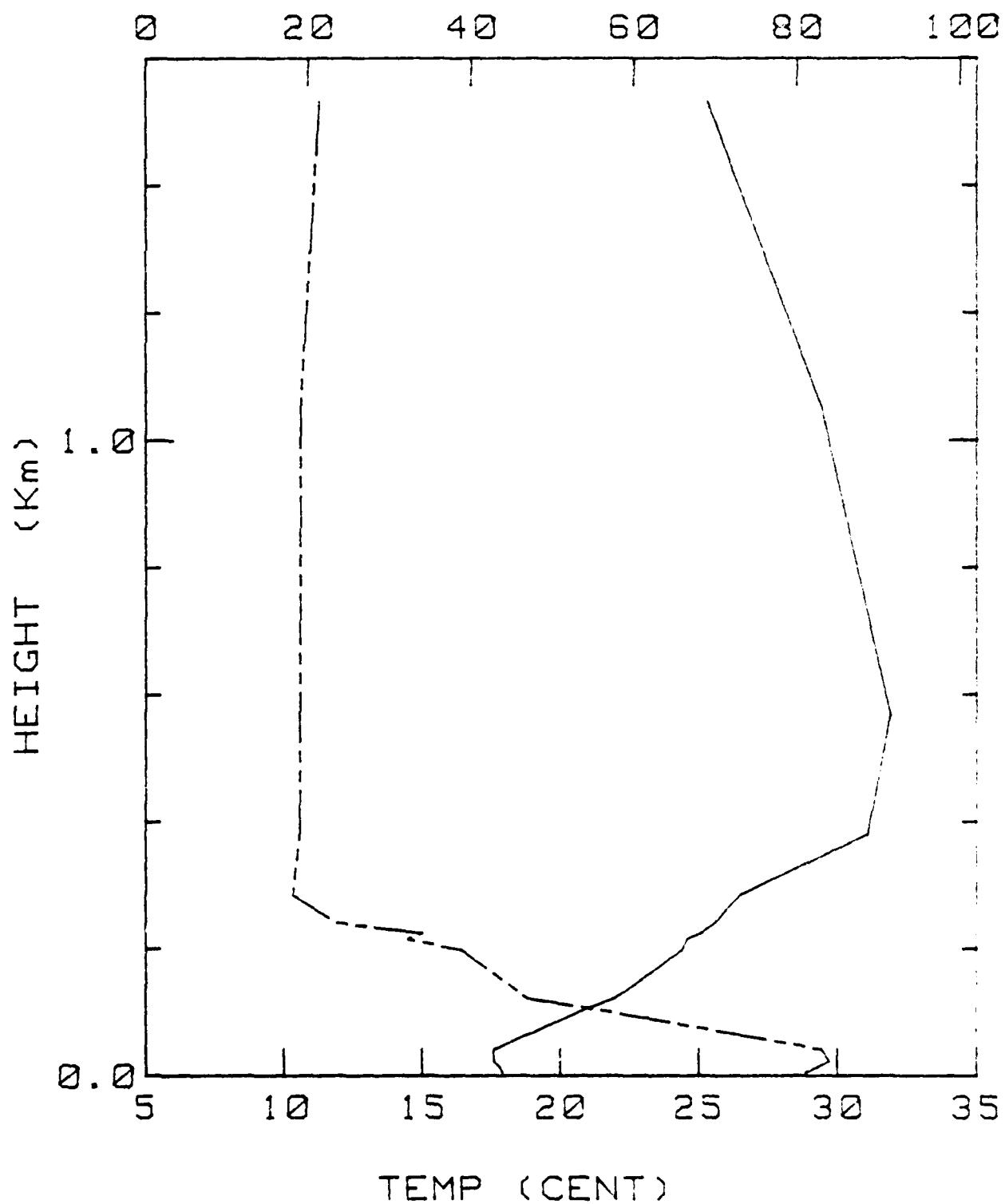
MIX RATIO (G/KG)



BLM-I 29 SEPT 80 630

Figure 5n1

REL HUMIDITY (%)



TEMP (CENT)

BLM-I 29 SEPT 80 1735

Figure 5n2

MIX RATIO (G/KG)

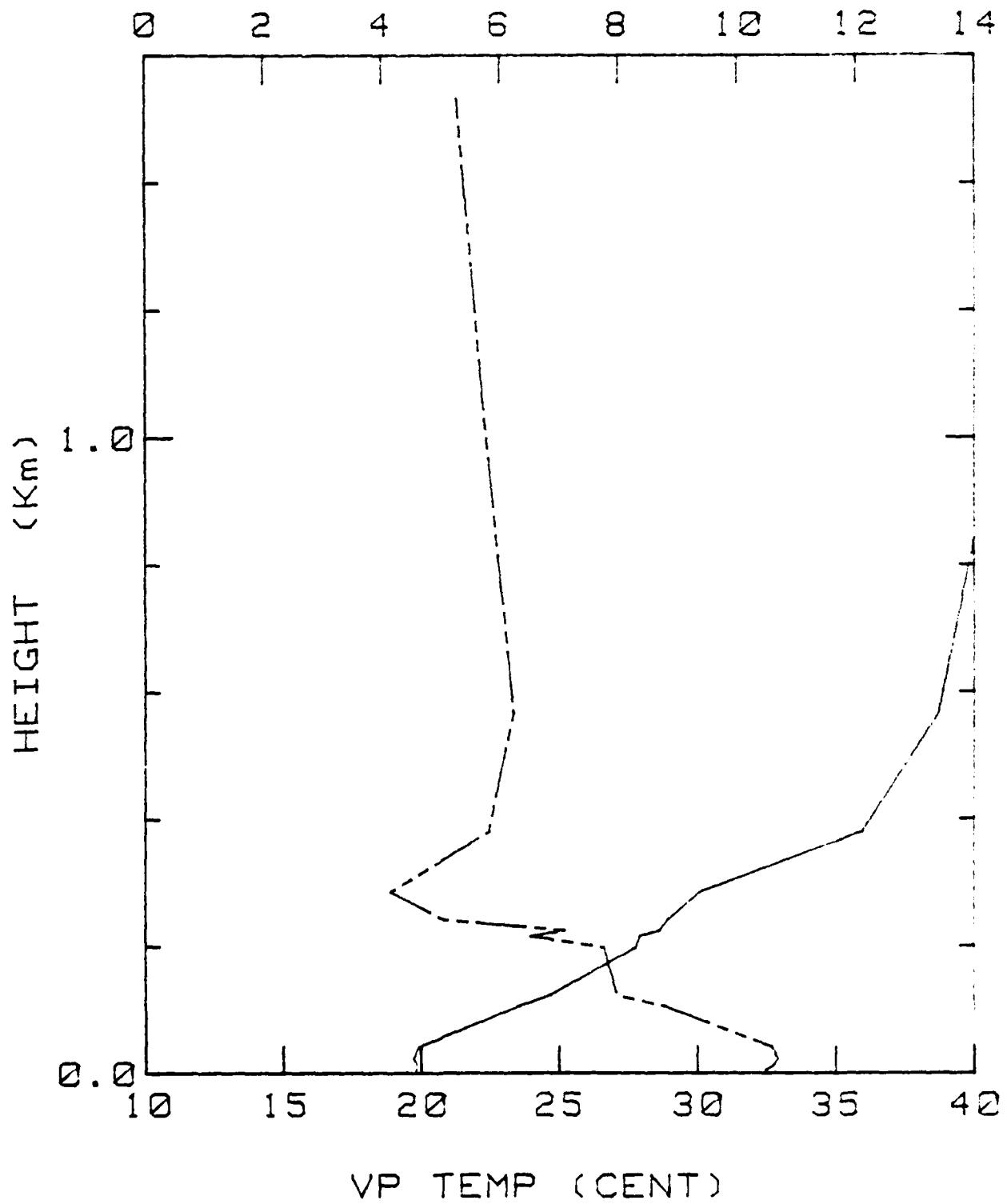
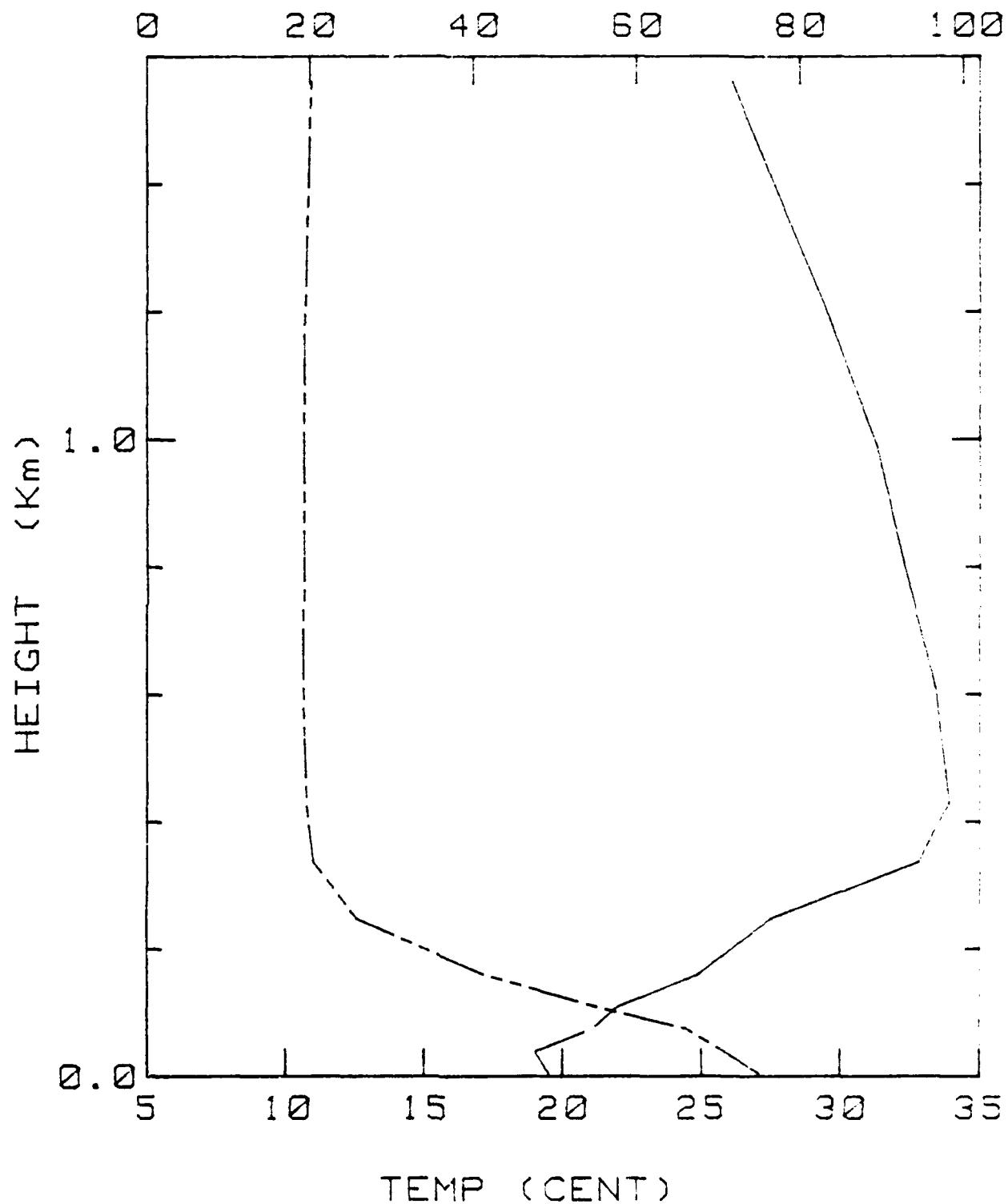


Figure 501

REL HUMIDITY (%)



BLM-I 30 SEPT 80 1207

AD-A098 341

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1981 6 E SCHACHER, K L DAVIDSON

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F/6 4/2

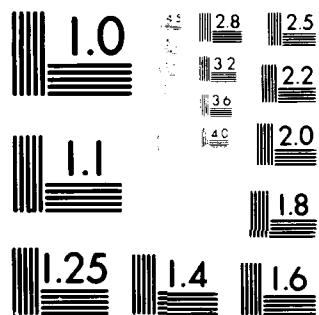
NL

2 of 2

474

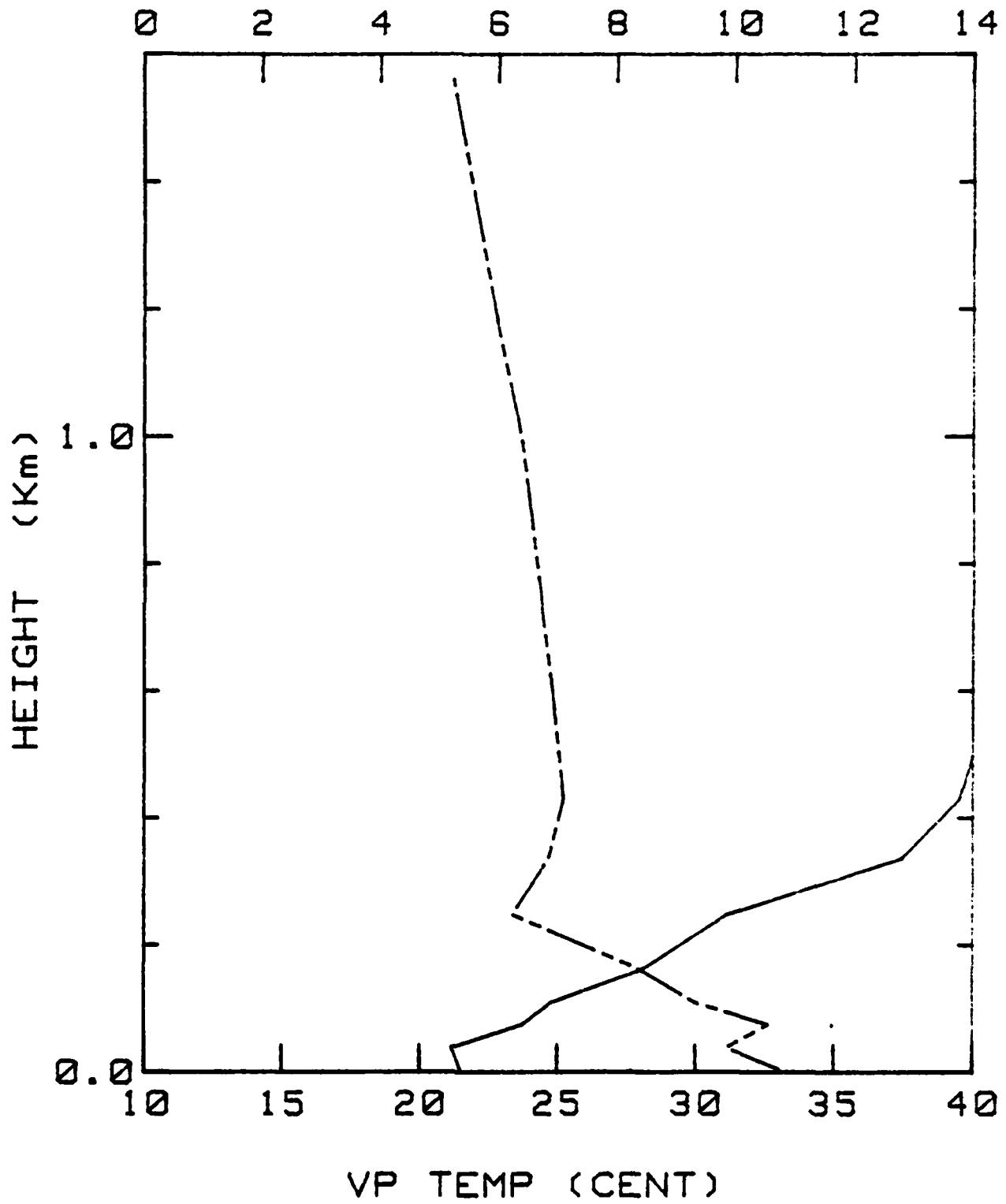
WAB 100

END
DATE
FILED
5-8-81
DTIC



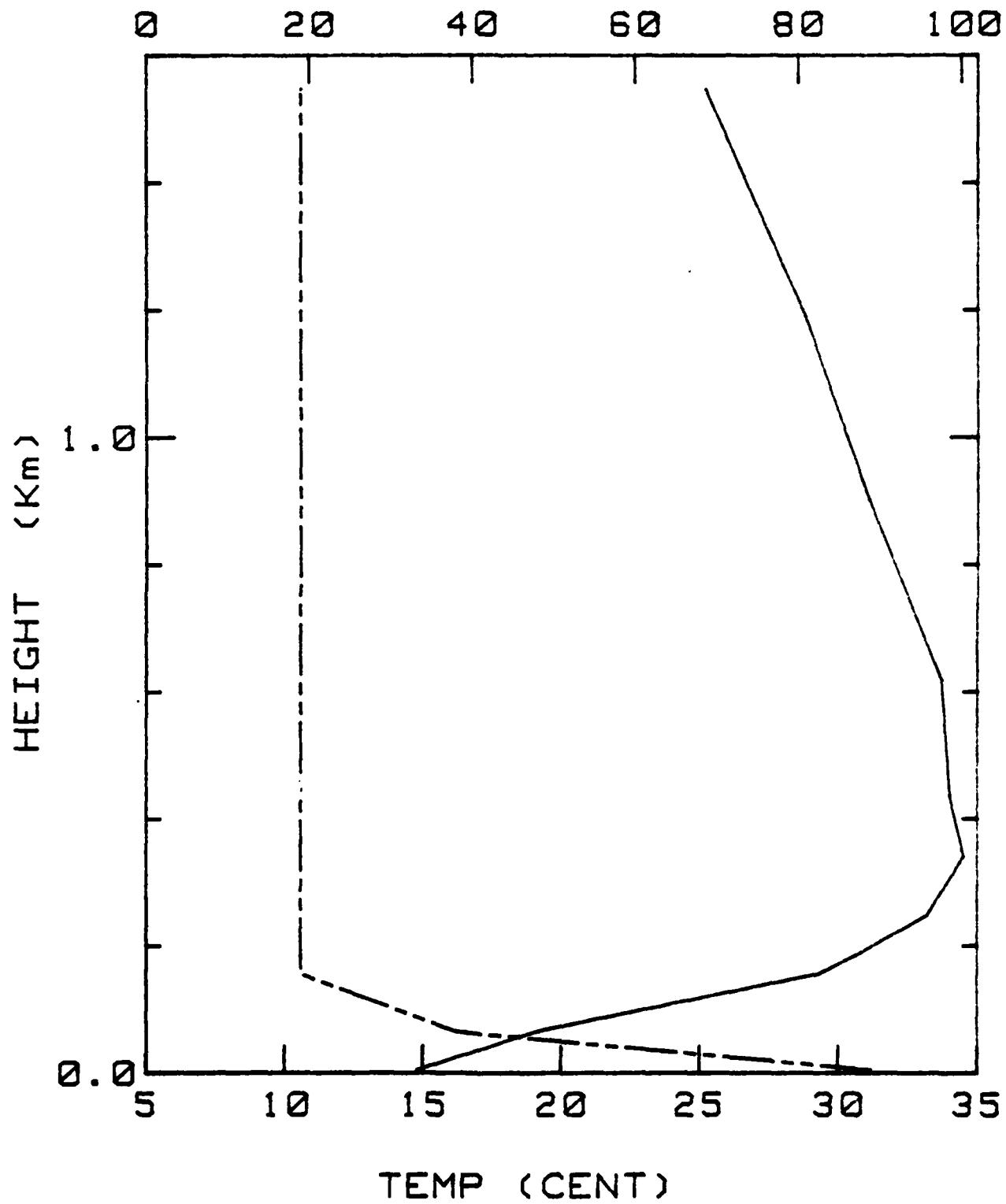
MICROCOPY RESOLUTION TEST CHART
MADE BY RICHARD C. STANLEY, LTD., LTD.

Figure 5o2
MIX RATIO (G/KG)



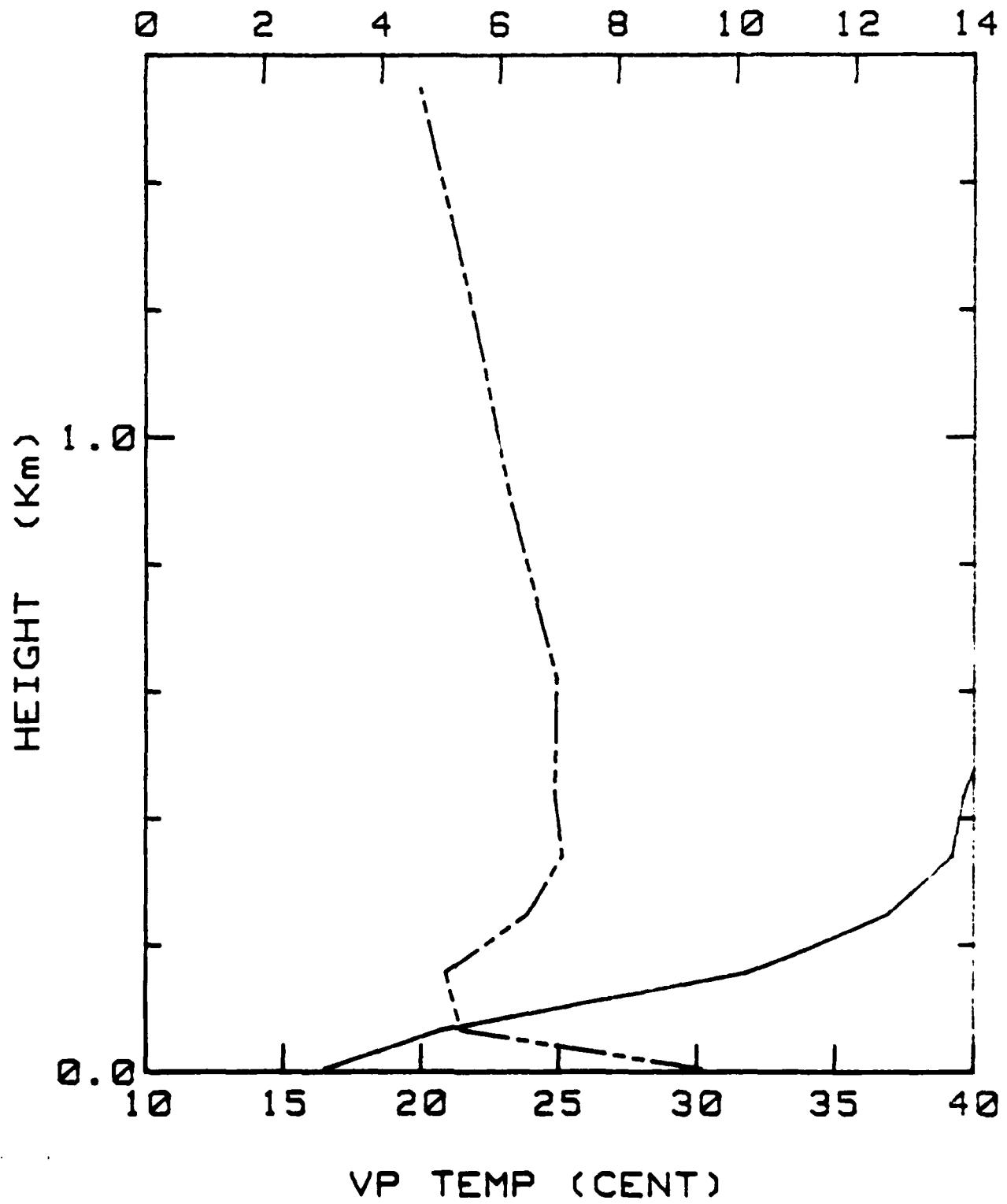
BLM-I 30 SEPT 80 1207

Figure 5pl
REL HUMIDITY (%)



BLM-I 1 OCT 80 25

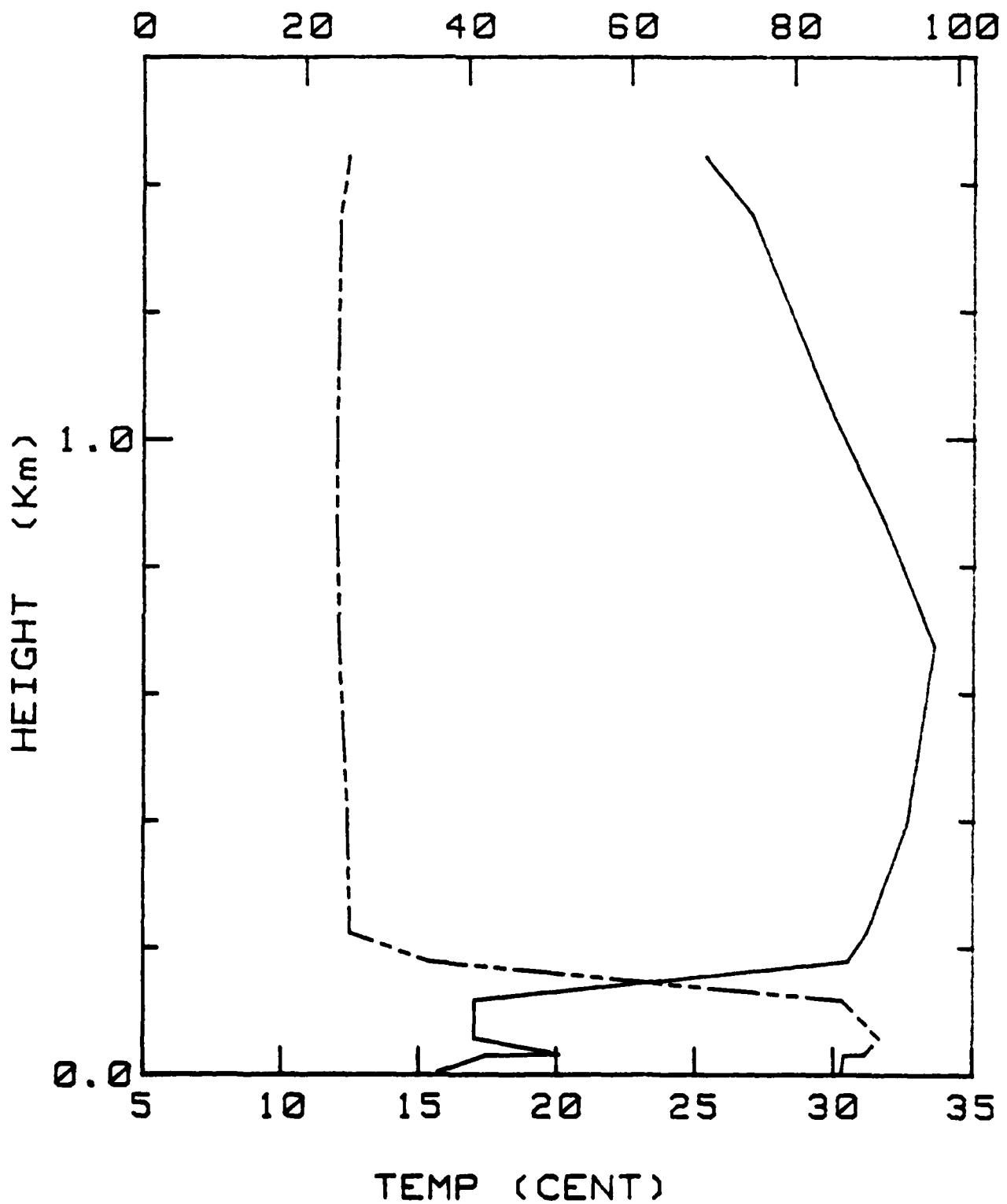
Figure 5p2
MIX RATIO (G/KG)



BLM-I 1 OCT 80 25

Figure 5ql

REL HUMIDITY (%)



BLM-I 1 OCT 80 1230

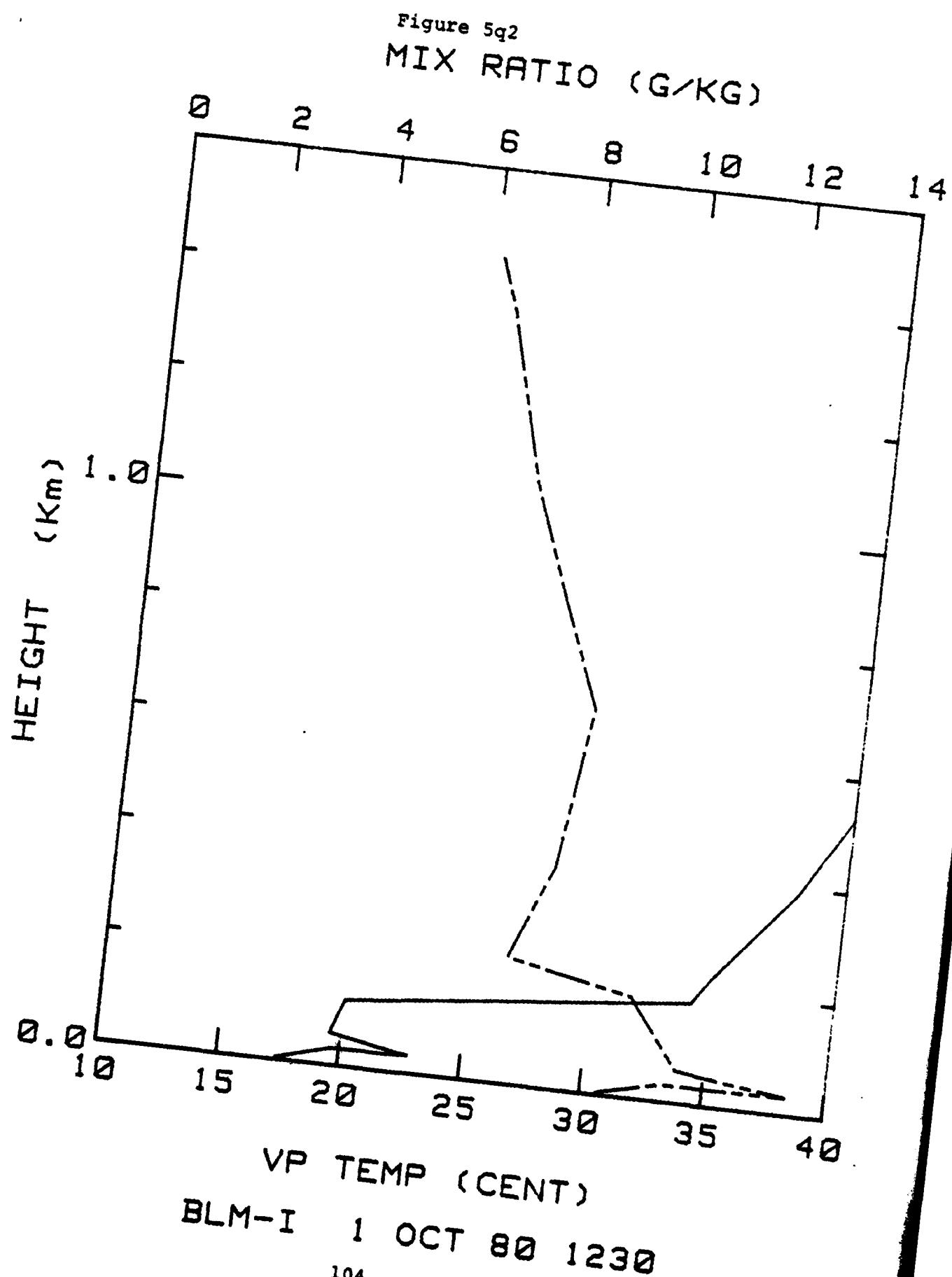
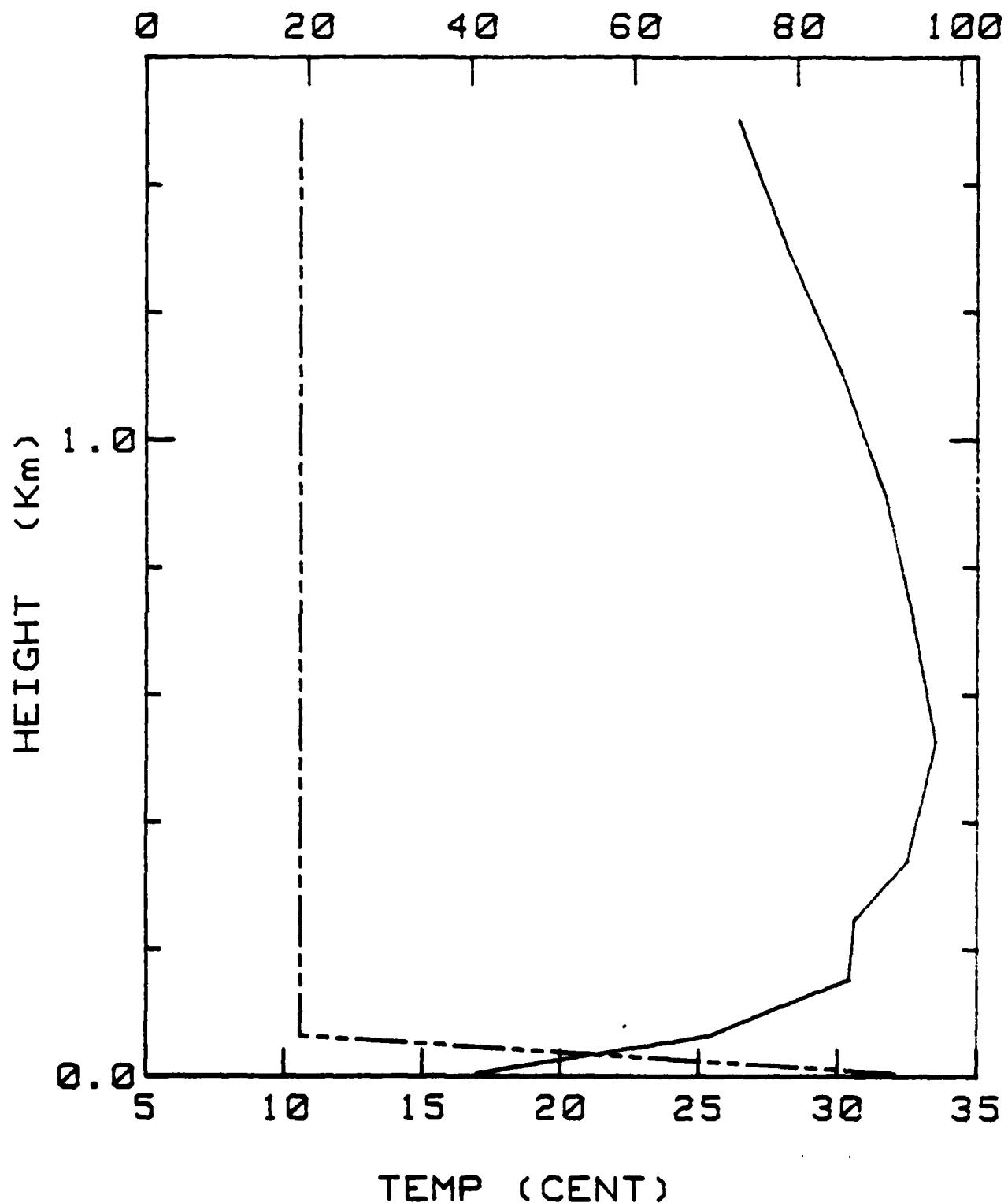


Figure 5q1

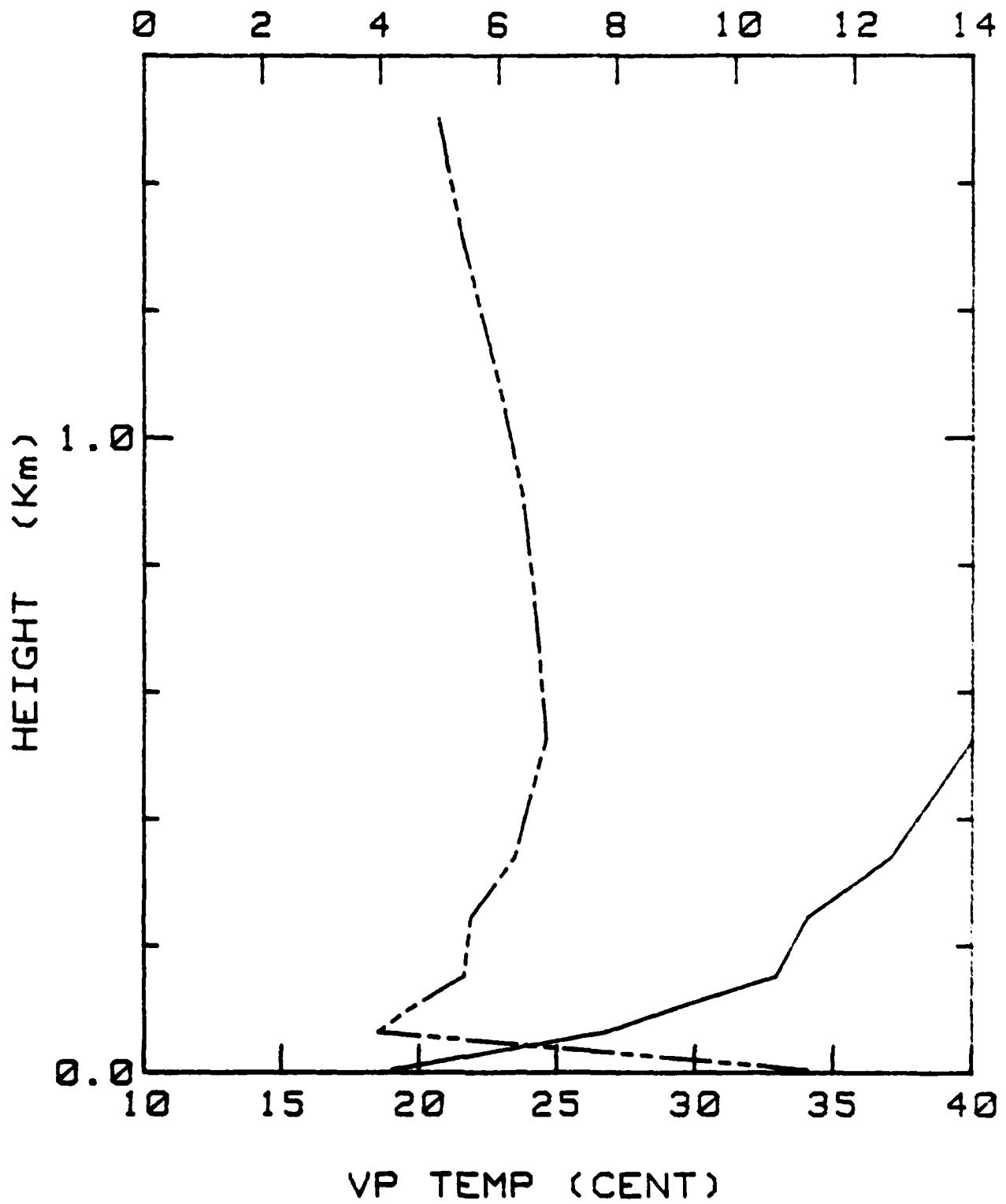
REL HUMIDITY (%)



BLM-I 1 OCT 80 2200

Figure 5r2

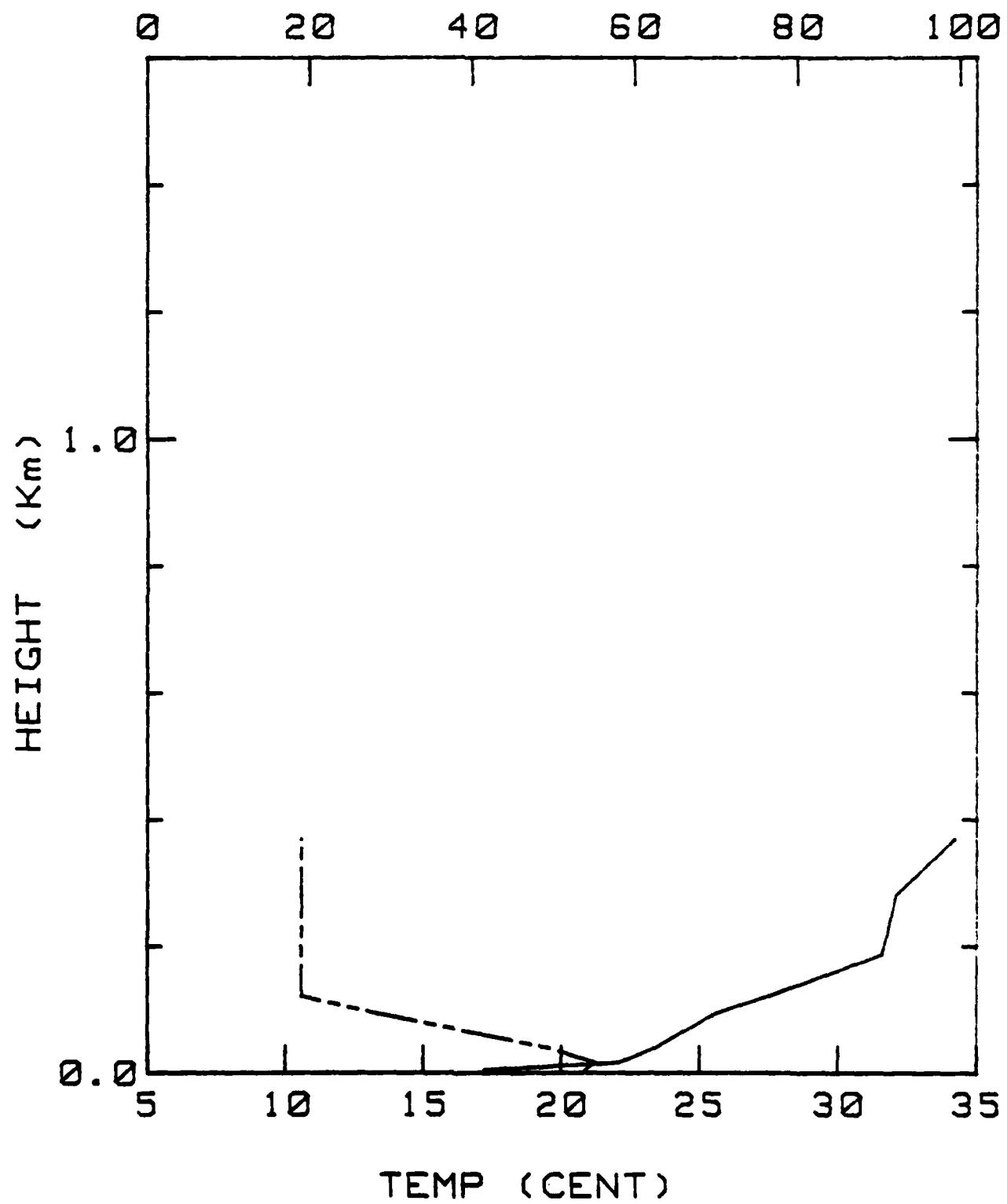
MIX RATIO (G/KG)



BLM-I 1 OCT 80 2200

Figure 5s1

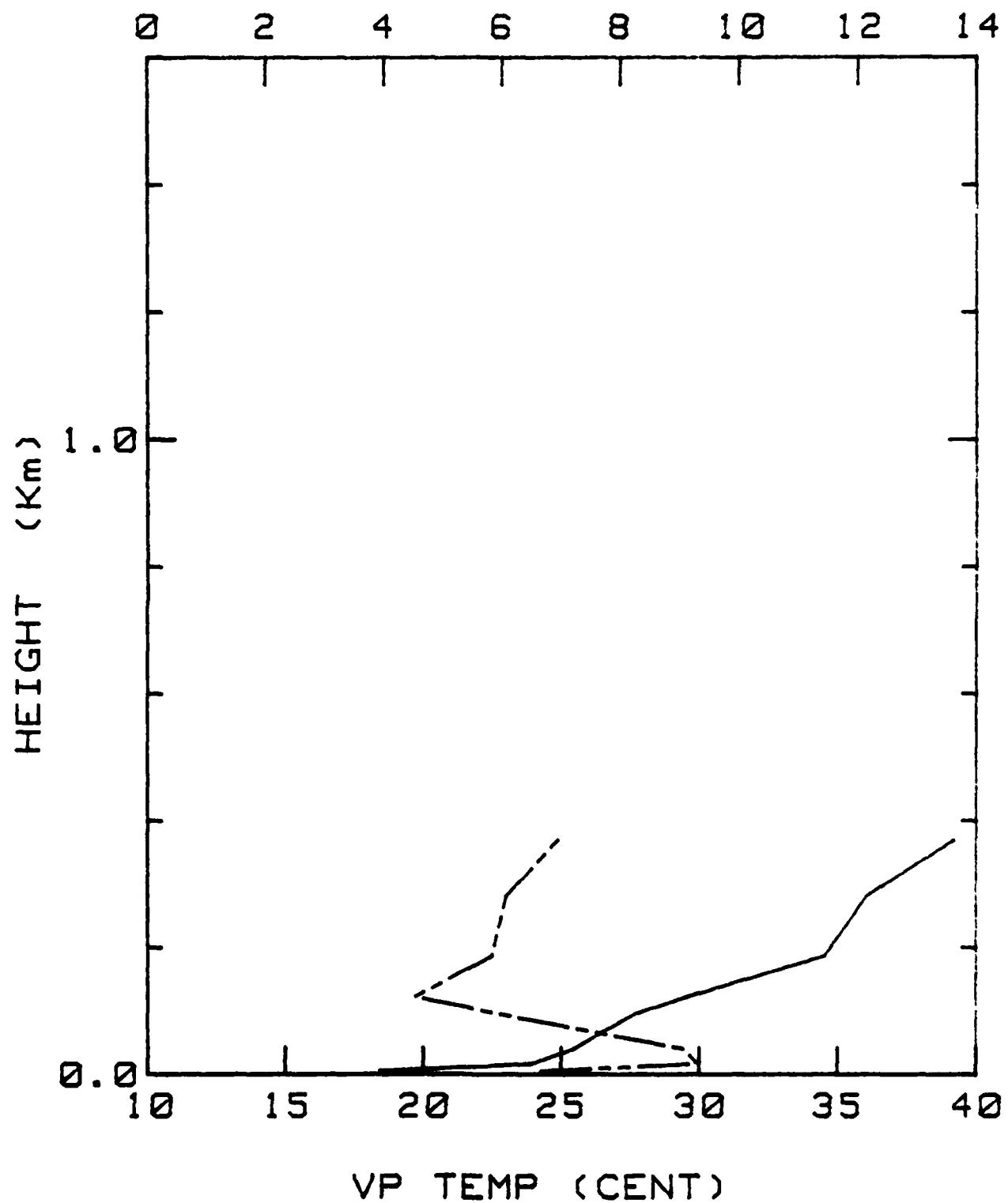
REL HUMIDITY (%)



BLM-I 2 OCT 80 1038

Figure 5s2

MIX RATIO (G/KG)



VP TEMP (CENT)

BLM-I 2 OCT 80 1038

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